

Submitted to: Sumitomo Metal Mining Pogo, LLC Delta Junction, Alaska Submitted by: AECOM Fort Collins, Colorado 60284905.2200 November 2013

Sumitomo Metal Mining Pogo LLC Unit 412 Incinerator Test Report

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Prepared By:

Emissions Measurements Manager

Reviewed By:

Doug Bopray

Air Quality Scientist

Executive Summary

Sumitomo Metal Mining Pogo LLC (Pogo) is located near Delta Junction, Alaska. Pogo operates a solid waste incinerator under an Alaska Department of Environmental Conservation (ADEC), Air Quality Control Minor Permit Number AQ0406MSS05, issued on May 12, 2011. Pogo's incinerator, permitted as Unit 412, is used to burn non-hazardous waste. Pogo's incinerator is considered a small, remote commercial and industrial solid waste incinerator under U.S. Environmental Protection Agency's (USEPA's) New Source Performance Standards for Commercial and Industrial Solid Waste Incineration (CISWI) Units, 40 Code of Federal Regulations (CFR) Part 60, Subpart CCCC.

40 CFR Part 60, Subpart CCCC, Table 8 specifies the applicable emission limits, averaging times, and performance test methods for determining compliance for the following pollutants from small, remote incinerators that commenced construction after June 4, 2010:

- Particulate (PM);
- Nitrogen Oxides (NO_x);
- Visual Smoke;
- Dioxins and Furans (D/F);
- Cadmium (Cd);
- Mercury (Hg);
- Sulfur Dioxide (SO₂);
- Carbon Monoxide (CO);
- Hydrochloric Acid (HCI); and
- Lead (Pb).

During September 29 through October 2, 2013, an initial performance test was conducted to determine compliance with the emissions limits in Table 8. The measurements and analytical procedures followed during the source testing are accepted USEPA Reference Method (RM) procedures and defined in 40 CFR 60, Appendix A. The measurements results are provided in the same engineering units as the applicable emissions standards and emission rate for ease of evaluation.

Pogo retained AECOM, Technical Services, Inc. (AECOM) to perform the required emissions measurements. AECOM is located at 1601 Prospect Parkway, Fort Collins, Colorado 80525-9769. Mr. John Rosburg, AECOM Emissions Measurements Manager, is the Project Manager for this test program. Mr. Rosburg may be reached by telephone at (970) 420-0602 or by e-mail at john.rosburg@aecom.com. Ms. Sally McLeod, Pogo's Environmental Manager was responsible for the coordination of the test program and collection of process data. Ms. McLeod may be reached by telephone at (907) 895-2879, by cell phone at (907) 978-3774, or by e-mail at Sally.Mcleod@smmpogo.com. Zach Hedgpeth, USEPA Region 10, observed emission measurements performed on September 29 and 30, 2013. Robin Wagner, ADEC, observed emission measurements performed on October 1, 2013.

Four RM5/26A RM 23 and RM 29 sample runs were performed at the Unit 412 incinerator test location. In addition, $10~NO_x$, SO_2 , and CO continuous emission monitor system (CEMS) sample runs were conducted at the Unit 412 test location. Three RM 22 sample runs also were performed.

In addition to source testing to demonstrate compliance with the Subpart CCCC, Table 8 emission limits, the initial performance test also served to establish the seven operating limits that Pogo identified in its

petition submitted to the USEPA pursuant to 40 CFR 60.2115. In its petition, Pogo proposed the operating limits on the following parameters:

- Charge rate;
- · Charge interval;
- Primary chamber temperature;
- Primary chamber burn time;
- Secondary chamber temperature;
- Secondary chamber burn time; and
- Waste composition.

In the USEPA's acceptance of Pogo's petition, it proposed establishing the waste composition limit by varying the relative amounts of each waste component on each day of testing. During a September 18, 2013, teleconference meeting with the USEPA, it was agreed that four test runs of each required method would be conducted over the four day testing period. On each day, the waste composition consisted of different percentages of its three components: municipal solid waste (MSW), sewage sludge, and cleanup adsorbs. The highest percentage of each waste component that was burned on one of those days would be established as the upper bound (provided that day's test results demonstrated compliance with applicable emission limits). On the fourth day of testing, the waste composition was composed of 100 percent MSW to determine whether an upper bound on the MSW component was necessary. Compliance with the HCI emission limit was not demonstrated while burning 100 percent MSW. Therefore, only the results of the first 3 day's test runs, comprising three valid runs of each required test method, are being used to demonstrate compliance with the applicable emission limits of Subpart CCCC and to establish the operating limits under which the incinerator will operate. The results from the day 4 testing are included in this report but are not included in the 3-run averages shown in the tables.

Table ES-1 provides the individual and average results of the measurements conducted on the first three days of testing. The results are provided in terms of pertinent concentrations (milligrams per dry standard cubic meter [mg/dscm] @ 7% oxygen [O₂], parts per million, volumetric dry [ppmvd], ppmvd @ 7% O₂, and nanograms per dry standard cubic meter [ng/dscm] @ 7% O₂). With the exception of SO_2 , **Table ES-1** shows that all the Subpart CCCC emissions limits were met for the various wastecomposition mixtures on the first 3 days of testing. A separate Site Specific Operating Report which provides all seven operating limits established by this performance test will be submitted by Pogo.

Table ES-0-1 Unit 412 Measurements Results Summary

Test Parameter	Units	9/29/13	9/30/13	10/1/13	3 Run Average	Emission Standard
PM	mg/dscm	86.8	56.4	75.5	72.87	270
SO ₂	ppmvd	35.1	30.1	19.8	27.2	1.2
NO _x	ppmvd	93.0	79.2	86.7	85.8	170
СО	ppmvd	0.3	1.5	0.7	1.0	13
D/F	TEQ ng/dscm ¹	0.032	0.267	0.113	0.137	31
Hydrogen Chloride (HCI)	ppmvd	193	136	138	155	200
Cd	mg/dscm	0.01	0.01	0.01	0.01	0.67
Pb	mg/dscm	0.01	0.51	0.22	0.28	2.0
Hg	mg/dscm	0.0023	0.0009	0.0002	0.0011	0.0035

Toxicity equivalence concentration (nano-grams per dry standard cubic meter.

Note 2: Visual determinations of smoke emissions were conducted between 9/30/13 and 10/1/13 according to RM 22. A total of three observation periods of 60 minutes each were performed. The observations were performed simultaneously with particulate, metals, and D/F sample runs. The emission frequency resulted in zero percent for all three observation periods.

Note 1: Measurement results are presented in the units of the applicable emission standards in 40 CFR Part 60, Subpart CCCC, Table 8 (results corrected to an oxygen content of 7 percent).

Contents

Exec	cutive	Summary	ES-1
1.0	Intro	oduction	1-1
2.0	Test	t Approach	2-1
	2.1	Equipment Preparation	2-1
	2.2	Summary of Field Measurements	2-1
	2.3	Particulate and Hydrogen Chloride Results	2-2
	2.4	Cadmium, Lead, and Mercury Results	2-4
	2.5	Dioxin and Furan Results	2-4
	2.6	Continuous Emission Monitor Results	2-8
	2.7	Visual Determination of Smoke Emissions Results	2-9
3.0	Proc	cess Description and Operation	3-1
	3.1	Process Description	3-1
	3.2	Process Operation	3-1
4.0	Meth	hodology	4-1
	4.1	Support Measurements for Stack Parameters	
		4.1.1 Selection of Traverse Points by Reference Method 1	
		4.1.2 Flow Rate Determination by Reference Method 2	
		4.1.3 Molecular Weight Determination by Reference Method 34.1.4 Percent Moisture Determination by Reference Method 4	
	4.2	Particulate Determination by Reference Method 5	
	4.3	Sulfur Dioxide Determination by Reference Method 6C	
	4.4	Nitrogen Oxides Determination by Reference Method 7E	
	4.5	Carbon Monoxide Determination by Reference Method 10	
	4.6	Visual Determination of Smoke Emissions by Reference Method 22	
	4.7	Dioxins and Furans Determination by Reference Method 23	
	4.7	4.7.1 Sample Train Component Preparation	
		4.7.2 Sample Collection	
		4.7.3 Sample Recovery	
		4.7.4 Sample Analysis	4-7
		4.7.5 Data Reduction	4-7
	4.8	Hydrogen Chloride Determination by Reference Method 26A	4-7
	4.9	Metals Determination by Reference Method 29	4-8

AECOM Environment ii

		4.9.1 4.9.2	Sampling by Reference Method 29Analyses by Reference Method 29	
	4.10	Calcula	ations and Nomenclature	4-10
5.0	Quali	ity Assu	rance/Quality Control	5-1
	5.1	Objecti	ves	5-1
	5.2	Field P	rogram	5-1
	5.3	Sample	e Documentation	5-2
	5.4	Analytic	cal Quality Control	5-2
	5.5	Data R	eduction, Validation, and Reporting	5-2

List of Appendices

Appendix A Field Data Forms and CEMS Data

Appendix B Laboratory Results

Appendix C Calibration Data

Appendix D Process Information

List of Tables

Table ES-1	Unit 412 Measurements Results Summary	ES-3
Table 2-1	Pogo's Unit 412 Test Matrix	2-1
Table 2-2	Pogo's Unit 412 Particulate and Hydrogen Chloride Results	2-3
Table 2-3	Pogo's Unit 412 Cadmium, Lead, and Mercury Results	2-5
Table 2-4	Pogo's Unit 412 Average Measured Test Parameters	2-6
Table 2-5	Pogo's Unit 412 Dioxin and Furan Results	2-7
Table 2-6	Pogo's Unit 412 Continuous Emission Monitor System	2-8
Table 2-7	Pogo's Unit 412 Visual Determination of Smoke Results	2-9
Table 3-1	Pogo's Unit 412 Summary of Process Operations	3-2
Table 4-1	Reference Method 29 Condensate (Impinger) Train	4-10

AECOM Environment iii

List of Figures

Figure 4-1	Reference Method 23 Sampling Train	4-6
Figure 4-2	Reference Method 29 Sampling Train	4-9

1.0 Introduction

Sumitomo Metal Mining Pogo LLC (Pogo) is located near Delta Junction, Alaska. Pogo operates its incinerator under an Alaska Department of Environmental Conservation (ADEC), Air Quality Control Minor Permit Number AQ0406MSS05, issued on May 12, 2011. Pogo's incinerator, permitted as Unit 412, is used to burn non-hazardous waste.

Pogo conducted an emissions measurements evaluation of Unit 412 in order to demonstrate compliance with the Commercial and Industrial Waste Incinerator (CISWI) emission standards and to establish the operating limits identified in Pogo's petition submitted to the U.S. Environmental Protection Agency (USEPA) under Code of Federal Regulations, Title 40, Part 60.2115 (40 CFR 60.2115). The September 2013 test program was designed to evaluate Unit 412 pollutant emission rates using different waste "recipes." The field measurements of Unit 412 included the following:

- Particulate (PM);
- Nitrogen Oxides (NO_x);
- Visual Smoke;
- Dioxins and Furans (D/F);
- Cadmium (Cd);
- Mercury (Hg);
- Sulfur Dioxide (SO₂);
- Carbon Monoxide (CO);
- Hydrochloric Acid (HCI); and
- Lead (Pb).

The measurements and analytical procedures followed for this source testing are accepted USEPA Reference Method (RM) procedures and defined in the (40 CFR 60), Appendix A. The measurements results are provided in the same engineering units as the applicable emissions standards and emission rate for ease of evaluation.

Pogo retained AECOM, Technical Services, Inc. (AECOM) to perform the required emissions measurements. AECOM is located at 1601 Prospect Parkway, Fort Collins, Colorado 80525-9769. Mr. John Rosburg, AECOM Emissions Measurements Manager, is the Project Manager for this test program. Mr. Rosburg may be reached by telephone at (970) 420-0602 or by e-mail at john.rosburg@aecom.com. Ms. Sally McLeod Pogo's Environmental Manager was responsible for the coordination of the test program and collection of process data. Ms. McLeod may be reached by telephone at (907) 895-2879, by cell phone at (907) 978-3774, or by e-mail at Sally.Mcleod@smmpogo.com. Zach Hedgpeth, USEPA Region 10, observed emission measurements performed on September 29 and 30, 2013. Robin Wagner, ADEC, observed emission measurement performed on October 1, 2013.

The following test report is organized as follows: the testing approach is provided in Chapter 2.0; a description of the process and operations is provided in Chapter 3.0; source test methodology, calculations, and nomenclature are presented in Chapter 4.0; a concise description of the quality assurance/quality control (QA/QC) procedures implemented are provided in Chapter 5.0; copies of the

field data sheets used and continuous emission monitor system (CEMS) 1-minute data averages are provided in **Appendix A**; copies of the laboratory results are provided in **Appendix B**; **Appendix C** contains copies of the equipment calibrations pertinent to this test program; and located in **Appendix D** are copies of the process information recorded during the test program.

2.0 Test Approach

The test plan and protocol outlined specific methods and procedures for quantifying PM, SO_2 , NO_x , CO_x visual smoke, D/F, HCl, Cd, Pb, and Hg emissions results from Unit 412. All measurements procedures followed for this project are accepted USEPA RM procedures and are defined in 40 CFR 60, Appendix A. **Table 2-1** provides a test matrix for the source tested and includes the test parameter, methods followed, number of sample runs, and run duration. The test matrix shown in **Table 2-1** is based on the performance test requirements of the CISWI rule for small remote incinerators (see 40 CFR 60 Subpart CCCC, Table 8).

Source	Test	Test	Method	Number	Minimum Run
ID	Type	Parameter		of Runs	Duration
Unit 412	Performance	Sample Points	RM1	1	NA
Incinerator	Test	Velocity	RM2	12	60 min
		Molecular Weight (O ₂ & CO ₂)	RM3A	12	NA
		Moisture	RM4	12	60 min
		Particulate	RM5	4	60 min
		Sulfur Dioxide	RM6C	10	60 min
		Nitrogen Oxides	RM7E	10	60 min
		Carbon Monoxide	RM10	10	60 min
		Visual Smoke Observations	RM 22	3	60 min
		Dioxin/Furan	RM 23	4	120 min
		Hydrochloric Acid	RM 26A	4	60 min
		Metals (Cd, Pb, Hg)	RM 29	4	120 min

Pogo submitted a test plan to the USEPA with a copy to Robin Wagner, ADEC. The test plan included a description of the methods and procedures to be used for sampling, QA/QC activities implemented, how the source was to be operated during the test, and how Pogo was to document that operation.

The field program was performed on September 28 through October 3, 2013. On Day 1 of the field effort, AECOM prepared the equipment for testing. Days 2 through 5 entailed the performance of four combined PM and HCl sample runs, four metals (Cd, Pb, Hg) sample runs, four D/F sample runs, and 10 combined NO_x , SO_2 , CO, O_2 , and CO_2 sample runs. On Day 6 demobilization of the equipment and field crew, as well as, sample shipping occurred.

2.1 Equipment Preparation

All equipment was prepared and calibrated in accordance with USEPA's Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III; Stationary Source Specific Methods, 40 CFR 60, Appendix A; and AECOM's general QA/QC policy described in Chapter 5.0 of this report. These procedures meet or exceed all USEPA requirements and guidelines for equipment maintenance and calibration. All equipment was in proper working order prior during the test program.

2.2 Summary of Field Measurements

The Unit 412 incinerator test program was performed according to approved USEPA methods. The methods selected and listed in **Table 2-1** above are applicable for the determination of the pollutant parameters required by the CISWI Rule. The field measurements results, presented in the following tables, are provided in the same engineering units as the CISWI Rule emission standards to facilitate the evaluation of compliance status and determine if pollution control is necessary.

The PM/HCl, metals (Cd, Pb, Hg) and D/F samples were withdrawn isokinetically from the source and collected on the front-half and condensate portions of the sample train. The sample volumes collected during each run are specific to the pollutant parameter and dictated by the CISWI Rule. A total of four, with a minimum run time of 72-minutes, sample runs were performed for combined PM/HCl. A total of four, with sample run times of 120-minutes or greater, sample runs were performed for metals (Cd, Pb, Hg). A total of four, with run times of 120-minutes or greater, sample runs were performed for D/F.

The gaseous pollutant (SO_2 , NO_x , CO) and diluents (O_2 and CO_2) parameters were measured with a CEMS. A total of 10, with 9 of them being 60-minutes or greater, sample runs were performed. Only one, 50-minute, sample run was performed on October 2 due to a failure of the permeation dryer which is the mechanism that removes moisture from the sample gas. The responses of the CEMS instruments were digitally recorded, at 1-minute intervals, using a Campbell Data Acquisition System (DAS). The CEMS' were calibrated with certified Protocol 1 calibration gas standards.

2.3 Particulate and Hydrogen Chloride Results

The particulate and HCl samples were collected simultaneously following RM 5 and RM 26A which were combined as allowed by the methods procedures. One sample was collected each of four consecutive test days. A total of 12 traverse points, each point sampled twice, through one test port, were used for each sample run. The particulate gravimetric analysis and HCl ion chromatography analysis were performed by TestAmerica located in West Sacramento, California. The particulate and HCl sample results are provided in **Table 2-2**. The table presents the recorded measured effluent parameters, calculated effluent volumetric flow rates, particulate results and HCl results.

The acetone blank residue mass is 1.4 milligrams (mg) which was subtracted from each sample's acetone residue results. The particulate concentration (milligrams per dry standard cubic meter [mg/dscm] @ 7% O_2) ranged from 56.37 mg/dscm @ 7% O_2 for Run I5-2 to 127.73 mg/dscm @ 7 % O_2 for Run I5-4. The average particulate concentration, of the first three sample runs, is 72.87 mg/dscm @ 7% O_2 .

The HCl blank residue concentration results were below the detection limit; therefore, no HCl blank corrections were performed on the HCl sample results. The HCl concentration (parts per million by volume [ppmv] @ 7% O₂) ranged from 136 ppmv @ 7% O₂ for Run I5-2 to 342 ppmv @ 7% O₂ for Run I5-4. The average HCl concentration, of the first three sample runs, is 155 ppmv @ 7% O₂.

Table 2-2 Pogo's Unit 412 Particulate and Hydrogen Chloride Results

Toot	15.4	15-2	15-3	15-4	
Test	l5-1 09/29/13			10/02/13	Avorago *
Parameters		09/30/13 1251-1410	10/01/13	1510-1629	Average *
	1106-1242	1231-1410	1506-1626	1510-1629	(Run 1-3)
Sample Time (min)	81	79	80	79	80
Vol meter (acf)	60.407	57.485	58.110	55.557	58.667
Ave. SQRT dP (in WC)1/2	0.102	0.100	0.100	0.100	0.101
` ,					
dH (in WC)	1.71	1.63	1.63	1.57	1.66
T stack (F)	1151.1	1148.4	1146.6	1206.2	1148.7
T meter (F)	60.3	68.7	65.3	88.1	64.8
P static (in WC)	0.04	0.04	0.04	0.04	0.04
P bar (in Hg)	28.00	28.25	28.40	28.45	28.22
P stack (in WC)	28.00	28.25	28.40	28.45	28.22
H2O Mass Gain (g)	139.00	126.80	132.00	145.00	132.60
Yd (meter coef.)	1.003	1.003	1.003	1.003	1.003
dH @ (in WC)	1.773	1.773	1.773	1.773	1.77
Cp (pitot coef.)	0.84	0.84	0.84	0.84	0.84
Dia stack (in)	30.0	30.0	30.0	30.0	30.0
Dia nozzle (in)	0.875	0.875	0.875	0.875	0.875
CO ₂ (%)	7.51	7.85	7.14	7.40	7.50
O ₂ (%)	10.71	10.39	11.21	11.10	10.77
Vol meter (std) (dscf)	57.797	54.598	55.846	51.252	56.080
Vol meter (std) (dscm)	1.64	1.55	1.58	1.45	1.59
Md (lb/lb-mole)	29.63	29.67	29.59	29.63	29.63
Ms (lb/lb-mole)	28.45	28.52	28.43	28.26	28.47
Vwc	6.54	5.97	6.21	6.83	6.24
H ₂ O (%)	10.2	9.9	10.0	11.8	10.0
ISO (%)	99.0	97.4	98.1	94.3	98.2
	Flow R	Rate			
Velocity (ft/s)	10.5	10.1	10.1	10.3	10.2
Vol. Flow Rate (acfm)	3,079	2,988	2,983	3,045	3,017
Vol. Flow Rate (wscfm)	944	926	931	917	934
Vol. Flow Rate (dscfm)	848	835	838	810	840
Fi	Iterable Partic	ulate Results			
Filter Mass Gain (mg)	23.5	14.1	16.5	39.9	18.0
Acetone Rinse Mass Gain (mg)	82.0	53.2	68.1	92.2	67.8
Acetone Blank Mass Gain (mg)	1.4	1.4	1.4	1.4	1.4
Filterable Particulate Mass Gain (mg)	104.1	65.9	83.2	130.7	84.4
Particulate Concentration (lb/dscf)	3.97E-06	2.66E-06	3.28E-06	5.62E-06	3.31E-06
Particulate Concentration (gr/dscf)	0.0278	0.0186	0.0230	0.0394	0.0231
Particulate Concentration (mg/dscm)	63.61	42.63	52.61	90.06	52.95
Particulate Conc. (mg/dscm @ 7% O ₂)	86.77	56.37	75.47	127.73	72.87
Particulate Emission Rate (lb/hr)	0.20	0.13	0.17	0.27	0.17
	Hydrochloric A	cid Results			
l					
HCI Mass (mg)	350	240	230	530	273
HCI Concentration (lb/dscf)	1.34E-05	9.69E-06	9.08E-06	2.28E-05	1.07E-05
HCI Concentrtion (ppmv)	141	102	96	241	113
HCl Concentration (ppmv) @ 7% O2	193	136	138	342	155
HCI Emission Rate (lb/hr)	0.68	0.49	0.46	1.11	0.54
* Avarage regulte are based on the first thr					

^{*} Average results are based on the first three runs of the sample series.

2.4 Cadmium, Lead, and Mercury Results

The Cd, Pb, and Hg samples were collected simultaneously following RM 29. The first sample run was abbreviated, due to the quartz nozzle breaking due to cooling while moving from one sample port to the other sample port. The USEPA's, Mr. Zach Hedgepeth, observed the test and determined that the abbreviated first run should be considered a valid run. The second through fourth sample runs were approximately 127-minutes in duration for the following test days. A total of 12 traverse points, each point sampled twice, through one test port were used for second through fourth sample runs. The metals analysis was performed by TestAmerica located in West Sacramento, California. The Cd, Pb, and Hg sample results are provided in **Table 2-3**. The table presents the individual and average (for the first three runs) recorded, measured effluent parameters, calculated effluent volumetric flow rates, and metals results.

The Cd, Pb, and Hg blank residue concentration results are 0.06 microgram per sample (μ g/sample), 8.5 ug/sample, and 0.051 μ g/sample, respectively. The Cd, Pb, and Hg blank residue mass was subtracted from each sample's results.

The cadmium concentration (mg/dscm @ 7% O₂) results for each of the three sample runs ranged from 0.01 mg/dscm @ 7% O₂ for Run 129-1 to 0.0051 mg/dscm @ 7% O₂ for Run 129-2. The average cadmium concentration, of the first three sample runs, is 0.01 mg/dscm @ 7% O₂.

The lead concentration (mg/dscm @ 7% O₂) ranged from 0.10 mg/dscm @ 7% O₂ for Run I29-1 to 0.51 mg/dscm @ 7% O₂ for Run I29-2. The average lead concentration, of the first three sample runs, is 0.28 mg/dscm @ 7% O₂.

The mercury concentration (mg/dscm @ 7% O₂) ranged from 0.0002 mg/dscm @ 7% O₂ for Runs I29-3 and I29-4 to 0.0023 mg/dscm @ 7% O₂ for Run I29-1. The average mercury concentration, of the first three sample runs, is 0.0011 mg/dscm @ 7% O₂.

2.5 Dioxin and Furan Results

The dioxin and furan samples were collected according to the procedures of RM 23. One sample run was performed during each of four consecutive test days. The four sample runs performed were 127 minutes in duration. A total of 12 traverse points, each point sampled twice, through one test port were used for each sample run. Two sample fractions (front half and back half) were submitted to and analyzed by Analytical Perspectives of Wilmington, North Carolina. Each front half sample was composed of a probe wash and filter. Each back half sample included rinses and XAD-2 resin trap.

Included in **Table 2-4** are the individual and average (for the first three runs) recorded dioxin and furan test parameters such as stack temperature, meter temperature, pressure, etc. Also included in this table are calculations of effluent molecular weight (wet and dry), moisture content, and isokinetics. In addition, the calculated effluent volumetric flow rates are provided.

The dioxin and furan results are provided in terms of toxicity equivalence (TEQ) concentration (nano grams per cubic meter [TEQ ng/m 3], and TEQ concentration nano-grams per cubic meter corrected to 7% oxygen [TEQ ng/m 3 at 7% O $_2$] and TEQ emission rate (nano-grams per second [ng/s]).

Table 2-5 presents the total dioxin and furan results of the four sample runs and average of the first three sample runs. The total dioxin and furan concentration ranged from 0.0928 TEQ ng/m^3 at 7% O_2 for Run I23-4 to 0.2670 TEQ ng/m^3 @ 7% O_2 for Run I23-2. The average dioxin and furan concentration, of the first three sample runs, is 0.0011 mg/dscm @ 7% O_2 .

Table 2-3 Pogo's Unit 412 Cadmium, Lead, and Mercury Results

Test	I29-1	129-2	129-3	129-4	
Parameters	09/29/13	09/30/13	10/01/13	10/02/13	Average *
	1406-1506	1505-1712	0859-1106	0845-1052	(Run 1-3)
Sample Time (min)	60	127	127	127	105
Vol meter (acf)	43.625	92.412	91.847	90.120	75.961
Ave. SQRT dP (in WC)1/2	0.10	0.10	0.10	0.10	0.10
dH (in WC)	1.63	1.63	1.63	1.65	1.63
T stack (F)	1144.6	1143.7	1145.1	1127.1	1144.5
T meter (F)	70.2	69.9	62.5	49.1	67.6
P static (in WC)	0.04	0.04	0.04	0.04	0.04
P bar (in Hg)	28.00	28.25	28.40	28.45	28.22
P stack (in WC)	28.00	28.25	28.40	28.45	28.22
H ₂ O Mass Gain (g)	126.10	206.80	198.70	190.60	177.20
Yd (meter coef.)	1.003	1.003	1.003	1.003	1.003
dH @ (in WC)	1.773	1.773	1.773	1.773	1.773
Cp (pitot coef.)	0.84	0.84	0.84	0.84	0.84
Dia stack (in)	30.0	30.0	30.0	30.0	30.0
Dia nozzle (in)	0.874	0.875	0.875	0.875	0.875
CO ₂ (%)	7.98	7.80	7.31	6.97	7.70
O ₂ (%)	10.25	10.31	10.91	11.27	10.49
Vol meter (dscf)	40.952	87.569	88.730	89.527	72.417
Vol meter (dscm)	1.16	2.48	2.51	2.54	2.05
Md (lb/lb-mole)	29.69	29.66	29.61	29.57	29.65
Ms (lb/lb-mole)	28.21	28.49	28.50	28.51	28.40
Vwc	5.94	9.73	9.35	8.97	8.34
H ₂ O (%)	12.7	10.0	9.5	9.1	10.7
ISO (%)	99.2	97.2	97.7	97.5	98.0
Velocity (ft/s)	10.2	Flow Rate 10.1	10.1	10.0	10.2
Vol. Flow Rate (acfm)	3,014	2,985	2,978	2,958	2,993
Vol. Flow Rate (acm) Vol. Flow Rate (wscfm)	928	928	930	936	2,993 929
Vol. Flow Rate (wsciii)	811	835	841	851	829
voi. Flow reace (assum)		etals Results	0+1	001	020
Cd Mass (ug)	9.0	13.0	9.3	9.9	10.4
Cd Blank (ug)	0.060	0.060	0.060	0.060	0.060
Cd Blank Corrected mass (ug)	8.94	12.94	9.24	9.84	10.37
Cd Concentration (ug/dscm)	7.71	5.22	3.68	3.88	5.53
Cd Concentration (mg/dscm @ 7% O ₂)	0.0101	0.0068	0.0051	0.0056	0.0073
Cd Concentration (lb/dscf)	4.15E-10	1.31E-10	9.14E-11	9.56E-11	2.13E-10
Cd Emission Rate (lb/hr)	2.02E-05	6.58E-06	4.61E-06	4.88E-06	1.05E-05
Pb Mass (ug)	97.0	980.0	410.0	360.0	495.7
Pb Blank (ug)	8.50	8.50	8.50	8.50	8.500
Pb Blank Corrected Mass (ug)	88.5	971.5	401.5	351.5	487.17
Pb Concentration (ug/dscm) Pb Concentration (mg/dscm @ 7% O ₂)	76.3	391.8	159.8	138.6	209.30
Pb Concentration (lb/dscf)	0.0996	0.5142	0.2223	0.2001	0.2787
Pb Concentration (lb/dscr) Pb Emission Rate (lb/hr)	4.11E-09 0.0002	9.86E-09 0.0005	3.97E-09 0.0002	3.41E-09	5.98E-09 0.0003
FD EITHSSION Rate (ID/III)	0.0002	0.0003	0.0002	0.0002	0.0003
Hg Empty Mass (ug)	ND	0.08	ND	ND	0.08
Hg Front Half (ug)	0.65	0.17	0.20	0.13	0.34
Hg HCI (ug)	0.59	0.25	0.28	0.34	0.37
Hg KMnO4 (ug)	ND	ND	ND	ND	0.00
Hg H2O2 (ug)	0.87	1.20	ND	ND	1.04
Hg Blank Sum (ug)	0.051	0.051	0.051	0.051	0.051
Hg Blank Corrected Mass (ug)	2.06	1.65	0.43	0.42	1.38
Hg Concentration (ug/dscm)	1.78	0.66	0.17	0.17	0.87
Hg Concentration (mg/dscm @ 7% O ₂)	0.0023	0.0009	0.0002	0.0002	0.0011
Hg Concentration (lb/dscf)	1.11E-10	4.14E-11	1.07E-11	1.03E-11	5.43E-11
	•				

[#] Average results are based on the first three runs of the sample series.

Table 2-4 Pogo's Unit 412 Average Measured Test Parameters

Test Parameters	123-1 09/29/13 1722-1929	123-2 09/30/13 0923-1130	I23-3 10/01/13 1159-1406	123-4 10/02/13 1157-1404	Average * (Run 1-3)
	407	407	407	407	407
Sample Time (min)	127	127	127	127	127
Vol meter (acf)	92.252	90.889	90.196	89.285	91.112
Ave. SQRT dP (in WC)1/2	0.100	0.100	0.100	0.100	0.100
dH (in WC)	1.64	1.64	1.62	1.57	1.63
T stack (F)	1136.9	1135.8	1162.7	1223.8	1145.1
T meter (F)	62.8	55.7	65.2	73.3	61.2
P static (in WC)	0.04	0.04	0.04	0.04	0.04
P bar (in Hg)	28.05	28.20	28.40	28.45	28.22
P stack (in WC)	28.05	28.20	28.40	28.45	28.22
H2O Mass Gain (g)	225.50	214.20	212.10	244.20	217.27
Yd (meter coef.)	1.003	1.003	1.003	1.003	1.003
dH @ (in WC)	1.773	1.773	1.773	1.773	1.77
Cp (pitot coef.)	0.84	0.84	0.84	0.84	0.84
Dia stack (in)	30.0	30.0	30.0	30.0	30.0
Dia nozzle (in)	0.875	0.875	0.875	0.875	0.875
CO ₂ (%)	7.45	8.11	7.83	7.10	7.80
O ₂ (%)	10.83	9.64	10.47	11.20	10.31
Vol meter (std) (dscf)	87.977	88.342	86.697	84.651	87.672
Vol meter (std) (dscm)	2.49	2.50	2.45	2.40	2.48
Md (lb/lb-mole)	29.63	29.68	29.67	29.58	29.66
Ms (lb/lb-mole)	28.37	28.49	28.47	28.20	28.44
Vwc	10.61	10.08	9.98	11.49	10.23
H ₂ O (%)	10.8	10.2	10.3	12.0	10.4
ISO (%)	98.4	98.1	96.8	97.5	97.8
	Flow F	Rate			
Velocity (ft/s)	10.2	10.1	10.2	10.4	10.2
Vol. Flow Rate (acfm)	2,996	2,981	2,996	3,064	2,991
Vol. Flow Rate (wscfm)	929	930	926	914	928
Vol. Flow Rate (dscfm)	829	834	830	804	831

^{*} Average results are based on the first three runs of the sample series.

Table 2-5 Pogo's Unit 412 Dioxin and Furan Results

	D No		20.4		00.0	Π.	00.0	Γ.	00.4			
	Run No.		23-1 /29/13		23-2		23-3 /01/13		23-4	۸۰۰۰	rogo *	
	Date Time		2-1929		09/30/13 0923-1130		1159-1406		10/02/13 1157-1404		rage *	
Sample Volume	dscf	172	87.977	092	88.342	110	86.697	113	84.651	(170	un 1-3) 87.672	
Sample Volume	m³		2.49		2.50		2.46		2.40		2.48	
Moisture Content	% v/v		10.8		10.2		10.3		12.0		10.4	
O ₂ Concentration	% v/v % v/v (dry)		10.83		9.64		10.47		11.20		10.4	
CO ₂ Concentration	% v/v (dry)		7.45		8.11		7.83		7.10		7.80	
Isokinetics	%		98		98		97		98		98	
Stack Flow rate	dscfm		829		834		830		804		831	
	dooniii											
PCDD / PCDF Parameters	TEF (a)	pg	ng/m³ TEQ	pg	ng/m³ TEQ	pg	ng/m³ TEQ	pg	ng/m³ TEQ	pg	ng/m³ TEQ	
Tarancicis	1Ει (α)		TEQ		TEQ		TEQ		ILQ		ILQ	
2,3,7,8-TCDD	1.00	2.34	9.4E-04	12.2	4.9E-03	6.58	2.7E-03	6.42	2.7E-03	7.04	2.8E-03	
1,2,3,7,8-PeCDD	0.50	6.45	1.3E-03	86.3	1.7E-02	25.8	5.3E-03	21.5	4.5E-03	39.5	7.9E-03	
1,2,3,4,7,8-HxCDD	0.10	13	5.2E-04	148	5.9E-03	29.9	1.2E-03	25.9	1.1E-03	63.6	2.6E-03	
1,2,3,6,7,8-HxCDD	0.10	33.9	1.4E-03	209	8.4E-03	69.1	2.8E-03	40.9	1.7E-03	104.0	4.2E-03	
1,2,3,7,8,9-HxCDD	0.10	18.9	7.6E-04	166	6.6E-03	44.6	1.8E-03	30.4	1.3E-03	76.5	3.1E-03	
1,2,3,4,6,7,8-HpCDD	0.01	316	1.3E-03	1,670	6.7E-03	750	3.1E-03	395	1.6E-03	912	3.7E-03	
OCDD	0.001	546	2.2E-04	2,600	1.0E-03	1,640	6.7E-04	989	4.1E-04	1,595	6.4E-04	
_2,3,7,8-TCDF	0.10	21.5	8.6E-04	107	4.3E-03	39.4	1.6E-03	40.2	1.7E-03	56	2.2E-03	
1,2,3,7,8-PeCDF	0.05	18	3.6E-04	166	3.3E-03	72.6	1.5E-03	61.6	1.3E-03	85.5	1.7E-03	
2,3,4,7,8-PeCDF	0.50	50	1.0E-02	450	9.0E-02	151	3.1E-02	125	2.6E-02	217	4.4E-02	
1,2,3,4,7,8-HxCDF	0.10	33.4	1.3E-03	327	1.3E-02	146	5.9E-03	113	4.7E-03	169	6.8E-03	
1,2,3,6,7,8-HxCDF	0.10	29.2	1.2E-03	368	1.5E-02	182	7.4E-03	123	5.1E-03	193	7.8E-03	
2,3,4,6,7,8-HxCDF	0.10	54.3	2.2E-03	830	3.3E-02	372	1.5E-02	235	9.8E-03	419	1.7E-02	
1,2,3,7,8,9-HxCDF	0.10	(1.71)	0.0E+00	(4.95)	0.0E+00	(4.76)	0.0E+00	(4.22)	0.0E+00	-3.81	0.0E+00	
1,2,3,4,6,7,8-HpCDF	0.01	143	5.7E-04	1,630	6.5E-03	871	3.5E-03	574	2.4E-03	881	3.5E-03	
1,2,3,4,7,8,9-HpCDF	0.01	27.6	1.1E-04	173	6.9E-04	199	8.1 <u>E</u> -04	102	4.3E-04	133	5. <u>4E-04</u>	
OCDF	0.001	142	5.7E-05	546	2.2E-04	961	3.9E-04	462	1.9E-04	550	2.2E-04	
TOTAL TEQs (ng/m	13)	=	0.0231		0.2167		0.0846		0.0650		0.1081	
TOTAL TEQs (ng/m	³ @ 7% O ₂)	=	0.0317		0.2670]	0.1125		0.0928		0.1371	
TOTAL TEQs (ng/s))		0.0090		0.0853		0.0331		0.0247		0.0425	

⁽a) U.S.EPA (1989) Toxic Equivalency Factor (TEF)

Note: Results below the detection limit are listed as the reporting limit, shown in parentheses, and treated as zero in the calculation of concentration on a TEQ basis.

EMPC - IF a result was reported as an Estimated Maximum Possible Concentration (EMPC), the EMPC result is reported as the actual conentration.

2.6 Continuous Emission Monitor Results

Ten continuous emission monitor sample runs were performed at the Unit 412 exhaust stack test location over a four day period. Each CEMS sample run included the measurements of gaseous pollutant (SO₂, NO_x, CO) and diluents (O₂ and CO₂) parameters. Prior to the initiation of the CEMS measurements, the CEMS was calibrated with USEPA Protocol 1 calibration gas standards following RMs 3A, 6C, 7E and 10. A calibration bias check of the CEMS was performed prior to the initiation and upon completion of each sample run. The CEMS response was digitally recorded and averaged at 1-minute intervals. The 1-minute data averages were used to calculate sample run averages.

As noted above, the CEMS permeation dryer, which removes moisture from the sample gas, failed 50 minutes into the first sample run (Run I29-4) performed on October 2. Therefore, no CEMS measurements could be conducted during the second (Run I23-4) and third (Run I5-4) sample runs performed that day. However, bag samples were collected during the sample runs on October 2 and subjected to the O_2 and CO_2 analyzers for the determination of sample gas molecular weight. **Table 2-6** presents the results of the CEMS sample runs. The results are presented in terms of concentration (ppmv and ppmv at 7% O_2) and emission rate (pound per hour [lb/hr]). The emission rate results provided in the table were calculated using the volumetric flow rate recorded by the corresponding isokinetic sample run conducted simultaneously with the CEMS sample run.

Table 2-6 Pogo's Unit 412 Continuous Emission Monitor System

Date	Time	Run	Flow Rate	O ₂	CO ₂		NO _x			СО			SO ₂			
		ID	(dscfm)	(%)	(%)	(ppm)	(ppm @ 7% Q ₂)	(lb/hr)	(ppm)	(ppm @ 7% Q)	(lb/hr)	(ppm)	(ppm @ 7% Q ₂)	(lb/hr)		
09/29/13	1106-1242	I5-1	848	10.71	7.51	71.2	97.1	0.43	0.5	0.7	0.00	18.5	25.2	0.16		
09/29/13	1406-1506	129-1	811	10.25	7.98	71.7	93.5	0.42	0.0	0.0	0.00	31.6	41.2	0.26		
09/29/13	1722-1929	123-1	829	10.83	7.45	64.1	88.5	0.38	0.1	0.2	0.00	28.2	39.0	0.23		
Average			829	10.59	7.65	69.0	93.0	0.41	0.2	0.3	0.00	26.1	35.1	0.22		
09/30/13	0923-1129	123-2	834	9.64	8.11	58.7	72.5	0.35	3.6	4.4	0.01	17.5	21.5	0.15		
09/30/13	1251-1410	15-2	835	10.39	7.85	64.5	85.3	0.39	0.0	0.0	0.00	26.1	34.6	0.22		
09/30/13	1506-1712	129-2	835	10.31	7.80	60.8	79.7	0.36	0.0	0.0	0.00	26.1	34.2	0.22		
Average			835	10.11	7.92	61.3	79.2	0.37	1.2	1.5	0.00	23.2	30.1	0.19		
10/01/13	0859-1106	129-3	841	10.91	7.31	64.7	90.1	0.39	0.2	0.3	0.00	13.5	18.8	0.11		
10/01/13	1159-1406	123-3	830	10.47	7.83	61.0	81.3	0.36	0.0	0.0	0.00	19.4	25.8	0.16		
10/01/13	1506-1626	15-3	838	11.21	7.14	61.9	88.8	0.37	1.3	1.9	0.00	10.3	14.7	0.09		
Average			836	10.86	7.43	62.5	86.7	0.38	0.5	0.7	0.00	14.4	19.8	0.12		
10/02/13	0845-0938	129-4	851	11.27	6.97	55.0	79.4	0.34	2.3	3.3	0.01	9.5	13.7	0.08		
10/02/13	1157-1404	I23-4 *	804	11.20	7.10	NA	NA	NA	NA	NA	NA	NA	NA	NA		
10/02/13	1510-1629	I5-4 *	810	11.10	7.40	NA	NA	NA	NA	NA	NA	NA	NA	NA		
Average			822	11.19	7.16	55.0	79.4	0.34	2.3	3.3	0.01	9.5	13.7	0.08		
Average Ru	uns 09/29/13	-10/01/1	831	10.66	7.56	63.6	85.8	0.38	0.8	1.0	0.00	20.3	27.2	0.17		

2.7 Visual Determination of Smoke Emissions Results

Visual determinations of smoke emissions from Unit 412 were conducted according to RM 22. A total of three observation periods of 60 minutes each were performed. The observations were performed simultaneously with particulate, metals, and D/F sample runs. **Table 2-7** presents the results of the visual observations. The emission frequency resulted in zero percent for all three observation periods.

Table 2-7 Pogo's Unit 412 Visual Determination of Smoke Results

Date	Time	Run	Accumulated Emission Time	Observation Period	Emission Frequency	
		ID	(seconds)	(seconds)	(%)	
09/30/13	1252-1352	15-2	0	3,600	0.0	
10/01/13	0910-1010	129-3	0	3,600	0.0	
10/01/13	1208-1308	123-3	0	3,600	0.0	
Average			0	3,600	0.0	

3.0 Process Description and Operation

3.1 Process Description

Unit 412 is an ACS, Inc., Model CA 400, solid waste incinerator used to reduce the amount of non-hazardous waste transported off site from the Pogo facility. The unit is fired by propane. The incinerator is equipped with one primary-chamber burner rated at 0.8 MMBtu/hr and two secondary-chamber burners each rated at 0.8 million British thermal units per hour (MMBtu/hr). The waste loading/burning capacity is an operating limit to be established during this performance test. A separate report describing the site-specific operating limits established during the test will be submitted separately.

3.2 Process Operation

The emission measurements of Unit 412 were conducted in accordance with the Test Plan and petition submitted by Pogo to the USEPA. For all measurements associated with Unit 412, all pertinent process and control device operations data were monitored and recorded. The following parameters were monitored and recorded during each sample run:

- Weight of each batch loaded into the incinerator;
- Weight of each of the 3 waste components (i.e., MSW, sludge, and adsorbs);
- Start time of each batch loaded;
- Time interval between batches loaded;
- Primary oven temperature at 5- minute intervals;
- Secondary oven temperature at 5 minute intervals;
- Primary oven burn time following loading of final batch; and
- Secondary burn time following completion of the primary burn cycle.

Table 3-1 presents a summary of the process parameters recorded during the measurements program. Included in the table is the date, time, and associated run identification (ID) of the process data collected. For each sample run, the average primary and secondary temperature (F) is listed. In addition, the total weight (Ib) of each charge type and total charge weight (Ib) are presented. The actual process operations data for the time periods during which testing was conducted are provided in **Appendix D** of this test report.

Table 3-1 Pogo's Unit 412 Summary of Process Operations

		Run	Average	Average	Type 2	Type 3			Total
Date	Time	ID	Primary	Secondary	Waste	Waste	Sludge	Adsorbs	Charge
			(F)	(F)	(lb)	(lb)	(lb)	(lb)	(lb)
9/29/2013	1106-1242	I5-1	1,471	1,827	84	50	29	29	192
9/29/2013	1406-1508	I29-1	1,525	1,826	44	28	128	33	233
9/29/2013	1721-1929	I23-1	1,453	1,828	52	21	200	61	334
9/30/2013	0923-1129	123-2	1,369	1,812	71	132	88	80	371
9/30/2013	1251-1410	I5-2	1,480	1,827	20	24	114	53	211
9/30/2013	1505-1712	129-2	1,542	1,826	13	118	116	118	365
10/1/2013	0858-1155	129-3	1,358	1,825	133	183	30	24	370
10/1/2013	1158-1405	I23-3	1,518	1,826	70	204	56	80	410
10/1/2013	1505-1625	I5-3	1,475	1,828	72	101	29	21	223
10/2/2013	0846-1053	I29-4	1377	1825	205	180	0	0	385
10/2/2013	1157-1404	I23-4	1460	1825	166	221	0	0	387
10/2/2013	1511-1630	I5-4	1398	1757	100	140	0	0	240

4.0 Methodology

The testing program was performed according to the following accepted and approved USEPA RMs as contained in the USEPA's Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III, Stationary Source Specific Methods, 40 CFR 60, Appendix A. The general procedures that were followed for this measurements evaluation included:

- RM 1 Sample Velocity Traverse for Stationary Sources;
- RM 2 Determination of Stack Gas Velocity and Volumetric Flow Rate (Type-S Pitot Tube);
- RM 3A Determination of Oxygen and Carbon Dioxide Concentrations in Emissions from Stationary Sources (Instrumental Analyzer Procedure);
- RM 4 Determination of Moisture Content In Stack Gases:
- RM 5 Determination of Particulate Matter Emissions from Stationary Sources;
- RM 6C Determination of Sulfur Dioxide Emissions from Stationary Sources (Instrumental Analyzer Procedure);
- RM 7E Determination of Nitrogen Oxides Emissions from Stationary Sources (Instrumental Analyzer Procedure);
- RM 10 Determination of Carbon Monoxide Emissions from Stationary Sources;
- RM 22 Visual Determination of Fugitive Emissions from Material Sources and Smoke Emissions from Flares
- RM 023 Determination of Polychlorinated Dibenzo-p-dioxin and Polychlorinated Dibenzofuran Emissions from Municipal Waste Combustors;
- RM 26A Determination of Hydrogen Halide and Halogen Emissions from Stationary Sources Isokinetic Method; and
- RM 29 Determination of Metals Emissions from Stationary Sources.

4.1 Support Measurements for Stack Parameters

USEPA RMs 1 through 4 were performed in support of the emissions measurements procedures selected for quantifying pollutant emission rates. RM 1, selection of sample points for velocity and particulate traverses, was conducted prior to the initiation of any emission measurements at the test location. The determination of stack gas flow rate, molecular weight, and moisture content (RMs 2 through 4) were integrated into and performed concurrently with each isokinetic sample run.

4.1.1 Selection of Traverse Points by Reference Method 1

USEPA RM 1, "Sample Velocity Traverses for Stationary Sources," was followed for the selection of measurement points at the test location. The physical characteristics of the test location meet the minimum criteria of RM 1 for isokinetic sampling. The calculated measurement points were used for all isokinetic sample runs. A copy of the RM 1 data form completed prior to sampling is located in **Appendix A** of this report.

4.1.2 Flow Rate Determination by Reference Method 2

USEPA RM 2, "Determination of Stack Gas Velocity and Volumetric Flow Rate (Type-S Pitot Tube)," was followed to measure the volumetric flow rate during each sample run at the sample location. This method was incorporated into, and conducted concurrently with, each isokinetic sample run.

RM 2 allows for a stainless steel Type-S or standard pitot tube to be connected to a differential pressure gauge (inclined manometer). The measured pressure differential, observed at each traverse point, was recorded on field data forms and used in determining the overall emission rate for each constituent.

In addition to velocity pressures, gas temperatures were measured and recorded concurrently with all differential pressure data. The temperature was measured with a Type K thermocouple located at the measurement tip of the pitot tube (in the same measurement plane). The Type K thermocouple was connected directly to a calibrated digital temperature indicator for accurate measurements.

4.1.3 Molecular Weight Determination by Reference Method 3

USEPA RM 3A, "Determination of Oxygen and Carbon Dioxide Concentrations in Emissions from Stationary Sources (Instrumental Analyzer Procedure)," was conducted concurrently with the pollutant measurements at the test location. During the first sample day, integrated gas samples were collected in Tedlar bags and subjected to a combination O_2/CO_2 analyzer. During the second and third sample days, sample gas was continuously extracted from the Unit 412 exhaust stack and directed to a combination O_2/CO_2 analyzer. Diluent O_2 and CO_2 data collected during the course of the sampling was used to determine effluent gas dry molecular weight in accordance with USEPA RM 3A. The results of the O_2 and CO_2 analysis were used for the determination of effluent molecular weight.

USEPA RM 3A analyzer calibration requirements include three point calibrations using USEPA Protocol 1 gas standards, and stringent instrument drift requirements. Calibrations will be completed at 80 to 100 percent of the full span value, 40 to 60 percent of the full span value, and 0 percent of the full span value (ultra-pure nitrogen for both analyzers).

The O_2/CO_2 analyzer was subjected to a zero and two up-scale calibration gases prior to and upon completion of the sample runs when they were used continuously. The gas standards were certified and traceable to USEPA Protocol 1 specifications, which require that the gas concentration be within ± 1 percent of the documented value. The response of the analyzers compared to each certified calibration standard must be within ± 2 percent of the high calibration gas standard (CS) value for each component as required by the method.

To calibrate the instruments, the gas standards were introduced directly to the monitors at the sample inlet located on the back of each instrument. For the continuous measurements, the amount of bias of the O_2/CO_2 instrument also was determined. This was accomplished by introducing zero and one span gas to the instrument at the point at which the sample probe and heated sample filter are connected. The response of the analyzers to the direct zero and span gases (bias check) must be less than ± 5 percent of the span value for each component as required by the method. The bias calibration check was performed prior to and upon completion of each sample run.

The magnitude of calibration drift was calculated for each continuous sample run. Calibration drift is the difference in the initial (pre-test) bias calibration response and the final (post-test) bias calibration response for the same gas standard. The calibration drift must be within ±3 percent of the CS over each sample run for each O₂/CO₂ gas standard as required by RM 3A.

4.1.4 Percent Moisture Determination by Reference Method 4

USEPA RM 4, "Determination of Moisture Content in Stack Gases," was incorporated into each isokinetic sample run. The determination of moisture content was accomplished by using a condenser and pump assembly, connected between a sample probe and metering system and performed concurrently with each sample run.

Throughout each isokinetic sample run, a known volume of gas (measured by a dry gas meter) was passed through the condenser assembly. Upon completion of each sample run, the total amount of condensate collected was gravimetrically measured and the net gain calculated. The total moisture gain,

volume of gas extracted, and measured meter temperature data were used to calculate the actual moisture content of the effluent.

4.2 Particulate Determination by Reference Method 5

USEPA RM 5, "Determination of Particulate Matter Emissions from Stationary Sources" was followed to determine particulate emission rates. Each RM 5 was conducted in accordance with all applicable USEPA quality assurance requirements

Samples were withdrawn isokinetically (100 percent \pm 10 percent) from the source using a modular isokinetic sampling system. The sampling train consisted of a quartz glass nozzle and probe assembly, heated stainless steel probe with an S-Type pitot tube attached, a heated filter, four chilled impingers, and a metering console. The particulate sample was collected on a quartz fiber filter supported by a Teflon frit and maintained at a temperature of 248 \pm 25°F. The impinger train was consistent with RM 5.

The system vacuum was used to extract the effluent gas through the interconnected, leak-free components. The entire system was "leak checked" before and after each individual sample run to ensure sample integrity following RM 5 procedures.

A "K-factor" (coefficient) was determined prior to the initiation of each sample run. This coefficient was based upon preliminary measurements of gas temperature, flow rate, pressure, and moisture content. Multiplying the K-factor by the measured differential pressure was used to determine the isokinetic sample rate for each sample point. If a variable changed during a sample run, the coefficient was adjusted to maintain isokinetic sampling rates. At isokinetic conditions, the velocity of the stack gas entering the nozzle of the extraction system will be equal to the effluent velocity at the sample point.

The quartz filter was removed from the filter holder and placed in a Petri dish and sealed. The impingers were recovered following RM 5 procedures. The RM 5 sample recovery was conducted in accordance with all applicable USEPA quality assurance requirements.

4.3 Sulfur Dioxide Determination by Reference Method 6C

Sulfur dioxide emissions were quantified at the Unit 412 exhaust stack according to USEPA RM 6C, "Determination of Sulfur Dioxide Emissions from Stationary Sources (Instrumental Analyzer Procedure)." This method allows for the determination of SO_2 concentrations by continuously extracting stack effluent and directing a portion of the sample to an SO_2 analyzer. An AMETEK Model 921M UV photometric SO_2 monitor was used to measure the concentration (parts per million [ppm] by volume) of the effluent at the test location on a dry basis.

RM 6C provides rigorous analyzer calibration requirements, including three point calibrations using USEPA Protocol 1 gas standards, and stringent instrument drift requirements. Calibrations were performed at 80 to 100 percent of the span value, 40 to 60 percent of the span value, and 0 percent of the span value (ultra-pure nitrogen).

The SO_2 analyzer was subjected to the zero and two up-scale calibration gases prior to and upon completion of the test series. The gas standards were certified and traceable to USEPA Protocol 1 specifications, which require that the gas concentration be within ± 1 percent of the documented value. The response of the analyzer compared to each certified calibration standard must be within ± 2 percent of the CS value for each component. To calibrate the instrument, the gas standards were introduced to the inlet of the SO_2 RM analyzer before and upon completion of each test series. The amount of bias of the SO_2 RM system was determined before and after each sample run. This was accomplished by delivering zero and one span gas directly to the point where the sample probe and heated sample filter were connected. The response of the analyzer to the bias checks must be less than ± 5 percent of the span value for each check.

The magnitude of calibration drift also was calculated. Calibration drift is the difference in the initial bias calibration response check and the final bias calibration response check for the same gas standard. The calibration drift must be within ±3 percent of the span for each sample run.

4.4 Nitrogen Oxides Determination by Reference Method 7E

USEPA RM 7E, "Determination of Nitrogen Oxides Emissions from Stationary Sources (Instrumental Analyzer Procedure)," was used to accomplish the Unit 412 NO_X measurements. This method allows for the determination of NO_X concentrations by continuously extracting effluent from the stack and directing a portion of the sample to a NO_X analyzer. A TEI Model 42C Chemiluminescent NO_X analyzer was used to measure the concentration (ppm by volume) of the effluent at the stack on a dry basis.

USEPA RM 7E provides rigorous analyzer calibration requirements, including three point calibrations using USEPA Protocol 1 gas standards, and stringent instrument drift requirements. Calibrations were completed at 80 to 100 percent of the span value, 40 to 60 percent of the span value, and zero percent of the span value (ultra-pure nitrogen).

The NO_X analyzer was subjected to a zero and two up-scale calibration gases prior to the performance of the sample runs. The gas standards were certified and traceable to USEPA Protocol 1 specifications, which require that the gas concentration is within ± 1 percent of the documented value. The response of the analyzer compared to each certified calibration standard must be within ± 2 percent of the CS for each component.

To calibrate the instrument, the gas standards were introduced directly to the NO_X monitor at the sample inlet located on the back of the instrument. The amount of bias of the NO_X CEMS was determined. This was accomplished by introducing zero and one span gas to the NO_X system at the point in which the sample probe and heated sample filter were connected. The response of the analyzer system to the zero and span gas (bias check) must be less than ± 5 percent of the CS for each component. The bias calibration check was performed prior to, and upon completion of, each sample run

The magnitude of calibration drift also was calculated. Calibration drift is the difference in the initial (pre-test) bias calibration response and the final (post-test) bias calibration response for the same gas standard. The calibration drift must be within ±3 percent of the CS each sample run for each gas standard.

4.5 Carbon Monoxide Determination by Reference Method 10

The CO measurements were conducted according to USEPA RM 10, "Determination of Carbon Monoxide Emissions from Stationary Sources." Sample gas was continuously extracted from the test location and directed to a TEI Model 48C, Gas Filter Correlation (GFC), NDIR CO instrument for analysis. The GFC feature of the CO analyzer eliminates potential interference by substances, which absorb infrared energy.

USEPA RM 10 provides rigorous analyzer calibration requirements, including three point calibrations using USEPA Protocol 1 gas standards, and stringent instrument drift requirements. Calibrations were completed at 80 to 100 percent of the span value, 40 to 60 percent of the span value, and zero percent of the span value (ultra-pure nitrogen).

The CO analyzer was subjected to a zero and two up-scale calibration gases prior to the performance of the sample runs. The gas standards were certified and traceable to USEPA Protocol 1 specifications, which require that the gas concentration is within ±1 percent of the documented value. The response of the analyzer compared to each certified calibration standard must be within ±2 percent of the CS for each component.

To calibrate the instrument, the gas standards were introduced directly to the CO monitor at the sample inlet located on the back of the instrument. The amount of bias of the CO CEMS was determined. This was accomplished by introducing zero and one span gas to the CO system at the point in which the sample probe and heated sample filter are connected. The response of the analyzer system to the zero and span gas (bias check) must be less than ±5 percent of the CS for each component. The bias calibration check was performed prior to, and upon completion of, each sample run.

The magnitude of calibration drift was also calculated. Calibration drift is the difference in the initial (pre-test) bias calibration response and the final (post-test) bias calibration response for the same gas standard. The calibration drift must be within ±3 percent of the CS each sample run for each gas standard.

4.6 Visual Determination of Smoke Emissions by Reference Method 22

This method is applicable for the determination of the frequency of smoke emission from stationary sources. Smoke emissions produced during source operations are observed without the aid of instruments. This method determines the amount of time that visible emissions occur during an observation period (the accumulated emission time). This method does not require the determination of opacity emissions.

4.7 Dioxins and Furans Determination by Reference Method 23

USEPA RM 23, "Determination of Polychlorinated Dibenzo-p-dioxin and Polychlorinated Dibenzofuran Emissions from Municipal Waste Combustors," was followed to determine D/F concentrations and emissions from the Unit 412 test location.

4.7.1 Sample Train Component Preparation

All glass parts of the sample train, including the sorbent trap, were pre-cleaned prior to sampling according to the following procedures.

- Soak in hot soapy water (Alconox) at 50 degrees Celsius (°C) or higher;
- Rinse three times with tap water;
- · Rinse three times with deionized water;
- Rinse three times with pesticide grade acetone;
- Rinse three times with pesticide grade methanol/methylene chloride;
- Bake at 450 degrees Fahrenheit (°F) for 2 hours; and
- Seal with clean Teflon tape.

The glassware was sealed with Teflon tape followed by aluminum foil until sample train assembly. Following sample recovery, the glassware was reused at the same sampling location as allowed by the method.

The XAD-2 resin traps were pre-cleaned and prepared by Analytical Perspectives. Each sorbent trap was charged with 20 to 30 grams of the precleaned resin and the five surrogate compounds listed in Table 2 of RM 23 were added to the resin. Care was taken to ensure that the resin was kept at temperatures below 120°F during shipment and before and after sample collection to prevent resin decomposition. The time between charging the trap and use in the field was minimized and was not allowed to exceed 14 days. The sorbent traps were shipped from Analytical Perspectives to the Pogo facility under strict chain-of-custody (COC) documentation.

4.7.2 Sample Collection

Samples for D/F were withdrawn isokinetically from the source using an RM 23 sampling train as depicted in **Figure 4-1**. The sampling train consisted of a quartz glass nozzle and probe liner, a pretreated glass fiber filter maintained at a temperature of $248^{\circ}F \pm 25^{\circ}F$, a water-cooled condenser, a sorbent trap containing XAD-2 resin, five chilled impingers, and a metering console. The water-cooled condenser and sorbent trap were arranged in a manner that allows the condensate to drain vertically through the trap. Gas entering the trap was maintained at or below 68°F. The first impinger (optional knockout) was empty, the second and third impingers each contained 100 ml of HPLC water, the fourth was empty, and the fifth contained pre-weighed silica gel. Sealing greases were not used on any portion of the sample train.

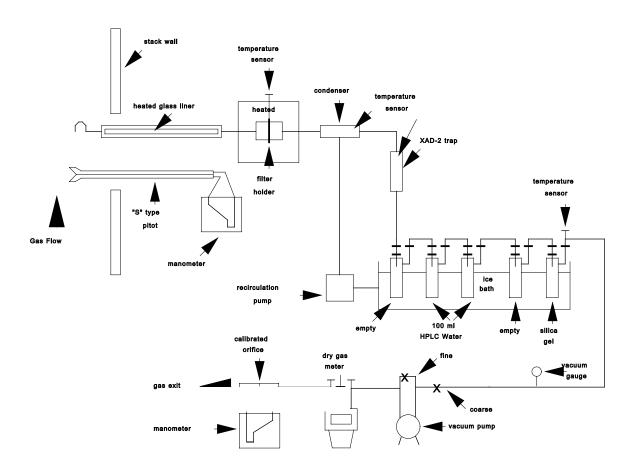


Figure 4-1 Reference Method 23 Sampling Train

4.7.3 Sample Recovery

Recovery of the samples and assembly of the sample trains for reuse was conducted in a dust-free environment. Each impinger and the XAD-2 trap was weighed prior to and at the conclusion of each sample run. The volume of water vapor condensed in the impingers, XAD resin, and silica gel was summed and entered into moisture content calculations.

All sample-exposed components of the sampling train were rinsed with acetone and methylene chloride (rinses recovered per RM 23), and toluene. Sample containers from a typical run include the following.

- Container 1 Filter(s);
- Container 2 Rinses of nozzle, probe, and front-half of filter holder and rinses of back-half of filter holder and condenser;
- Container 3 XAD cartridge and resin;
- Container 4 Impinger contents; and
- Container 5 Silica gel.

The samples, comprised of containers 1 through 3, were shipped to Analytical Perspectives, Inc. under strict COC documentation. Appropriate shipping containers were used to keep the samples cool during shipping.

4.7.4 Sample Analysis

The RM 23A samples were analyzed by Analytical Perspectives, Inc. in strict accordance with Analytical Perspective's QA Program. The filter(s), XAD-2 resin, toluene and methylene chloride rinses were analyzed for tetra-octa (4-8) D/F according to USEPA RM 23 with high-resolution gas chromatography/high resolution mass spectrometry. All extracts from one run were analyzed in separate front half and back half sample fractions.

4.7.5 Data Reduction

The D/F results are expressed in terms of toxicity equivalents (TEQ), as specified in 40 CFR 63.1342. The D/F congeners (tetra, hepta, hexa and octa) were converted to TEQ using toxicity equivalence factors (TEFs), as the summation of the TEFs of the congeners, multiplied by their relative concentrations.

Any D/F congeners that are reported by Analytical Perspectives, Inc. as nondetected (below the method detection limit ND) are counted as zero for the purpose of calculating the total D/F TEQ concentration for that sample, as specified in RM 23 (§7.4).

4.8 Hydrogen Chloride Determination by Reference Method 26A

USEPA RM 26A, "Determination of Hydrogen Halide and Halogen Emissions from Stationary Sources Isokinetic Method," was followed for the determination of HCI emissions at the Unit 412 test location. This method was performed in conjunction with the particulate measurement procedures as allowed by the methods. Included in the RM 26A sampling system was a calibrated quartz glass nozzle and probe assembly, stainless steel probe, insulated filter oven, glass filter holder and tared quartz-fiber filter, condenser assembly, and calibrated extraction system. The system vacuum extracted the effluent sample gas through the interconnected, leak-free components. The entire system was "leak checked" before and after each individual sample run to ensure sample integrity.

A "K-factor" (coefficient) was determined prior to the initiation of each RM 26A sample run. This coefficient was based upon preliminary measurements of gas temperature, flow rate, pressure, and moisture content. Multiplying the K-factor by the measured differential pressure at each sample point provided for isokinetic sample rates for each sample point. If a variable changed during a sample run, the coefficient was adjusted to maintain isokinetic sample rates. At isokinetic conditions, the velocity of the stack gas entering the nozzle of the extraction system was equal to the effluent velocity at the sample point.

The condenser assembly consisted of a series of five glass impingers with glass inserts interconnected to each other by glass U-tubes, providing a "leak tight" seal with 28/15 ball and socket connections. The

first and second impingers contained sulfuric acid (H_2SO_4). The third and fourth impingers contained sodium hydroxide (NaOH). The fifth impinger was filled with a pre-weighed amount of silica gel to capture any residual moisture from the sample stream. The impinger train was set in an ice bath to maintain the extracted gas outlet temperature at or below 70°F. By cooling the sample, all water vapor and gases were condensed and collected.

Three valid sample runs were performed at the test location. Upon completion of each sample run, the probe was removed from the effluent and allowed to cool. A leak check of the sampling system was then performed to verify the integrity of the system. The leak rate must not exceed 0.02 actual cubic feet per minute (acfm) in order for the test to be considered valid.

Each sample train was carefully recovered. The H_2SO_4 solution in the first two impingers was quantitatively recovered in a glass sample container. The impingers and connecting glassware were then rinsed with water and added to the same sample jar. The contents of the third and fourth impingers were placed in a glass sample jar. The silica gel from the fifth impinger was weighed to determine the moisture gain.

Portions of the H₂SO₄ absorbing reagent was collected for a blank and diluted to the approximate volume of the corresponding sample jars with rinse water from the same wash bottle used. All liquid levels were marked. The H₂SO₄ sample jars and reagent blanks were sent to TestAmerica located in West Sacramento, California, for HCl analysis by ICPMS.

4.9 Metals Determination by Reference Method 29

USEPA RM 29, "Determination of Metals Emissions from Stationary Sources," will be followed to determine the metals (Cd, Pb, Hg) emission rates exhausted by Unit 412. Included in the RM 29 sampling system will be a calibrated glass or Teflon coated stainless steel nozzle, stainless steel probe, glass or Teflon probe liner, insulated filter oven, glass filter holder, and tared quartz-fiber filter, condenser assembly, and calibrated extraction system. The system vacuum will be used to extract the effluent gas through the interconnected, leak-free components. The entire system will be "leak checked" before and after each individual sample run to ensure sample integrity.

A "K-factor" (coefficient) will be determined prior to the initiation of each mercury sample run. This coefficient will be based upon preliminary measurements of gas temperature, flow rate, pressure, and moisture content. Multiplying the K-factor by the measured differential pressure will determine the isokinetic sample rate for each sample point. If a variable changes during a sample run, the coefficient will be adjusted to maintain isokinetic sampling rates. At isokinetic conditions, the velocity of the stack gas entering the nozzle of the extraction system will be equal to the effluent velocity at the sample point.

4.9.1 Sampling by Reference Method 29

By this method, Cd, Pb, and Hg emissions were withdrawn isokinetically from the selected source, collected on a heated quartz fiber filter (maintained at a controlled temperature of 248 ± 25 °F), and passed through a series of chilled impingers containing solutions of nitric acid/hydrogen peroxide (HNO₃/H₂O₂) and potassium permanganate (KMnO₄) as shown in **Figure 4-2**.

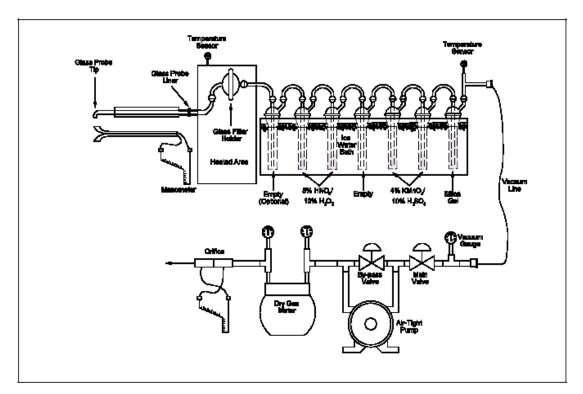


Figure 4-2 Reference Method 29 Sampling Train

The sample components were recovered in separate front-half (probe wash and filter) and back-half (impinger solutions) fractions. The front-half and back-half components were rinsed with 0.1 normal (N) nitric acid (HNO₃) to capture all residue and collected in their respective containers. The probe wash, digested filter, and aliquots of impinger solutions were analyzed for the selected metals by inductively coupled plasma-mass spectroscopy (ICPMS) analysis or cold vapor atomic absorption (CVAA) analysis.

The condenser assembly consisted of a series of six glass impingers with glass inserts interconnected to each other by glass U tubes, providing a "leak tight" seal with 28/15 ball and socket connections. The first and second impingers contained HNO_3/H_2O_2 . The third impinger was left empty. The fourth and fifth impingers contained $KMnO_4$. The sixth impinger was filled with a pre-weighed amount of silica gel to capture any residual moisture from the sample stream. The impinger train was set in an ice bath to maintain the extracted gas outlet temperature at or below $70^{\circ}F$. By cooling the sample, all water vapor and gases were condensed and collected. **Table 4-1** describes the condensate (impinger) train configuration for RM 29 testing including the $KMnO_4$ impingers which are exclusive to mercury capture and analysis.

Prior to sampling, the impingers and their contents were weighed and the initial weights recorded. Upon completion of sampling, the impingers were removed from the ice bath and the moisture gain determined gravimetrically by subtracting the final weight from the initial weight for each impinger.

Three valid sample runs were performed for each of the processes being tested. Upon completion of each sample run, the probe was removed from the exhaust stack and allowed to cool. A leak check of the sampling system was then performed to verify the integrity of the system. The leak rate must not exceed 0.02 actual cubic feet per minute (acfm), in order for the test to be considered valid.

AECOM Environment 4-10

Impinger No.	Contents	Configuration
1	100 ml HNO ₃ /H ₂ O ₂	Straight
2	100 ml HNO ₃ /H ₂ O ₂	Greenburg-Smith
3	Empty	Straight
4	100 ml KMnO ₄ (Optional)	Straight
5	100 ml KMnO ₄ (Optional)	Straight
6	200 - 300 grams Silica Gel	Straight

Table 4-1 Reference Method 29 Condensate (Impinger) Train

Each sample train was carefully recovered. The filter was removed from its sample holder with Teflon-coated or non-metallic tweezers and placed in a labeled petri dish. The nozzle, probe, and front-half of the filter holder were first rinsed with 0.1 NHNO₃ to collect any of the selected metals that adhered to the front-half components. The rinse was quantitatively recovered in a glass sample container. The contents of the first two impingers were placed in a glass sample jar and the contents of the third impinge were placed in a separate sample jar. The impingers and filter back-half were then rinsed with 100 ml of 0.1 NHNO₃ and added to the respective same sample jar. The contents of the fourth and fifth impingers were placed in a glass sample jar; these impingers were then rinsed with 100 ml of KMnO₄ and added to the same sample jar. The silica gel from the sixth impinger was weighed to determine moisture gain.

4.9.2 Analyses by Reference Method 29

Each recovered sample was composed of five fractions: a filter, HNO_3 front-half wash, HNO_3/H_2O_2 impinger contents with rinse, empty impinge with rinse and $KMnO_4$ impinger contents and rinse. The filters were digested and added to the probe wash for mercury analysis. Proportional aliquots of the probe rinse (front-half of the sample train) and samples recovered from impingers 1 and 2 and rinses, empty impinge, and rinse (back-half of the sample train) were combined and analyzed for selected metals by ICPMS and mercury by CVAA.

4.10 Calculations and Nomenclature

The following section presents the calculations for determining flow rate, molecular weight, and moisture content. In addition, calculations for the determination of particulate concentration and pollutant emission rate are provided below. The nomenclature for each calculation also is defined.

Calculations

Stack Pressure (in Hg):

$$P_s = P_b + \frac{P_g}{13.6}$$

Volume of Water Collected (scf):

$$V_{wc(std)} = 0.04707 \times MG$$

Gas Meter Volume at Standard Conditions (dscf):

$$V_{m(std)} = V_m \times Y_d \times \left(\frac{T_{std}}{P_{std}}\right) \times \left(\frac{P_b + \frac{\Delta H_{avg}}{13.6}}{T_{m(avg)}}\right)$$

Fractional Moisture Content (dimensionless):

$$B_{ws} = \frac{V_{wc(std)}}{V_{wc(std)} + V_{m(std)}}$$

Moisture Content (%):

$$H_2O\% = B_{ws} \times 100$$

Molecular Weight (dry, lb/lb-mole):

$$M_d = (0.44 \times \% CO_2 + (0.32 \times \% O_2) + (0.28 \times (100 - \% CO_2 - \% O_2))$$

Molecular Weight (wet, lb/lb-mole):

$$M_s = M_d \times (1 - B_{ws}) + (18 \times B_{ws})$$

Velocity (feet per second):

$$V_s = 85.49 \times C_p \times \sqrt{\Delta p} \times \sqrt{\frac{T_s}{P_s \times M_w}}$$

Flow Rate (actual cubic feet per minute):

$$Q_a = V_s \times A_s \times 60$$

Flow Rate (dry standard cubic feet per minute):

$$Q_s = Q_a \times (1 - B_{ws}) \times 17.64 \times \left(\frac{P_s}{T_s}\right)$$

Percent Isokinetic (%):

$$\% I = \frac{0.09450 \times T_{s} \times V_{m(std)}}{P_{s} \times V_{s} \times A_{n} \times \Theta \times (I - B_{ws})}$$

Particulate Concentration (lb/dscf):

$$C_{particulate} = \frac{MG_{particulate}}{453.5924 \text{ x V}_{m(\text{std})}}$$

Particulate Emission Rate (lb/hr):

$$E_p = C_{particulate} x dscfm x 60$$

Gaseous Pollutant Concentration (dry, ppm):

$$C_{gas} = (C' - C_o) \times \left(\frac{C_{ma}}{C_m - C_o}\right)$$

Gaseous Pollutant Emission Rate (lb/hr):

$$E_{gas} = \frac{C_{gas} \times MW \times Q_s \times 60}{385 \times 1,000,000}$$

Emissions of D/F (ng TEQ/dscm):

$$C_{(D/F)T} = \frac{\sum_{i=1}^{n} C_{(D/F)_i} TEF_i}{V_{m(std)}} \frac{ng}{1,000pg} \frac{(20.9-7)}{(20.9-\%O_2)}$$

Nomenclature

A_n Cross-Sectional Area of the Nozzle (square feet)

A_s Cross-Sectional Area of the Stack (square feet)

B_{ws} Water Vapor in Gas Stream (proportional by volume)

C' Average Gas Concentration Indicated by Analyzer, dry basis (ppm)

CC Confidence Coefficient (one tailed, 2.5% error)

C_{gas} Corrected Effluent Gas Concentration, dry basis (ppm)

C_m Average of Initial and Final System Calibration Bias Check Responses for the Upscale Calibration Gas (ppm)

C_{ma} Actual Concentration of Upscale Calibration Gas (ppm)

C_o Average of Initial and Final System Calibration Bias Check Responses for the Zero Gas (ppm)

C_p Pitot Tube Coefficient, Dimensionless (0.84 for Type-S)

Cparticulate Concentration (lb//dscf)

C_{(D/F)I} Concentration of D/F congener i in sample (pg/liter)

C_{(D/F)T} Total concentration of D/F congeners in sample (ng/liter)

D/F Stack concentration of polychlorinated dibenzo-p-dioxins and polychlorinated dibenzofurans (ng TEQ/dscm)

 Δ P Average Velocity Head of Gas (in WC)

E_p Particulate Emission Rate (lb/hr)

H₂O% Moisture Content of Gas Stream (%)

M_d Molecular Weight of Stack Gas, dry basis (lb/lb-mole)

M_s Molecular Weight of Stack Gas, wet basis (lb/lb-mole)

MG_{particulate} Particulate mass gain (mg)

MW Molecular Weight of Pollutant ($SO_2 = 64$, $NO_X = 46$, CO = 28)

ng nanograms (10⁻⁹ grams)

pg picograms (10⁻¹² grams)

P_b Uncorrected Barometric Pressure (in Hg)

P_q Static Pressure of Stack Gas (in WC)

P_s Absolute Pressure of Stack Gas (in Hg)

P_{std} Standard Absolute Pressure (29.92 in. Hg)

%CO₂ Percent Carbon Dioxide, Dry Basis

%O₂ Percent Oxygen, Dry Basis

%I Isokinetic sample rate (%)

Q_a Actual Flow Rate (acfm)

Q_s Dry Standard Flow Rate (dscfm)

RM Reference Method (RM 6C, RM 7E or RM 10) Data Average (Arithmetic Mean)

T_{m(avg)} Average DGM Absolute Temperature (°R)

T_s Average Stack Gas Temperature (°R)

V_s Average Gas Velocity (feet per minute)

T_{std} Standard Absolute Temperature (528 °R)

V_m Dry Gas Volume as Measured by the DGM (dcf)

 $V_{\text{m(std)}} \qquad \text{Dry Gas Volume Corrected to Standard Conditions (dscf)}$

 $V_{\text{wc(std)}} \hspace{0.5cm} \text{Volume of H}_2\text{O Collected in Impingers and Silica Gel Corrected to Standard Conditions (ml)} \\$

Y_d DGM Calibration Factor

Θ Sample Time (minutes)

5.0 Quality Assurance/Quality Control

5.1 Objectives

The objectives of AECOM's QA/QC program are as follows:

- To continually monitor the precision and accuracy of the data being generated for all source emission measurements.
- To implement measures designed to control the precision and accuracy of all data generated for individual sources.
- To maintain permanent records of analytical QC data and equipment calibrations that include traceability and certification.
- To identify, document, and maintain a COC log, which accounts for each method sample collected during each measurement program.

5.2 Field Program

All primary, USEPA-approved testing procedures selected for this test program are referenced in 40 CFR 60, Appendix A. No deviations from these procedures were expected or necessary. All field personnel responsible for this emission test program strictly followed the procedures dictated by the applicable test methods.

All field test personnel involved with this test program are experienced and trained in field sampling methods and procedures. Each field personnel was assigned key responsibilities in phases of sample collection, sample recovery, COC, and transportation of samples. Basic responsibilities for field personnel include, but are not limited to:

Record keeping. Field personnel recorded all pertinent test parameters and relevant observations on the appropriate field data forms.

Safety requirements. Field personnel are familiar with all company safety regulations and are provided with all the necessary safety equipment.

Sample handling. Field personnel are trained in the proper procedures for handling samples including: use of sample containers, sample preservation, identification, storage of collected samples, and COC.

Instrumentation. Specific field personnel are trained in the proper operation, calibration, trouble shooting, and maintenance of the instrumentation intended for this program. This includes the use of pumps, control console(s), samplers, and instrumentation.

Quality control (QC). Field personnel are trained in all aspects of QC that relate directly to the specific reference method test procedures, sample handling, analyses, and reporting.

Mr. John Rosburg, of AECOM, is the designated field manager and was responsible for coordinating testing activities with Pogo and ADEC. He provided answers to questions concerning test methodology, QC, and all other project aspects. The field manager also was responsible for delegating work assignments to the members of the test crew, making sure all QA/QC procedures are carried out, and documenting all field activities in a bound log book.

All field instrumentation was maintained and calibrated according to all applicable USEPA guidelines. Records of instrument maintenance and calibration are kept in historical files and continually updated. Calibrations of all field instrumentation, at a minimum, meet or exceed the mandated procedures stipulated in the Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III. All

AECOM Environment 5-2

documentation of calibrations are maintained on file at all times. Calibration documentation for the equipment used in this test program is provided in the appendices of this test report.

5.3 Sample Documentation

All field data collected for each selected reference method test procedure was documented on field data forms. Each form, specific to each particular sample run, included information as to the source tested, date and time of sample collection, analyst(s) performing the test, and all data necessary for test validation. Each field data sheet was completed by the responsible technician at the time of the test and checked by the Field Manager for accuracy and completeness after each test series. Copies of all raw field data sheets are included in the appendices of this test report, with the originals maintained in project files at AECOM's Fort Collins office.

Sample containers utilized for the collection and storage of samples are specific to each test procedure. Filter substrates were maintained in individually labeled polyethylene Petri dishes sufficient in size to receive the samples unaltered and with the exposed surface protected from sample loss.

Collection of all blanks was specific to each test performed. The field blanks were collected at the test location and subjected to the same ambient conditions as the samples. This type of blank was collected for each reagent used in each test series and analyzed in the same manner as the sample itself.

Each recovered sample was labeled with standard sample tags and uniquely identified. The tags provided information regarding the unit tested, sample location, date and time of collection, reagent(s) used, and the test number. The sample containers were sealed, liquid level marked (if applicable), and properly stored until they were transported to the laboratory.

Standard COC forms were completed before any samples were transported to the laboratory. This procedure is dictated by the USEPA and strictly adhered to by AECOM. Each sample was tagged with a COC tag, which requires the same information as the field sample label.

5.4 Analytical Quality Control

All analytical procedures used for this program are approved by the USEPA and referenced in 40 CFR 60 (where applicable). AECOM's QA/QC program meets or exceeds USEPA standards. All particulate gravimetric analysis was performed by TestAmerica in West Sacramento, California. The D/F XAD-2 resin traps and filters were prepared by Analytical Perspectives of Wilmington, North Carolina, who also performed the sample RM 23 analyses. The metals (Cd, Pb, Hg) and HCl analyses were performed by TestAmerica.

5.5 Data Reduction, Validation, and Reporting

AECOM has implemented specific measures to ensure that reliable data is generated as a result of the sampling and analytical activities of every field program. The objective of this phase of AECOM's QA/QC program is to follow the proper collection of representative and QA field and analytical data with approved data reduction methods and equations.

All calculations are performed using QA spreadsheets incorporating standard accepted equations, as required by the applicable pollutant specific sampling methodology. Data reduction was performed by qualified engineers or data analysts familiar with standard engineering practices and approved methods. Calculation methods and equations, including conversion factors and units, are defined in this test report to allow the reviewer to easily reproduce the final results from the raw field data and process information provided in the appendices of the report. This final report includes all raw data, QA/QC documentation, and process data collected during the test program. The initial draft of this test report, including both narrative and calculations, was subjected to review by the project manager and/or Principal-in-Charge, prior to final publication.

AECOM Environment

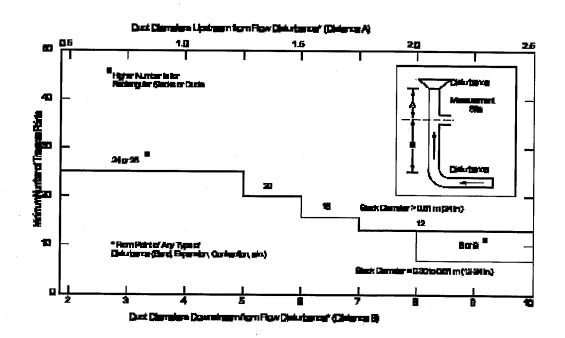
Appendix A

Field Data Forms and CEMS Data

RM 1 - Minimum Number of Traverse Points

Client Sumitomo Metal Mining Inc.	Stack Diameter (in)	30	•
Location Delta Junction, AK	Upstream Distance (in)	36	Diameters 1.2
Source Incinerator	Downstream Distance (in)	144	Diameters 4.8
Operator J. Rosburg	Port Depth (in)	4.0	
	Part Diameter (in)	4	

			Location of	Traverse P			1			
İ				Numbe	r of travers	e points				
İ	L			% of stack d		m inside wa	ıll)			
		6	8	10	12	16	20	24	Distance (in)	Distance with port (in)
-	1	4,4	3,2	2.6	2.1	1.6	1,3	1,1	1.0	5,0
	2	14.5	10.5	8.2	6.7	4.9	2.9	3.2	2.0	6,0
	3	29.6	19.4	14.6	11.8	8.5	6.7	5.5	3,5	7.5
	4	70.4	32.3	22,6	17.7	12.5	9.7	7.9	5.3	9.3
	5	85,4	67.7	34.2	25.0	16.9	12.9	10.5	7.5	11.5
	6	95,6	80.6	66.8	35.6	22.0	16.5	12.2	10.7	14.7
	7		89.5	77.4	64.4	28,3	20,4	16.1	19.3	23,3
	8		96.8	85.4	75.0	37.5	25.0	19.4	22.5	26.5
Traverse Point Number	9			91.8	82.3	62.5	30.6	23.0	24.7	28.7
Ξ	10			97.4	88.2	71.7	38.8	27.2	26.5	30.5
Ž	11				93,3	78.0	61.2	32.3	28.0	32.0
Ħ	12				97.9	83.1	69.4	39.8	29.0	33.0
<u>.</u>	13					87.5	75.0	60.2		
υ -	14					91.5	79,6	67.7		
ĕ	15					95.1	83,5	72.8		
ĕ	16					98.4	87.1	77.0		
20	17						90.3	80.6		
	18						93.3	83.9		
	19						96.1	86.8		
	20						98.7	88.6		
	21							92.1		
	22							94.5		
	23							96.8		
	24							99,9		



Run I5-1 09/29/13		* · · · · · · · · · · · · · · · · · · ·											
Time (1-min)	NOx (ppm)	(ppm Cor.)	Ox (ib/hr)	CO (ppm)	CO (ppm Cor.)	(lb/hr)	SO2 (ppm)	SO (ppm Cor.)	2 (lb/hr)	O2 (%)	O2 (% Cor.)	CO2 (%)	CO2 (% Cor.)
1106	56.1	56.9	0.35	-0.2	0.1	0.00	1.9	1.2	0.01	11.98	11.95	5.86	6.21
1107	56.5	57.3	0.35	-0.2	0.1	0.00	2.6	1.8	0.01	12.79	12.76	5.58	5.92
1108 1109	177.7 189.8	180.3 192.6	1.10 1.17	-0.6	-0.3	0.00	52.1	51.6	0.44	9.06	9.02	8.80	9.35
1110	192.3	195.1	1.17	0.4	0.7 1.0	0.00 0.00	48.3 57.8	47.7	0.40	11.13	11.09	7.32	7.77
1111	171.2	173.7	1.06	1.1	1.4	0.00	49.1	57.2 48.5	0.48 0.41	10.62 10.92	10.58 10.88	7.55 7.25	8.02 7.70
1112	144.6	146.7	0.89	2.4	2.7	0.01	40.3	39.6	0.34	10.73	10.69	7.35	7.70
1113	116.8	118.5	0.72	3.8	4.0	0.01	36.8	36.2	0.31	10.70	10.66	7.25	7.70
1114	81.4	82.6	0.50	4.5	4.7	0.02	33.0	32.4	0.27	9.62	9.58	7.95	8.44
1115 1116	58.1 47.8	59.0 48.6	0.36 0.30	1.7	1.9	0.01	25.3	24.6	0.21	9.35	9.31	7.97	8.46
1117	46.9	47.6	0.30	-0.2 -0.3	0.1 0.0	0.00 0.00	18.5 14.1	17.8 13.3	0.15	10.13	10.09	7.46	7.92
1118	52.0	52.8	0.32	-0.5	-0.2	0.00	12.1	11.3	0.11 0.10	10.02 10.54	9.98 10.50	7.49 7.06	7.95 7.50
1119	51.6	52.4	0.32	-0.5	-0.2	0.00	10.1	9.3	0.08	11.62	11.58	6.35	6.74
1120	56.3	57.1	0.35	-0.4	-0.1	0.00	8.7	7.9	0.07	11.53	11.49	6.44	6.84
1121 1122	57.7 64.9	58.6 65.9	0.36 0.40	-0.4	-0.1	0.00	8.3	7.6	0.06	11.70	11.66	6.24	6.62
1123	56.5	57.3	0.40	-0.4 -0.2	-0.1 0.1	0.00 0.00	7.9 8.4	7.1 7.6	0.06 0.06	11.98	11.95	6.05	6.42
1124	54.2	55.0	0.33	1.3	1.6	0.01	8.9	8.1	0.07	12.31 12.13	12.28 12.10	5.81 6.18	6.17 6.56
1125	43.8	44.5	0.27	0.1	0.4	0.00	13,6	12.8	0.11	9.23	9,19	8.06	8.56
1126	44.3	44.9	0.27	-0.4	-0.1	0.00	15.7	14.9	0.13	9.88	9.84	7.51	7.97
1127 1128	46.2	47.0	0.29	-0.4	-0.1	0.00	15.1	14.3	0.12	10.38	10.34	7.27	7.72
1129	45.7 51.0	46.4 51.8	0.28 0.31	-0.5 -0.6	-0.1 -0.3	0.00	15.4	14.6	0.12	9.98	9.94	7.45	7.91
1130	49.9	50.6	0.31	-0.6	-0.3	0.00 0.00	16.2 15.3	15.4 14.5	0.13 0.12	10.22	10.18 10.94	7.23 6.74	7.68 7.16
1131	51.4	52.2	0.32	-0.5	-0.2	0.00	13.4	12.7	0.12	10.50	10.55	7.03	7.16 7.46
1132	53.5	54.3	0.33	-0.6	-0.3	0.00	13.2	12.5	0.11	10.57	10.53	6.98	7.41
1133	51.2	52.0	0.32	-0.6	-0.3	0.00	12.4	11.6	0.10	11.13	11.09	6.57	6.97
1134 1135	54.5 53.2	55.4 54.0	0.34	-0.6	-0.3	0.00	12.1	11.4	0.10	10.87	10.83	6.83	7.25
1135	53.2	54.0 53.9	0.33 0.33	-0.6 -0.7	-0.3 -0.4	0.00 0.00	12.2 12.2	11.4	0.10	10.60	10.56	6.95	7.37
1137	55.5	56.4	0.34	-0.7	-0.4	0.00	11.2	11.4 10.4	0.10 0.09	11.16 11.23	11.12 11.19	6.51 6.57	6.91 6.98
1138	51.9	52.7	0.32	-0.6	-0.3	0.00	10.7	10.0	0.03	10.93	10.89	6.70	7.12
1139	53.7	54.5	0.33	-0.7	-0.3	0.00	10.8	10.0	0.08	11.22	11.18	6.51	6.91
1140	64.1	65.1	0.40	-0.7	-0.4	0.00	22.7	22.0	0.19	10.41	10.37	7.89	8.38
1141 1142	108.5 61.4	110.1 62.3	0.67 0.38	-0.6 -0.8	-0.3 -0.5	0.00	42.8	42.2	0.36	9.77	9.73	8.46	8.99
1143	50.8	51.6	0.31	-1.0	-0.7	0.00 0.00	32.9 21.5	32.3 20.8	0.27 0.18	9.38 9.87	9.34	8.26	8.77
1144	55.4	56.2	0.34	-1.0	-0.7	0.00	18.7	17.9	0.15	10.06	9.83 10.02	7.93 7.66	8.42 8.13
1145	53.0	53.8	0.33	-1.0	-0.7	0.00	16.3	15.5	0.13	11.23	11.19	6.87	7.29
1146	55.8	56.6	0.34	-1.0	-0.7	0.00	13.6	12.9	0.11	10.83	10.79	7.15	7.59
1147 1148	62.5 60.5	63.4	0.39	-1.1	-0.8	0.00	12.8	12.0	0.10	11.12	11.08	6.82	7.24
1149	65.5	61.4 66.4	0.37 0.40	-1.0 -0.9	-0.7 -0.6	0.00 0.00	12.0	11.3	0.10	11.96	11.93	6.27	6.65
1150	66.2	67.2	0.41	-1.0	-0.7	0.00	11.4 10.9	10.6 10.1	0.09 0.09	11.61 11.50	11.57 11.46	6.53 6.51	6.93
1151	69.3	70.4	0.43	-1.0	-0.7	0.00	10.6	9.9	0.08	11.99	11.96	6.13	6.90 6.50
1152	61.6	62.5	0.38	-0.8	-0.5	0.00	12.1	11.3	0.10	10.83	10.79	7.04	7.47
1153	57.4	58.3	0.35	-1.0	-0.7	0.00	13.0	12.2	0.10	10.09	10.05	7.38	7.84
1154 1155	63.0 66.8	64.0 67.8	0.39	-1.1	-0.8	0.00	12.4	11.6	0.10	10.61	10.57	6.96	7.39
1156	62.9	63.8	0.41 0.39	-1.0 0.7	-0.7 0.9	0.00 0.00	11.1 9.8	10.3 9.0	0.09 80.0	10.99 11.93	10.95	6.82	7.23
1157	60.9	61.8	0.38	-0.9	-0.6	0.00	10.2	9.4	0.08	10.76	11.90 10.72	6.20 6.90	6.58 7.33
1158	57.0	57.9	0.35	-1.2	-0.9	0.00	11.1	10.4	0.09	11.19	11.15	6.61	7.01
1159	61.9	62.8	0.38	-1.3	-1.0	0.00	13.2	12.5	0.11	10.40	10.36	7.25	7.70
1200 1201	63.0 59.8	64.0 60.7	0.39 0.37	-1.4 -1.5	-1.1 -1.2	0.00	16.8	16.1	0.14	9.85	9.81	7.54	8.01
1202	61.5	62.4	0.37	-1.5 -1.4	-1.2 -1.1	0.00 0.00	18.5 18.7	17.8 18.0	0.15 0.15	10.49 9.95	10.45 9.91	7.08	7.52
1203	62.7	63.7	0.39	-1.5	-1.1	0.00	18.4	17.7	0.15	9.98	9.94	7.53 7.40	8.00 7.86
1204	59.1	60.0	0.37	-1.5	-1.1	0.00	17.1	16.3	0.14	10.84	10.80	6.85	7.27
1205	61.2	62.1	0.38	-1.4	-1.1	0.00	16.0	15.3	0.13	10.32	10.28	7.27	7.72
1206	62.6	63.6	0.39	-1.4	-1.1	0.00	15.9	15.2	0.13	10.33	10.29	7.18	7.62
1207 1208	61.0 67.3	61.9 68.3	0.38 0.42	-1.4 -1.4	-1.1 -1.1	0.00 0.00	15.1 13.1	14.3 12.4	0.12	11.28	11.24	6.49	6.89
1209	66.8	67.8	0.41	-1.4	-1.0	0.00	13.1	12.4	0.10 0.10	11.56 11.47	11.52 11.43	6.41 6.38	6.80 6.77
1210	72.0	73.1	0.44	-1.4	-1.0	0.00	12.4	11.7	0.10	11.92	11.43	6.03	6.39
1211	60.4	61.3	0.37	-1.0	-0.7	0.00	13.4	12.6	0.11	11.64	11.60	6.32	6.71
1212 1213	55.6 187.2	56.4	0.34	-1.3	-0.9	0.00	13.6	12.8	0.11	11.17	11.13	6,55	6.95
1213	124.3	190.0 126.1	1.15 0.77	59.6 31.3	59.0 31.1	0.22 0.11	68.2 36.6	67.7 35.9	0.57 0.30	9.12	9.08	8.88	9.43
1215	74.2	75.3	0.46	0.6	0.9	0.00	32.9	30.9 32.2	0.30	11.65 10.14	11.61 10.10	7.12 7.87	7.56 8.36
1216	54.3	55.1	0.34	-0.6	-0.3	0.00	24.1	23.4	0.20	9.78	9.74	7.87 7.91	8.40
1217	52.9	53.7	0.33	-1.3	-0.9	0.00	. 17.9	17.2	0.15	10.55	10.51	7.40	7.86
1218	57.4 50.2	58.2	0.35	-1.6	-1.2	0.00	14.9	14.2	0.12	10.08	10.04	7.62	8.09
1219 1220	59.3 65.6	60.2 66.6	0.37 0.41	-1.6 -1.5	-1.3 -1.2	0.00	13.2	12.5	0.11	11.24	11.20	6.75	7.16
1221	63.6	64.5	0.41	-1.5 -1.5	-1.2 -1.2	0.00 0.00	10.9 9.9	10.1 9.1	0.09 0.08	11.29 11.24	11.25	6.77	7.18
1222	60.5	61.4	0.37	-1.5	-1.2	0.00	9.1	8.4	0.08	12.20	11.20 12.17	6.66 5.97	7.07 6.34
1223	66.8	67.8	0.41	-1.4	-1.1	0.00	8.6	7.9	0.07	11.99	11.96	6.19	6.57
1224	66.6	67.6	0.41	-1.4	-1.1	0.00	8.7	8.0	0.07	11.90	11.87	6.15	6.52
1225 1226	65.7 60.5	66.7	0.41	-1.5	-1.2	0.00	11.3	10.6	0.09	11.00	10.96	6.75	7.16
1226	60.5 60.8	61.4 61.7	0.37 0.38	-1.5 -1.6	-1.2 -1.3	0.00 0.00	11.9	11.2	0.09	10.64	10.60	7.02	7.45
1228	62.5	63.5	0.39	-1.6 -1.5	-1.3 -1.2	0.00	12.1 11.8	11.3 11.1	0.10 0.09	10.30 11.16	10.26 11.12	7.15 6.54	7.59
1229	65.8	66.8	0.41	-1.3	-0.9	0.00	15.4	14.6	0.12	10.94	10.90	7.12	6.94 7.56
1230	116.2	117.9	0.72	-1.9	-1.6	-0.01	39.0	38.4	0.32	9.80	9.76	8.04	8.54
1231	120.8	122.6	0.75	-1.7	-1.3	0.00	38.6	38.0	0.32	10.77	10.73	7.43	7.89
1232 1233	116.8 100.6	118.5	0.72	-1.8	-1.5	-0.01	39.6	38.9	0.33	10.18	10.14	7.79	8.27
1234	78.4	102.1 79.6	0.62 0.48	-1.1 0.3	-0.8 0.6	0.00 0.00	39.3 39.7	38.7 39.0	0.33	9.82	9.78	8.01	8.51
1235	60.0	60.9	0.37	-0.7	-0.4	0.00	39.7	33.0	0.33 0.28	9.76 9.28	9.72 9.24	7.89 8.25	8.38 8.76
1236	50.1	50.9	0.31	-1.8	-1.5	-0.01	32.5	31.8	0.27	9.09	9.24	8.25 8.14	8.76 8.64
1237	51.1	51.9	0.32	-2.1	-1.8	-0.01	25.1	24.4	0.21	10.46	10.42	7.33	7.78
1238	54.3	55.1.	0.34	-2.1	-1.7	-0.01	20.8	20.1	0.17	10.02	9.98	7.53	8.00
1239 1240	56.2 55.9	57.1 56.7	0.35	-2.1	-1.7 4.7	-0.01	19.2	18.5	0.16	10.65	10.61	7.04	7.47
1241	55.9	56.7 56.8	0.34 0.35	-2.0 -2.1	-1.7 -1.7	-0.01 -0.01	16.8 16.6	16.1 15.9	0.14	10.89	10.85	6.99	7.42
	55.0] 55.6	. 0.00	-2.1	-1.7	-0.01	16.6	15.9	0.13	10.48	10.44	7.16	7.60
Ave	70.1	71.2	0.43	0.2	0.5	0.00	19.2	18.5	0.16	10.75	10.71	7.07	7.51

Table 2 Continuous Emissions Measurements Results Run I29-1 09/29/13

Time (1-min)	NOx (ppm)	NOx (ppm Cor.)	(lb/hr)	CO (ppm)	(ppm Cor.)	(lb/hr)	SO2 (ppm)	SO: (ppm Cor.)	2 (lb/hr)	O2 (%)	O2 (% Cor.)	CO2 (%)	CO2
-	(FF)	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		(66)	(PP.III COI.)	(16/11)	(ррпп)	(ррш оот.)	(10/111)	(76)	(% 001.)		(78 CO
1406	69.9	70.7	0.41	-1.4	-0.3	0.00	18.4	17.8	0.14	11.01	10.99	6.75	7.19
1407	74.7	75.6	0.44	-1.2	-0.1	0.00	17.4	16.8	0.14	12.22	12.21	5.94	6.32
1408	91.7	92.8	0.54	0.8	. 1.8	0.01	29.4	29.0	0.23	9.67	9.65	8.27	8.82
1409 ~	139.8	141.4	0.82	0.7	1.7	0.01	36.9	36.7	0.30	9.59	9.57	8.34	8.89
1410	139.9	141.5	0.82	-1.2	-0.1	0.00	40.3	40.1	0.32	9.76	9.74	8.25	8.79
1411	131.0	132.5	0.77	-1.7	-0.6	0.00	45.5	45.4	0.37	9.30	9.28	8.46	9.02
1412	112.7	114.0	0.66	-1.7	-0.7	0.00	46.4	46.3	0.37	9.19	9.17	8.54	9.10
1413	114.2	115.5	0.67	-1.7	-0.7	0.00	45.7	45.6	0.37	8.81	8.78	8.59	9.10
1414	94.6	95.7	0.56	-1.6	-0.6	0.00	37.4	37.1	0.30	9.52	9.50	8.17	8.7
1415 1416	80.1 53.6	81.0	0.47	-1.7	-0.6	0.00	36.5	36.3	0.29	8.52	8.49	8.73	9.3
1417	46.9	54.3 47.5	0.32 0.28	-1.7 1.7	-0.6	0.00	34.0	33.7	0.27	9,65	9.63	7.87	8.39
1418	49.6	50.2	0.29	-1.7 -1.8	-0.7 -0.7	0.00	26.7	26.3	0.21	9.36	9.34	8.14	8.68
1419	49.8	50.4	0.29	-1.0 -1.7	-0.7	0.00 0.00	26.1 21.4	25.7 20.9	0.21	9.58	9.56	7.84	8.36
1420	53.6	54.3	0.32	-1.8	-0.7	0.00	22.3	21.7	0.17 0.18	10.54 9.93	10.52 9.91	7.29 7.65	7.77 8.15
1421	55.3	55.9	0.33	-1.8	-0.7	0.00	21.0	20.4	0.17	10.57	10.55	7.13	7.60
1422	52.1	52.7	0.31	-1.8	-0.7	0.00	18.2	17.6	0.17	10.57	10.55	7.13 7.12	7.59
1423	57.9	58.6	0.34	-1.6	-0.6	0.00	19.7	19.1	0.15	10.77	10.75	6.99	7.4
1424	59.2	59.9	0.35	-1.3	-0.3	0.00	26.4	25.9	0.13	10.79	10.77	7.35	7.83
1425	70.0	70.8	0.41	-1.6	-0.5	0.00	36.0	35.7	0.29	9.34	9.32	8.23	8.77
1426	90.7	91.8	0.53	-1.2	-0.2	0.00	41.5	41.3	0.33	10.78	10.76	7.31	7.79
1427	84.0	85.0	0.49	-1.6	-0.5	0.00	48.4	48.4	0.39	9.23	9.21	8.24	8.78
1428	93.0	94.1	0.55	-1.8	-0.7	0.00	43.2	43.1	0.35	9.12	9.10	8.41	8.97
1429	82.2	83.2	0.48	-1.9	-0.8	0.00	43.7	43.6	0.35	8.64	8.61	8.51	9.07
1430	57.9	58.6	0.34	-2.0	-0.9	0.00	37.6	37.4	0.30	9.66	9.64	7.91	8.43
1431	46.0	46.6	0.27	-1.9	-0.9	0.00	35.7	35.4	0.29	9.23	9.21	8.14	8.68
1432	46.4	46.9	0.27	-2.0	-0.9	0.00	33.4	33.0	0.27	9.53	9.51	7.83	8.3
1433	47.4	47.9	0.28	-2.1	-1.0	0.00	29.3	28.9	0.23	10.53	10.51	7.22	7.69
1434	52.1	52.7	0.31	-2.0	-0.9	0.00	26.5	26.1	0.21	9.93	9.91	7.64	8.14
1435	53.3	53.9	0.31	-2.0	-1.0	0.00	27.8	27.4	0.22	10.54	10.52	7.10	7.57
1436	53.6	54.2	0.32	-2.0	-0.9	0.00	22.1	21.5	0.17	10.75	10.73	7.08	7.54
1437	58.5	59.2	0.34	-2.0	-1.0	0.00	24.8	24.3	0.20	10.42	10.40	7.19	7.66
1438	62.3	63.0	0.37	-2.0	-1.0	0.00	22.1	21.5	0.17	11.37	11.36	6.57	7.00
1439 1440	58.8	59.5	0.35	-1.6	-0.5	0.00	20.3	19.8	0.16	11.94	11.93	6.28	6.68
1441	116.0 100.7	117.3 101.9	0.68 0.59	-1.9 -2.1	-0.9	0.00	39.5	39.3	0.32	9.85	9.83	8.24	8.78
1442	58.1	58.8	0.34	-2.1 -2.2	-1.1 -1.1	0.00	47.8 45.4	47.7 45.3	0.39	9.48	9.46	8.30	8.86
1443	55.9	56.5	0.33	-2.2	-1.2	0.00	38.3	38.1	0.37 0.31	9.02 10.38	9.00 10.36	8.33	8.88
1444	51.4	52.0	0.30	-2.2	-1.1	0.00	32.2	31.8	0.26	10.51	10.49	7.33 7.31	7.81
1445	55.4	56.1	0.33	-2.2	-1.1	0.00	30.3	29.9	0.24	10.45	10.43	7.20	7.67
1446	54.9	55.6	0.32	-2.2	-1.1	0.00	28.6	28.2	0.23	11.35	11.34	6.63	7.06
1447	56.7	57.4	0.33	-2.2	-1.1	0.00	26.4	25.9	0.21	10.79	10.77	7.05	7.51
1448	59.1	59.8	0.35	-2.2	-1.1	0.00	26.0	25.6	0.21	10.88	10.86	6.86	7.31
1449	57.3	57.9	0.34	-2.2	-1.1	0.00	26.0	25.5	0.21	11.63	11.62	6.42	6.84
1450	61.2	62.0	0.36	-2.2	-1.2	0.00	22.8	22.3	0.18	11.05	11.03	6.80	7.24
1451	67.1	67.9	0.39	-2.3	-1.2	0.00	22.8	22.3	0.18	11.06	11.04	6.70	7.13
1452	73.2	74.1	0.43	-2.2	-1.2	0.00	22.1	21.6	0.17	11.89	11.88	6.13	6.53
1453	67.5	68.3	0.40	-2.3	-1.2	0.00	19.6	19.0	0.15	11.84	11.83	6.26	6.67
1454	74.0	74.9	0.44	-2.2	-1.2	0.00	21.0	20.5	0.17	11.63	11.62	6.31	6.72
1455	72.6	73.5	0.43	-1.9	-0.8	0.00	25.7	25.3	0.20	11.33	11.32	6.71	7.18
1456	103.4	104.6	0.61	-2.3	-1.2	0.00	46.5	46.4	0.38	9.51	9.49	8.27	8.82
1457	81.6	82.6	0.48	-2.3	-1.2	0.00	48.0	48.0	0.39	9.59	9.57	8.22	8.76
1458	57.5	58.1	0.34	-2.3	-1.2	0.00	46.3	46.2	0.37	9.09	9.07	8.50	9.06
1459	51.5	52.1	0.30	-2.3	-1.2	0.00	43.8	43.6	0.35	9.48	9.46	8.04	8.57
1500	57.3	57.9	0.34	-2.3	-1.2	0.00	40.5	40.3	0.33	10.14	10.12	7.71	8.22
1501	65.3	66.0	0.38	-2.3	-1.2	0.00	42.6	42.5	0.34	9.76	9.74	7.80	8.31
1502 1503	68.6	69.4	0.40	-2.3	-1.2	0.00	35.5	35.2	0.28	10.89	10.87	7.00	7.46
1503	66.2 68.7	67.0 69.5	0.39	-2.3	-1.2 1.3	0.00	30.3	29.9	0.24	10.71	10.69	7.19	7.66
1504	70.5	71.3	0.40	-2.3 -2.3	-1.2 -1.2	0.00	28.5	28.1	0.23	10.60	10.58	7.15	7.62
1505	70.5 66.9	71.3 67.7	0.41 0.39	-2.3 -2.3	-1.2 -1.2	0.00	25.5	25.0 23.0	. 0.20	11.24	11.23	6.66	7.10
.000	00,0	01.1	0.03	-2.3	-1.2	0.00	24.4	23.9	0.19	11.34	11.33	6.71	7.15
Ave	70.8	71.7	0.42	-1.9	-0.8	0.00							i

9/13													
Time (1-min)	NOx (ppm)	NO (ppm Cor.)	x (lb/hr)	CO (ppm)	CO (ppm Cor.)	(lb/hr)	SO2 (ppm)	(ppm Cor.)	12 (lb/hr)	O2 (%)	O2 (% Cor.)	CO2 (%)	CO2 (% Cor.)
1722	76.9	78.0	0.46	0.1	0.0	0.00	4.2	4.0	0.03	11.91	11.90	6.07	6.48
1723 1724	77.1 82.7	78.2 83.9	0.46 0.50	0.3 0.3	0.2 0.2	0.00	5,6 20.5	5.4 20.1	0.04 0.17	13.22 9.69	13.22 9.57	5.28 8.13	5.61 8.68
1726 1728	106.0 67.0	107.5 57.8	0.64 0.34	-0.1 0.0	-0.1 -0.1	0.00 0.00	39.7 27.5	39.1 27.0	0.32 0.22	9.72 10.63	9.70	7.81 7.09	8.34 7.57
1727 1728	68.3 63.1	59.1 64.0	0.35 0.38	-0.1 -0.1	-0.1 -0.1	0.00 0.00	19.0 17.5	18.6 17.1	0.15 0.14	10.86 10.85	10.96 10.84	6.80 6.89	7.38 7.36
1729 1730	83.1 66.6	64.0 68.5	0.38 0.40	-0.1 0.1	-0.1 0.0	0.00	16.0	15.7 14.1	0.13 0.12	11.50 11.51	11.49 11.60	6.38 6.52	6.81 6.86
1731 1732	68.3 66.1	69.3 67.0	0.41 0.40	0.2 0.3	0.2 0.3	0.00	15.0 15.7	14.7	0.12 0.13	11.17	11.16	6.66	7.11
1733	70.6	71.6	0.43	0.4	0.4	0.00	16.2	15.4 15.9	0.13	11.66 11.83	11.65 11.82	6.27 6.27	6.69 6.69
1734 1735	67.4 74.7	68.3 76.7	0.41 0.46	0.6 0.6	0.6 0.6	0.00 0.00	16.1 14.6	16.8 14.3	0.13 0.12	11.38 11.47	11.37 11.46	6.60 6.38	6.93 6.81
1736 1737	72.1 74.5	73.1 75.5	0.43 0.45	0.6	0.6 0.3	0.00	13.2 12.5	12.9 12.2	0.11 0.10	12.22 11.91	12.21 11.90	5.89 6.18	6.28 6.59
1738 1739	74.7 70.7	76.7 71.7	0.45 0.43	0.5 0.5	0.5 0.4	0.00	12.7 16.8	12,4 16.5	0.10 0.14	11.88 12.13	11,85 12,12	6.13 6.97	6.54
1740 1741	64.5 55.2	65.4 58.0	0.39	0.6	0.6	0.00	21.2	20.8	0.17	10.85	10,84	7.09	6.37 7.67
1742 1743	54.0	54.8	0.33	0.2 0.2	0.2 0.2	0.00 0.00	25.4 23.6	25.0 23.2	0.21 0.19	9.80 10.65	9.78 10.64	7.70 7.04	8.22 7.62
1744	60.9 60.0	61.7 60.8	0.37 0.36	0.3 0.6	0.2 0.4	0.00	19.8 21.0	19.4 20.6	0.16 0.17	11.23 10.77	11.22 10.76	6.76 6.99	7.22 7.46
1745 1746	63.6 67.6	64.4 68.6	0.38 0.41	0.3 0.3	0.2 0.2	0.00	20.5 18.3	20.1 18.0	0.17 0.15	11.21 11.67	11.20 11.66	6,61 6,42	7.06 6.86
1747 1748	66.0 67.6	67.0 68.6	0.40 0.41	0.3 0.3	0.3 0.3	0.00 0.00	18.8 18.4	18.4 18.0	0.15 0.15	11.10 11.68	11.09 11.67	6.71 6.26	7.16 6.68
1749 1750	71.8 69.4	72.8 70.4	0.43	0.3 0.3	0.3	0.00	16.8	16.4	0.14	11.77	11.76	6.33	6.76
1761 1762	69.1	60.0	0.36	0.3	0.3	0.00	18.9 28.1	18.6 27.6	0.16 0.23	11.23 10.28	11.22 10.27	6.61 7.23	7.05 7.72
1763	47.7 45.1	48.4 45.7	0.29 0.27	0.3 0.3	0.2 0.3	0.00	35.7 33.4	35.1 32.8	0.29 0.27	9.80 9.33	9.78 9.31	7.60 7.81	8.11 8.34
1764 1766	62.3 72.4	63.2 73.4	0.38 0.44	0.2 0.4	- 0.1 0.3	0.00	23.6 19.6	23.2 19.2	0.19 0.16	11.50 12.17	11.49 12.16	6.33 6.08	6.76 6.49
1758 1757	65.2 67.6	68.1 68.3	0.39 0.35	0.3 -0.1	0.3 -0.1	0.00	20.4 31.1	20.0 30.6	0.17 0.25	10.88 9.66	10.87 9.64	7.17 8.03	7.66
1768 1769	55.7 60.4	66.4 61.2	0.34	0.0	0.0 -0.2	0.00	29.0	28.5	0.24	9,64	9.62	7.98	8,67 8,52
1800	59.9	8.03	0.36	0.0	0.0	0.00	27.7 23.8	27.2 23.4	0.23 0.19	9,49 10,49	9.47 10.48	7.86 7.31	8.39 7.80
1801 1802	53.7 53.0	64.6 63.8	0.32 0.32	0.0	-0.1 -0.1	0.00 0.00	22.6 22.0	22.2 21.6	0.1B 0.18	10.09 10.77	10.08 10.76	7.47 6.93	7.98 7.40
1803 1804	65.6 63.9	56.3 54.6	0.33 0.32	0.0 0.1	-0.1 0.0	0.00 0.00	18.7 18.5	18.3 18.1	0.15 0.15	11.29 10.73	11.28 10.72	6.70 6.98	7.15 7.45
1805 1806	67.6 68.3	58.3 59.1	0.35 0.35	0.0 0.0	-0.1 0.0	0.00	18.8	18.4 16.0	0.15 0.13	10.97	10.95	6.73	7.18
1807	56.7	67.6	0.34	0.1	0.0	0.00	16.4	16.0	0.13	11.08	11.69 11.07	6.36 6.70	6.79 7.15
1808 1809	62.9 63.9	63.8 64.8	0.38 0.39	0.0 0.1	0.0 0.1	0.00 0.00	15.9 14.9	15.5 14.6	0.13 0.12	11.31 11.92	11.30 11.91	6.47 6.12	6.91 6.53
1810 1811	67.1 68.2	68.0 69.2	0.40 0.41	0.1 0.2	0.0 0.1	0.00	14.5 15.4	14.2 15.0	0.12 0.12	11.48 11.84	11.47 11.83	6.46 6.19	6.89 6.60
1812 1813	59.0 49.0	69.8 49.7	0.36 0.30	0.4 0.1	0.4 0.0	0.00	23.9 25.8	23.5 25.4	0.19 0.21	10.43 10.02	10.42 10.00	7.44 7.61	7.94 8.13
1814 1815	67.9 56.4	58.8 57.2	0.35 0.34	0.0	0.0 -0.1	0.00	24.6 24.2	24.2 23.8	0.20	10.74	10.73	7.01	7.48
1816	64.5	55.2	0.33	-0.1	-0.1	0.00	26.3	26.8	0.20 0.21	11.38 10.87	11.37 10.86	6.68 6.96	7.13 7.43
1817 1818	62.0 59.7	62.8 60.8	0.37 0.38	-0.1 0.0	-0.2 -0.1	0.00	25.4 23.5	25.0 23.1	0.21 0.19	10.97 11.78	10.96 11.77	6.82 6.23	7.28 6,65
1819 1820	65.8 62.0	66.7 62.8	0.40 0.37	0.0	0.0 0.0	0.00	22.2 28.5	21.8 26.0	0.18 0.21	11.48 10.75	11.47 10.74	6.55 6.97	6.99 7.44
1821 1822	47.2 45.6	47.8 48.2	0.28 0.27	0.1 0.2	0.1 0.1	0.00	42.3 42.4	41.7 41.7	0.34 0.35	10.16 9.30	10.15	7.31	7.80
1823	47.6	48.3	0.29	0.1	0.1	0.00	41.2	40.6	0.33	10.02	10.00	7.93 7.30	8.47 7.79
1824 1825	61.2 62.7	62.0 63.6	0.37 0.38	0.1 0.2	0.1 0.1	0.00 0.00	27.4 23.4	27.0 23.0	0.22 0.19	11.78 11.44	11.76 11.43	6.31 6.45	6.73 6.88
1826 1827	71.6 70.7	72.6 71.7	0.43 0.43	0.1 0.4	0.1 0.3	0.00 0.00	23.0 23.4	22.6 23.0	0.19 0.19	11.52 12.69	11.51 12,69	6.37 5.68	6.79 6.04
1828 1829	74.9 68.5	75.9 69.5	0.45 0.41	0.8 0.1	0.7 0.1	0.00	23.0 25.2	22.6 24.7	0.19 0.20	10.86 10.68	10.95 10.67	6.99 7.06	7.48 7.64
1830 1831	71.4 63.0	72.4 63.9	0.43	0.1 0.2	0.0	0.00	24.0 36.0	23.5 36.4	0.19	11.28 10.29	11.27	6.69	7.03
1832 1833	64.1	54.9	0.33	0.2	0.1	0.00	45.4	44.7	0.37	9.21	10.28 9.19	7.42 7.89	7.92 8.42
1834	54.6 53.5	65.3 64.2	0.33 0.32	0.1 0.2	0.1 0.2	0.00 0.00	44.8 48.8	44.1 48.1	0.36 0.40	10.02 9.15	10.00 9.13	7.46 8.02	7.97 8.66
1836 1836	54.6 59.6	65.3 60.6	0.33 0.38	0.2 0.2	0.1 0.1	0.00	50.0 37.6	49.3 37.0	0.41 0.31	9.83 11.10	9.81 11.09	7.48 6.80	7.99 7.26
1837 1838	63.8 69.7	64.7 70.7	0.38 0.42	0.1 0.1	0.1 0.0	0.00	38.2 35.0	35.6 34.4	0.29 0.28	10.87 11.00	10.86 10.99	6.91 6.76	7.37 7.22
1839 1840	64.8 68.0	85.7 68.9	0.39 0.41	0.1 0.1	0.0 0.1	0.00	30.2 29.1	29.7 28.6	0.26	11.74	11.73	6.33	6.76
1841	70.2	71.2	0.42	0.0	0.0	0.00	30.2	29.7	0.24 0.25	11.10 10.98	11.09 10.97	6.78 6.80	7.24 7.26
1842 1843	68.9 72.6	69.8 73.5	0.41 0.44	0.1 0.2	0.0 0.2	0.00 0.00	29.3 31.2	28.8 30.6	0.24 0.26	11.68 11.69	11.65 11.68	6.31 6.49	6.74 6.92
1844 1845	63.4 58.6	64.3 57.3	0.38 0.34	0.3 0.0	0.2 0.0	0.00 0.00	33.1 42.1	32.6 41.5	0.27 0.34	9.92 9.91	9.90 9.89	7.73 7.66	8.25 8.18
1846 1847	53,0 51,4	53.8 52.1	0.32 0.31	0.1 0.1	0.1 0.0	0.00	40.1 43.3	39.4 42.8	0.33 0.35	10.12 9.59	10.11	7.65 7.87	8.17 8.40
1848 1849	61.4 63.1	52.1 53.9	0.31 0.32	0.0 0.1	0.0 0.0	0.00	41.9 42.0	41.2 41.4	0.34	10.57 9.87	10.68 9.86	7.22	7.71
850 851	58.2 68.4	59.0	0.36	0.1	0.1	0.00	42.7	42.0	0.36	10.11	10.10	7.74	9.26 7.94
852	61.2	69.2 62.0	0.36 0.37	0.1	0.0 0.0	0.00	39.7 39.3	39.0 38.7	0.32 0.32	10.89 10.19	10.88 10.18	7.03 7.45	7.51 7.95
863 864	65.8 64.5	66.7 65.4	0.40 0.39	0.1 0.1	0.0 0.1	0.00	38.8 36.0	38.2 35.4	0.32 0.29	10.54 10.90	10.53 10.89	7.12 7.01	7.60 7.48
1866 1866	64.8 68.1	65.7 69.1	0.39 0.41	0.1 0.1	0.1 0.0	0.00	36.6 36.0	36.0 35.4	0.30 0.29	10.29 10.70	10.28 10.69	7.33 6.99	7.83 7.46
857 858	68.7 67.4	67.6 68.4	0.40 0.41	0.1 0.2	0.1 0.1	0.00	33.1 32.1	32.6 31.6	0.27 0.26	11.16 10.63	11.15 10.52	6.80 7.14	7.26
859 800	68.8	69.7	0.41	0.4	0.4	0.00	31.8	31.3	0.26	11.81	11.80	6.34	7.62 6.76
901	90.3 78.7	91.6 79.8	0.54 0.47	0.4	0.4	0.00	56.6 70.0	55.8 69.0	0.46 0.57	9.27 9.14	9.25 9.12	8.63 8.63	9.22 9.22
902 903	66.0 63.7	66,8 64.6	0.34 0.32	-0.1 0.0	-0.1 -0.1	0.00	60.2 45.0	59.4 44.3	0.49 0.37	9.34 10.57	9.32 10.66	8.17 7.41	8.72 7.91
1904 1905	66.1 67.1	55.8 57.9	0.33 0.34	0.0	0.0	0.00	40.2 36.6	39.6 36.0	0.33	10.03 10.95	10.02 10.94	7.65 6.95	8.17 7.42
908 907	62.0 63.9	62.8	0.37	0.1	0.1	0.00	32.3	31.8	0.26	10.85	10,84	7.11	7.59
908	63.1	64.8 64.0	0.38	0.0	0.0 0.1	0.00	33.1 30.3	32.5 29.8	0.27 0.25	10.58 11.48	10.57 11.47	7.14 6.56	7.62 7.00
909 910	65.9 69.2	66.9 70.2	0.40 0.42	0.2 0.1	0.2 0.1	0.00 0.00	29.6 30.8	29.1 30.3	0.24 0.25	11.01 10.98	11.00 10.95	6.93 6.83	7.40 7.29
911 912	66.6 67.4	67.6 68.3	0.40 0.41	0.2 0.3	0.2 0.2	0.00	28.6 27.6	28.1 27.1	0.23 0.22	11.61 10.97	11.60 10.96	6.51 6.86	6.95 7.33
913 914	70.2 70.6	71.2	0.42	0.2	0.2	0.00	26,7	26.2	0.22	11.57	11.56	6.38	6.81
915	70.6	71.6 71.6	0.43	0.3 0.3	0.2 0.3	0.00	24.5 27.2	24.0 26.7	0.20 0.22	11.75 11.22	11.74 11.21	6.38 6.69	6.81 7.14
916 917	65.8 78.4	66.8 79.6	0.40 0.47	0.9 0.3	0.8 0.2	0.00	33.9 56.9	33.4 56.0	0.28 0.48	10.82 8.99	10.81 8.97	7.18 8,62	7.67 9.21
918 919	65.2 68.0	68.8	0.33 0.36	0.1 0.1	0.0	0.00	51.6 41.6	50.9 41.0	0.42	9.33	9.31	8.13	8.68
920	67.2	67.9	0.34	0.1	0.1	0.00	39.9	39.3	0.34 0.32	10.26 9.81	10.25 9.79	7.61 7.77	8.13 8,30
921 922	63.6 67.7	54.3 58.5	0.32 0.35	0.2 0.3	0.1 0.3	0.00	35.4 31.7	34.9 31.1	0.29 0.26	11.00 10.62	10.99 10.61	6.95 7.27	7.42 7.76
923 924	60.7 68.9	61.5 59.8	0.37 0.36	0.3 0.3	0.3 0.2	0.00	31.8 28.2	31.3 27.7	0.26 0.23	10.78	10.77	7.00 6.78	7.47 7.21
926	62.0 64.8	62.9 65.7	0.37	0.3 0.3	0.3	0.00	27.5	27.0	0.22	10.78	10,77	7.02	7.49
		67.5	0.39	0.3	0.3		27.1	26.6	0.22	11.44	11.43	6.51	6.95
926 927 928	66.6 67.2	68.1	0.40	0.4	0.4 0.3	0.00	24.5 24.8	24.0 24.3	0.20	11.41 10.85	11.40 10.94	6.64 6.85	7.09 7.32

09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	со
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	910	16.60	15.45	19.9	13.1	-3.4	30.6	10.9
2013	272	911	0.05	0.10	100.6	228.5	4.7	225.2	99.3
2013	272	912	0.02	0.06	100.6	238.1	0.9	237.2	100.3
2013	272	913	0.01	0.05	100.6	236.9	1.1	235.9	100.3
2013	272	914	0.01	0.04	99.2	195.8	-1.5	208.3	100.3
2013	272	915	0.00	0.03	89.5	93.7	1.2	92.5	94.7
2013	272	916	0.00	0.03	90.7	91.7	0.4	91.0	92.8
2013	272	917	1.12	1.56	86.5	86.7	-1.0	90.9	91.7
2013	272	918	19.89	19.32	5.7	5.2	-1.7	12.1	21.0
2013	272	. 919	20.06	19.38	0.3	0.0	-0.1	0.0	0.1
2013	272	920	20.07	19.39	0.1	0.0	-0.1	-0.1	0.0
2013	272	921	17.93	16.86	0.3	0.0	-0.1	-0.1	0.1
2013	272	922	10.07	9.65	0.1	-0.1	-0.1	0.0	0.9
2013	272	923	9.04	6.82	1.7	0.3	-1.3	1.4	4.1
2013	272	924	0.51	0.07	33.1	29.2	-1.2	30.2	41.3
2013	272	925	0.01	0.04	44.2	44.0	0.4	43.7	47.2
2013	272	926	0.00	0.03	44.9	44.6	0.4	44.4	47.2
2013	272	927	16.26	0.07	13.7	13.1	-3.8	20.0	23.0
2013	272	928	20.97	0.07	0.3	0.0	-0.1	0.0	23.0 2.7
2013	272	929	20.98	0.07	0.1	-0.1	-0.1	0.0	2.7
2013	272	930	20.95	0.09	1.3	0.0	0.0	-0.1	2. <i>1</i> 2.7
2013	272	931	1.75	0.17	81.3	64.6	-4.2	79.7	2. <i>1</i> 67.2
2013	272	932	0.09	0.02	89.9	90.4	0.1	90.1	
2013	272	933	0.07	0.02	89.8	90.4	0.1	90.1	91.4
2013	272	934	0.06	0.01	47.6	58.3	7.3	50.8	91.3
2013	272	935	0.04	0.01	45.3	45.4	7.3 0.4	44.9	59.3
2013	272	936	0.04	0.00	45.4	45.4	0.4	44.9 44.9	46.4
2013	272	937	0.03	0.00	45.4 45.4	45.8	0.4		46.3
2013	272	938	5.30	5.26	25.2	28.5	0.4	45.3	46.2
2013	272	939	10.05	9.53	0.8	0.2	-0.1	27.3	32.7
2013	272	940	10.06	9.55 9.55	0.5	0.2		0.1	0.3
2013	272	941	10.07	9.55	0.5	0.0	-0.1 -0.1	0.0	-0.6
2013	272	942	10.15	9.34	0.9	2.6	2.5	-0.1 -0.1	-0.7
2013	272	943	13.24	5.09	13.2	58.7	6.1	-0.1 69.8	-0.9
2013	272	944	13.30	5.04	8.5	70.4	-0.1 -3.2	76.4	-0.2 0.0
2013	272	945	13.28	5.05	5.5	70.4	-3.2 -3.5	76. 4 76.9	
2013	272	946		5.04	3.9	70.8	-3.5 -1.1	73.3	-0.1
2013	272	947	13.34			73.1	2.2	71.0	-0.2 -0.4
2013	272	948	13.25	5.09		77.4	6.2	71.0	-0. 4 -0.6
2013	272	949	13.32	5.04	2.1	73.8	1.7	72.0	-0.6 -0.7
2013	272	950	13.29	5.06	1.9	70.4	-2.8	76.2	-0. <i>1</i> -0.8
2013	272	951	13.31	5.05	1.7	69.9	-4.6	77.6	-0.8 -1.0
2013	272	952	13.30	5.05	1.6	69.7	-3.0	75.6	-1.0
2013	272	953	13.30	5.05	1.5	70.7	-1.0	73.4	-1.0 -1.1
2013	272	954	13.33	5.03	1.5	72.1	1.8	70. 1 70.1	-1.2
2013	272	955	13.37	4.99	1.3	74.4	4.5	69.9	-1.2 -1.3
2013	272	956	14.40	4.37	1.1	72.5	13.3	58.9	-1.3 2.5
2013	272	957	13.38	5.07	1.1	66.8	8.7	58.0	1.2
2013	272	958	11.56	6.13	1.4	61.8	4.8	56.8	-1.6
2013	272	959	11.58	6.11	1.4	57.5	-0.5	58.1	-1.8 -1.8
2013	272	1000	11.52	6.15	1.4	55.1	-4.8	60.9	-1.0 -2.0
2013	272	1001	11.73	5.98		57.9	1.6		
2013	272	1002	11.90	5.91	1.2	57.5	0.8	56.2 56.4	-2.0
2013	272	1002	11.74	6.07		57.5 55.9			-2.1
2013	272	1003	11.59		1.1	55.9 54.9	-0.1 -2.1	56.8	-2.1
2013	272	1005	11.59	6.11	1.2	54.9 54.7	-2.1 -2.5	56.9 57.7	-2.2
2013	272	1006	11.58		1.2	60.6	-2.5 5.1		-2.2
	~	1000	11.50	0.11	1.1	00.0	3 . 1	55.3	-2.3

09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1007	11.70	6.04	1.0	54.6	-4.5	60.2	-2.3
2013	272	1008	11.67	6.02	1.0	55.7	-2.3	57.7	-2.3
2013	272	1009	11.96	5.87	1.1	58.1	2.9	55.2	-2.3
2013	272	1010	11.98	5.90	1.0	54.7	-1.1	56.5	-2.3
2013	272	1011	11.69	6.07	1.0	55.8	-0.1	56.1	-2.3
2013	272	1012	11.61	6.10	1.1	55.1	-2.6	57.9	-2.3
2013	272	1013	11.66	6.06	1.1	56.7	1.5	55.0	-2.3
2013	272	1014	11.64	6.07	1.1	59.5	4.1	55.2	-2.3
2013	272	1015	11.71	6.03	0.9	54.7	-4.5	60.1	-2.3
2013	272	1016	11.89	5.88	0.9	56.6	1.3	55.3	-2.3
2013	272	1017	12.00	5.86	0.9	56.6	1.4	55.1	-2.3
2013	272	1018	11.91	5.96	0.8	55.3	0.4	56.3	-2.3
2013	272	1019	11.72	6.04	0.9	56.3	1.1	55.1	-2.3
2013	272	1020	11.69	6.05	0.9	54.5	-3.3	58.4	-2.3
2013	272	1021	11.67	6.07	1.0	55.8	-0.2	55.8	-2.3 -2.3
2013	272	1022	11.62	6.09	0.9	56.5	-0.2 -1.1	55.6 57.6	-2.3
2013	272	1023	11.77	5.96	0.9	55.1	-2.2	57.3	-2.3 -2.3
2013	272	1024	11.90	5.90	1.0	58.0	2.6	57.3 55.1	-2.3 -2.3
2013	272	1025	12.10	5.82	0.9	55.2	0.5	54.4	
2013	272	1026	11.77	6.03	0.9	54.6	-0.3	55.8	-2.3
2013	272	1027	11.68	6.05	0.9	54.4	-0.3 -3.8		-2.3
2013	272	1028	11.68	6.05	0.8	54.4 57.9	-3.6 2.8	59.5	-2.3
2013	272	1029	11.68	6.05	0.8	57.9 56.8		55.2 50.5	-2.3
2013	272	1030	11.85	5.90			0.4	56.5	-2.3
2013	272	1030	12.07	5.80	0.9	54.7	-2.8	57.8	-2.3
2013	272	1031	11.83		0.9	57.3 55.7	2.8	54.4	-2.3
2013	272	1032	11.73	6.00 6.01	0.8	55.7	1.0	55.7	-2.3
2013	272	1033			0.8	54.2	-2.5	56.7	-2.3
2013	272	1034	11.72 11.71	6.02	0.8	54.6	-2.9	58.3	-2.3
2013	272	1035	11.71	6.02	0.9	57.3	2.1	55.0	-2.3
2013	272	1036	11.75	6.00 5.89	0.9	58.5	3.7	54.6	-2.3
2013	272	1037	12.10		0.9	53.5	-5.0	59.6	-2.3
2013	272	1038		5.77	0.9	57.7	3.1	54.5	-2.3
2013	272	1039	11.99	5.91	0.9	54.7	0.6	54.9	-2.3
2013	272	1040	11.69	6.05	0.8	54.6	-0.8	55.3	-2.3
2013			11.76	6.00 6.01	0.9	53.6	-2.6	57.2	-2.3
2013	272 272	1042 1043	11.76		1.0	59.5	5.1	54.4	-2.3
2013	272	1043 1044	11.74	6.01	1.0	55.0	-2.3	57.5	-2.3
2013	272	1044	11.89 12.01	5.88	0.9	55.1 57.0	-0.6	55.5	-2.3
2013	272	1045	11.93	5.83	0.9	57.8 55.0	3.1	54.8	-2.3
2013	272	1046	11.93	5.90 5.98	0.8 0.9	55.2 55.9	-1.2	56.6	-2.3
2013	272	1047				00.0	1.4	55.4	-1.2
2013	272	1048	11.76	5.99 5.98	0.8 0.9	53.4	-3.0	56.4	0.3
2013	272	1049	11.79			53.7	-2.9	57.2	0.2
2013	272 272	1050	11.83	5.95	1.9	56.8	3.1	53.7	0.1
2013	272 272	1051	11.81	5.96	3.9	55.5	0.3	55.0	0.1
2013	272 272		12.08	5.76	3.6	52.2	-4.1	56.8	0.1
		1053	12.24	5.71	3.2	55.7	2.5	53.4	0.1
2013	272	1054	11.97	5.92	2.8	53.9	0.0	54.7	0.1
2013	272	1055	11.89	5.93	2.6	52.7	-1.4	54.0	0.1
2013	272	1056	11.89	5.91	2.5	53.3	-2.5	56.5	0.1
2013	272	1057	12.00	5.85	2.5	56.5	3.3	53.1	0.0
2013	272	1058	11.86	5.94	2.3	56.7	2.5	53.9	-0.1
2013	272	1059	11.86	5.91	2.3	53.8	-4.0	58.6	-0.1
2013	272	1100	12.23	5.68	2.2	55.1	1.8	53.2	-0.1
2013	272	1101	12.19	5.75	2.1	55.2	1.7	53.4	-0.1
2013	272	1102	12.01	5.89	2.1	54.6	0.9	54.3	-0.1
2013	272	1103	11.84	5.95	2.0	54.3	-0.7	54.6	-0.2

09/29/13	3								
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1104	11.86	5.93	2.0	53.1	-3.8	57.9	-0.2
2013	272	1105	11.83	5.95	2.0	55.3	0.7	54.5	-0.2
2013	272	1106	11.98	5.86	1.9	56.1	2.7	53.2	-0.2
2013	272	1107	12.79	5.58	2.6	56.5	-3.4	62.7	-0.2
2013	272	1108	9.06	8.80	52.1	177.7	-3.3	187.2	-0.6
2013	272	1109	11.13	7.32	48.3	189.8	-1.5	191.2	0.4
2013	272	1110	10.62	7.55	57.8	192.3	1.4	190.9	0.7
2013	272	1111	10.92	7.25	49.1	171.2	-1.0	172.0	1.1
2013	272	1112	10.73	7.35	40.3	144.6	2.1	142.4	2.4
2013	272	1113	10.70	7.25	36.8	116.8	2.2	114.8	3.8
2013	272	1114	9.62	7.95	33.0	81.4	-4.9	86.8	
2013	272	1115	9.35	7.97	25.3	58.1	1.6	56.4	4.5 1.7
2013	272	1116	10.13	7.46	18.5	47.8	1.6	46.4	
2013	272	1117	10.02	7.49	14.1	46.9	-4.5		-0.2
2013	272	1118	10.54	7.49 7.06	14.1	52.0		51.4	-0.3
2013	272	1119	11.62	6.35			2.0	50.0	-0.5
2013	272	1120	11.53		10.1	51.6	-0.7	52.3	-0.5
2013	272	1121		6.44	8.7	56.3	1.0	55.0	-0.4
2013	272	1121	11.70	6.24	8.3	57.7	-3.1	61.6	-0.4
2013	272 272	1122	11.98	6.05	7.9	64.9	3.3	61.5	-0.4
2013			12.31	5.81	8.4	56.5	-7.8	65.4	-0.2
	272	1124	12.13	6.18	8.9	54.2	-1.3	55.4	1.3
2013	272	1125	9.23	8.06	13.6	43.8	-3.4	47.0	0.1
2013	272	1126	9.88	7.51	15.7	44.3	-1.6	45.7	-0.4
2013	272	1127	10.38	7.27	15.1	46.2	1.4	44.6	-0.4
2013	272	1128	9.98	7.45	15.4	45.7	-3.7	49.3	-0.5
2013	272	1129	10.22	7.23	16.2	51.0	1.7	49.1	-0.6
2013	272	1130	10.98	6.74	15.3	49.9	-2.0	51.7	-0.6
2013	272	1131	10.59	7.03	13.4	51.4	-0.6	51.9	-0.5
2013	272	1132	10.57	6.98	13.2	53.5	0.6	52.6	-0.6
2013	272	1133	11.13	6.57	12.4	51.2	-4.1	55.2	-0.6
2013	272	1134	10.87	6.83	12.1	54.5	2.7	51.8	-0.6
2013	272	1135	10.60	6.95	12.2	53.2	-1.1	54.2	-0.6
2013	272	1136	11.16	6.51	12.2	53.0	-3.9	56.8	-0.7
2013	272	1137	11.23	6.57	11.2	55.5	3.5	51.7	-0.6
2013	272	1138	10.93	6.70	10.7	51.9	-3.9	55.6	-0.6
2013	272	1139	11.22	6.51	10.8	53.7	-1.4	55.1	-0.7
2013	272	1140	10.41	7.89	22.7	64.1	2.0	61.9	-0.7
2013	272	1141	9.77	8.46	42.8	108.5	-0.7	108.9	-0.6
2013	272	1142	9.38	8.26	32.9	61.4	-0.4	61.8	-0.8
2013	272	1143	9.87	7.93	21.5	50.8	1.2	49.4	-1.0
2013	272	1144	10.06	7.66	18.7	55.4	0.6	54.7	-1.0
2013	272	1145	11.23	6.87	16.3	53.0	-3.8	56.6	-1.0
2013	272	1146	10.83	7.15	13.6	55.8	-2.6	58.3	-1.0
2013	272	1147	11.12	6.82	12.8	62.5	2.2	60.0	-1.1
2013	272	1148	11.96	6.27	12.0	60.5	-3.5	63.8	-1.0
2013	272	1149	11.61	6.53	11.4	65.5	1.7	63.6	-0.9
2013	272	1150	11.50	6.51	10.9	66.2	-2.9	69.8	-1.0
2013	272	1151	11.99	6.13	10.6	69.3	-1.9	71.2	-1.0
2013	272	1152	10.83	7.04	12.1	61.6	3.6	57.9	-0.8
2013	272	1153	10.09	7.38	13.0	57.4	-3.2	60.7	-1.0
2013	272	1154	10.61	6.96	12.4	63.0	-0.8	63.7	-1.1
2013	272	1155	10.99	6.82	11.1	66.8	3.1	63.6	-1.0
2013	272	1156	11.93	6.20	9.8	62.9	-5.2	68.8	0.7
2013	272	1157	10.76	6.90	10.2	60.9	3.1	57.8	-0.9
2013	272	1158	11.19	6.61	11.1	57.0	-4.7	61.6	-1.2
2013	272	1159	10.40	7.25	13.2	61.9	1.3	60.4	-1.3
2013	272	1200	9.85	7.54	16.8	63.0	-0.3	63.0	-1.4

09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	СО
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1201	10.49	7.08	18.5	59.8	-4.0	63.6	-1.5
2013	272	1202	9.95	7.53	18.7	61.5	1.3	59.9	-1.4
2013	272	1203	9.98	7.40	18.4	62.7	1.6	61.1	-1.5
2013	272	1204	10.84	6.85	17.1	59.1	-4.0	62.9	-1.5
2013	272	1205	10.32	7.27	16.0	61.2	1.1	60.1	-1.4
2013	272	1206	10.33	7.18	15.9	62.6	0.2	62.2	-1.4 -1.4
2013	272	1207	11.28	6.49	15.1	61.0	-3.8	64.7	-1.4 -1.4
2013	272	1208	11.56	6.41	13.1	67.3	4.7	62.4	-1. 4 -1.4
2013	272	1209	11.47	6.38	12.8	66.8	-4.7 -4.7	71.9	
2013	272	1210	11.92	6.03	12.4	72.0			-1.4
2013	272	1211	11.64	6.32	13.4	60.4	2.4	69.5	-1.4
2013	272	1212	11.17	6.55	13.4		0.1	60.3	-1.0
2013	272	1212	9.12	8.88		55.6	-1.0	56.3	-1.3
2013	272	1213			68.2	187.2	-5.7	224.2	59.6
2013			11.65	7.12	36.6	124.3	-7.1	133.5	31.3
2013	272	1215	10.14	7.87	32.9	74.2	-3.2	77.4	0.6
	272	1216	9.78	7.91	24.1	54.3	2.3	51.9	-0.6
2013	272	1217	10.55	7.40	17.9	52.9	-1.7	54.4	-1.3
2013	272	1218	10.08	7.62	14.9	57.4	-4.1	61.4	-1.6
2013	272	1219	11.24	6.75	13.2	59.3	-3.4	62.6	-1.6
2013	272	1220	11.29	6.77	10.9	65.6	4.1	61.4	-1.5
2013	272	1221	11.24	6.66	9.9	63.6	-1.5	64.9	-1.5
2013	272	1222	12.20	5.97	9.1	60.5	-6.0	67.1	-1.5
2013	272	1223	11.99	6.19	8.6	66.8	4.9	61.9	-1.4
2013	272	1224	11.90	6.15	8.7	66.6	-4.2	71.6	-1.4
2013	272	1225	11.00	6.75	11.3	65.7	1.3	64.3	-1.5
2013	272	1226	10.64	7.02	11.9	60.5	1.9	58.4	-1.5
2013	272	1227	10.30	7.15	12.1	8.06	-2.0	62.8	-1.6
2013	272	1228	11.16	6.54	11.8	62.5	-3.1	65.4	-1.5
2013	272	1229	10.94	7.12	15.4	65.8	-0.6	66.4	-1.3
2013	272	1230	9.80	8.04	39.0	116.2	-4.1	120.4	-1.9
2013	272	1231	10.77	7.43	38.6	120.8	-2.0	122.6	-1.7
2013	272	1232	10.18	7.79	39.6	116.8	0.1	116.6	-1.8
2013	272	1233	9.82	8.01	39.3	100.6	-4.6	105.9	-1.1
2013	272	1234	9.76	7.89	39.7	78.4	-2.9	81.2	0.3
2013	272	1235	9.28	8.25	33.7	60.0	-0.4	60.3	-0.7
2013	272	1236	9.09	8.14	32.5	50.1	-0.4	50.3	-1.8
2013	272	1237	10.46	7.33	25.1	51.1	-0.5	51.5	-2.1
2013	272	1238	10.02	7.53	20.8	54.3	-2.0	56.2	-2.1
2013	272	1239	10.65	7.04	19.2	56.2	-Ò.5	56.5	-2.1
2013	272	1240	10.89	6.99	16.8	55.9	1.5	54.2	-2.0
2013	272	1241	10.48	7.16	16.6	55.9	-2.9	58.8	-2.1
2013	272	1242	11.41	6.51	16.1	56.1	-4.7	60.7	-2.0
2013	272	1243	10.88	6.94	14.6	59.9	2.9	56.9	-2.0
2013	272	1244	11.04	6.74	14.6	62.4	3.2	59.4	-2.1
2013	272	1245	4.02	2.08	44.1	67.7	5.9	61.8	35.2
2013	272	1246	0.09	0.05	84.0	91.1	0.3	90.9	87.2
2013	272	1247	0.08	0.02	87.3	91.0	0.4	90.6	90.5
2013	272	1248	0.08	0.01	81.1	87.8	-0.1	87.8	89.9
2013	272	1249	0.06	0.01	43.4	49.5	2.0	47.6	50.7
2013	272	1250	0.05	0.00	45.5	45.4	0.4	44.9	45.6
2013	272	1251	5.93	5.85	24.0	21.4	-3.8		
2013	272	1252	10.02	9.50	1.7	0.0	-3.6 -0.1	28.3 0.0	29.7
2013	272	1252	10.02	9.52	1.7	-0.1			-0.7
2013	272	1253	9.86	9.52 9.17	1.5	-0.1 9.6	-0.1	-0.1	0.3
2013	272	1254	13.60	9.17 4.94	4.0		5.2	4.2	0.3
2013	272 272	1255	21.18			44.0	-3.9	54.2	1.3
2013	272 272			0.06	0.6	0.2	-0.3	1.0	2.6
2013	212	1257	21.19	0.04	0.5	-0.1	-0.1	-0.1	2.8

09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1258	21.20	0.03	0.6	-0.1	-0.1	-0.1	2.8
2013	272	1259	21.20	0.03	0.6	-0.1	-0.1	-0.1	2.7
2013	272	1300	21.21	0.03	0.5	-0.1	-0.1	0.0	2.7
2013	272	1301	21.21	0.03	0.5	-0.1	-0.1	-0.1	2.7
2013	272	1302	21.21	0.02	0.5	-0.1	-0.1	0.0	2.6
2013	272	1303	21.21	0.03	0.4	-0.1	-0.1	0.0	2.6
2013	272	1304	21.22	0.02	0.4	0.0	-0.1	-0.1	2.6
2013	272	1305	21.22	0.02	0.4	-0.1	-0.1	-0.1	2.5
2013	272	1306	21.22	0.02	0.5	-0.1	-0.1	-0.1	2.4
2013	272	1307	21.22	0.02	0.5	-0.1	-0.1	-0.1	2.3
2013	272	1308	21.22	0.02	0.5	-0.1	-0.1	0.0	2.3
2013	272	1309	21.22	0.02	0.5	-0.1	-0.1	-0.1	2.2
2013	272	1310	21.22	0.02	0.5	-0.1	-0.1	0.0	2.2
2013	272	1311	21.22	0.01	0.5	-0.1	-0.1	-0.1	2.1
2013	272	1312	21.22	0.01	0.5	-0.1	-0.1	0.0	2.1
2013	272	1313	21.22	0.01	0.5	-0.1	-0.1	-0.1	2.0
2013	272	1314	21.22	0.01	0.4	-0.1	-0.1	0.0	1.9
2013	272	1315	21.22	0.01	0.4	-0.1	-0.1	-0.1	1.9
2013	272	1316	21.22	0.01	0.4	-0.1	-0.1	0.0	1.8
2013	272	1317	21.22	0.01	0.5	-0.1	-0.1	-0.1	1.9
2013	272	1318	21.22	0.01	0.4	-0.1	-0.1	-0.1	1.8
2013	272	1319	21.22	0.01	0.4	-0.1	-0.1	-0.1	1.7
2013	272	1320	21.22	0.01	0.4	-0.1	-0.1	0.0	1.7
2013	272	1321	21.22	0.01	0.4	-0.1	-0.1	-0.1	1.6
2013	272	1322	21.22	0.01	0.5	-0.1	-0.1	-0.1	1.7
2013	272	1323	21.22	0.01	0.5	-0.1	-0.1	-0.1	1.6
2013	272	1324	21.22	0.02	0.5	-0.1	-0.1	-0.1	1.6
2013	272	1325	21.22	0.02	0.4	-0.1	-0.1	-0.1	1.5
2013	272	1326	21.22	0.02	0.4	-0.1	-0.1	0.0	1.5
2013	272	1327	21.22	0.02	0.4	-0.1	-0.1	-0.1	1.5
2013	272	1328	21.22	0.02	0.4	-0.1	-0.1	0.0	1.4
2013	272	1329	21.22	0.02	0.5	-0.1	-0.1	-0.1	1.4
2013	272	1330	21.22	0.02	0.5	-0.1	-0.1	-0.1	1.4
2013	272	1331	21.22	0.02	0.4	-0.1	-0.1	0.0	1.4
2013	272	1332	21.23	0.02	0.4	-0.1	-0.1	-0.1	1.4
2013	272	1333	21.23	0.01	0.5	-0.1	-0.1	-0.1	1.3
2013	272	1334	21.22	0.01	0.4	-0.1	-0.1	-0.1	1.3
2013	272	1335	21.22	0.01	0.5	-0.1	-0.1	-0.1	1.2
2013	272	1336	21.22	0.01	0.4	-0.1	-0.1	0.0	1.3
2013	272	1337	21.22	0.01	0.3	-0.1	-0.1	0.0	1.2
2013	272	1338	21.22	0.01	0.4	-0.1	-0.1	-0.1	1.1
2013	272	1339	21.22	0.01	0.4	-0.1	-0.1	0.0	1.1
2013	272	1340	21.22	0.01	0.3	-0.1	-0.1	-0.1	1.1
2013	272	1341	21.22	0.01	0.4	-0.1	-0.1	0.0	
2013	272	1342	21.22	0.01	0.4	-0.1	-0.1		
2013	272	1343	21.22	0.01	0.4	-0.1	-0.1	0.0	
2013	272	1344	21.22	0.01	0.4	-0.1	-0.1	-0.1	1.0
2013	272	1345	21.22	0.02	0.5	-0.1	-0.1	-0.1	0.9
2013	272	1346	21.21	0.01	0.3	-0.1	-0.1	0.0	0.9
2013	272	1347	21.21	0.01	0.3	-0.1	-0.1	-0.1	0.9
2013	272	1348	21.21	0.01	0.3	-0.1	-0.1	0.0	0.8
2013	272	1349	16.81	3.05	0.9	14.2	-4.9	22.5	0.4
2013	272	1350	10.90	6.86	5.7	61.6	-4.5	66.0	-1.0
2013	272	1351	12.26	6.09	9.0	69.6	0.5	69.1	-0.9
2013	272	1352	9.45	8.19	16.5	59.4	2.3	57.0	-0.9
2013	272	1353	9.88	7.66	21.2	60.4	-0.1	60.3	-1.2
2013	272	1354	10.96	7.02	18.8	60.1	-5.0	65.0	-1.1

09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1355	10.37	7.31	18.9	66.7	3.2	63.6	-1.2
2013	272	1356	10.44	7.18	19.7	65.1	-2.3	67.3	-1.2
2013	272	1357	11.29	6.65	18.8	63.8	-2.6	66.3	-1.2
2013	272	1358	10.71	7.08	18.9	65.0	2.7	62.1	-1.2
2013	272	1359	10.65	7.04	19.1	63.8	-3.4	67.0	-1.2
2013	272	1400	11.18	6.62	18.7	68.4	3.1	65.0	-1.3
2013	272	1401	11.35	6.64	18.3	63.1	-4.9	67.6	-1.3
2013	272	1402	10.85	6.89	18.8	69.4	3.1	66.4	-1.3
2013	272	1403	10.97	6.75	18.1	69.0	-1.1	70.0	-1.4
2013	272	1404	11.68	6.32	16.6	68.5	-1.7	70.0	-1. 4 -1.4
2013	272	1405	11.19	6.72	17.6	69.2	0.5	68.6	-1.4
2013	272	1406	11.01	6.75	18.4	69.9	-4.7	74.7	-1.3 -1.4
2013	272	1407	12.22	5.94	17.4	74.7	3.3	74.7 71.4	-1. 4 -1.2
2013	272	1408	9.67	8.27	29.4	91.7	3.2	88.3	
2013	272	1409	9.59	8.34	36.9	139.8	-1.7		0.8
2013	272	1410	9.76	8.25	40.3			141.3	0.7
2013	272	1411	9.30	8.46		139.9	0.2	139.6	-1.2
2013	272	1412	9.19	8.54	45.5	131.0	2.4	128.4	-1.7
2013	272	1413	8.81		46.4	112.7	-4.5	118.0	-1.7
2013	272	1413	9.52	8.59	45.7	114.2	11.2	102.9	-1.7
2013	272	1415		8.17	37.4	94.6	0.1	95.4	-1.6
2013	272		8.52	8.73	36.5	80.1	3.1	76.9	-1.7
2013	272 272	1416	9.65	7.87	34.0	53.6	-0.1	53.6	-1.7
2013		1417	9.36	8.14	26.7	46.9	0.9	46.0	-1.7
	272	1418	9.58	7.84	26.1	49.6	-2.0	51.7	-1.8
2013	272	1419	10.54	7.29	21.4	49.8	-2.6	52.3	-1.7
2013	272	1420	9.93	7.65	22.3	53.6	2.5	51.3	-1.8
2013	272	1421	10.57	7.13	21.0	55.3	1.1	53.8	-1.8
2013	272	1422	10.77	7.12	18.2	52.1	-3.1	55.0	-1.8
2013	272	1423	10.84	6.99	19.7	57.9	2.1	55.7	-1.6
2013	272	1424	10.79	7.35	26.4	59.2	-3.6	62.6	-1.3
2013	272	1425	9.34	8.23	36.0	70.0	-3.9	74.5	-1.6
2013	272	1426	10.78	7.31	41.5	90.7	-3.6	95.4	-1.2
2013	272	1427	9.23	8.24	48.4	84.0	2.1	82.9	-1.6
2013	272	1428	9.12	8.41	43.2	93.0	0.3	93.0	-1.8
2013	272	1429	8.64	8.51	43.7	82.2	3.2	78.9	-1.9
2013	272	1430	9.66	7.91	37.6	57.9	-1.5	59.3	-2.0
2013	272	1431	9.23	8.14	35.7	46.0	2.3	43.6	-1.9
2013	272	1432	9.53	7.83	33.4	46.4	-1.7	48.1	-2.0
2013	272	1433	10.53	7.22	29.3	47.4	-1.6	48.9	-2.1
2013	272	1434	9.93	7.64	26.5	52.1	2.0	49.9	-2.0
2013	272	1435	10.54	7.10	27.8	53.3	0.1	53.1	-2.0
2013	272	1436	10.75	7.08	22.1	53.6	-2.5	55.9	-2.0
2013	272	1437	10.42	7.19	24.8	58.5	-2.5	60.6	-2.0
2013	272	1438	11.37	6.57	22.1	62.3	0.1	62.0	-2.0
2013	272	1439	11.94	6.28	20.3	58.8	-4.9	64.5	-1.6
2013	272	1440	9.85	8.24	39.5	116.0	1.1	114.6	-1.9
2013	272	1441	9.48	8.30	47.8	100.7	4.4	96.0	-2.1
2013	272	1442	9.02	8.33	45.4	58.1	-1.3	59.2	-2.2
2013	272	1443	10.38	7.33	38.3	55.9	0.4	55.3	-2.3
2013	272	1444	10.51	7.31	32.2	51.4	-2.0	53.5	-2.2
2013	272	1445	10.45	7.20	30.3	55.4	-1.4	56.7	-2.2
2013	272	1446	11.35	6.63	28.6	54.9	0.2	54.6	-2.2
2013	272	1447	10.79	7.05	26.4	56.7	-0.2	56.9	-2.2
2013	272	1448	10.88	6.86	26.0	59.1	-3.2	62.2	-2.2
2013	272	1449	11.63	6.42	26.0	57.3	-0.6	57.7	-2.2
2013	272	1450	11.05	6.80	22.8	61.2	1.3	59.9	-2.2
2013	272	1451	11.06	6.70	22.8	67.1	-4.9	72.5	-2.3

09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1452	11.89	6.13	22.1	73.2	3.2	69.9	-2.2
2013	272	1453	11.84	6.26	19.6	67.5	-5.7	73.5	-2.3
2013	272	1454	11.63	6.31	21.0	74.0	2.8	71.2	-2.2
2013	272	1455	11.33	6.71	25.7	72.6	-2.4	74.9	-1.9
2013	272	1456	9.51	8.27	46.5	103.4	-0.5	104.0	-2.3
2013	272	1457	9.59	8.22	48.0	81.6	-5.7	88.5	-2.3
2013	272	1458	9.09	8.50	46.3	57.5	-1.2	58.7	-2.3
2013	272	1459	9.48	8.04	43.8	51.5	-0.1	51.5	-2.3
2013	272	1500	10.14	7.71	40.5	57.3	-3.3	60.3	-2.3 -2.3
2013	272	1501	9.76	7.80	42.6	65.3	-3.3 -0.6	66.1	
2013	272	1502	10.89	7.00	35.5	68.6	1.2		-2.3
2013	272	1503	10.03	7.19	30.3	66.2		67.4	-2.3
2013	272	1504	10.77	7.1 9 7.15	28.5		-2.0	68.0	-2.3
2013	272	1505	11.24			68.7	-1.0	69.6	-2.3
2013	272	1506	11.2 4 11.34	6.66	25.5	70.5	1.5	68.8	-2.3
2013	272			6.71	24.4	66.9	-4.5	71.4	-2.3
2013	272 272	1507	10.88	6.92	25.0	71.4	1.8	69.5	-2.3
		1508	11.26	6.60	24.6	70.8	-1.1	71.8	-2.3
2013	272	1509	11.76	6.36	20.4	69.5	-1.6	70.9	-2.3
2013	272	1510	11.20	6.68	21.4	72.1	1.7	70.2	-2.3
2013	272	1511	10.47	7.62	39.9	76.6	-2.5	84.0	-2.2
2013	272	1512	10.15	8.12	78.1	140.7	-6.6	149.7	-2.3
2013	272	1513	9.78	7.89	70.3	101.0	-1.4	104.0	-2.3
2013	272	1514	9.91	7.78	50.6	47.7	-3.6	51.3	-2.3
2013	272	1515	9.80	7.69	45.6	47.8	-1.0	48.7	-2.3
2013	272	1516	10.98	6.92	39.8	49.2	1.3	47.7	-2.3
2013	272	1517	10.45	7.28	33.6	51.4	-0.6	52.1	-2.3
2013	272	1518	10.65	7.02	32.4	57.3	-2.8	60.1	-2.3
2013	272	1519	11.58	6.44	28.5	63.3	2.1	60.9	-2.3
2013	272	1520	11.10	6.79	28.4	62.5	-2.1	64.8	-2.3
2013	272	1521	10.98	6.78	28.4	65.5	-1.8	67.1	-2.3
2013	272	1522	11.68	6.28	23.7	69.2	3.0	66.2	-2.3
2013	272 .	1523	11.60	6.43	22.5	64.8	-6.5	71.6	-2.3
2013	272	1524	11.36	6.49	24.9	71.5	3.1	68.5	-2.3
2013	272	1525	11.91	6.07	29.5	69.8	-0.4	70.1	-2.3
2013	272	1526	12.30	5.90	24.8	70.8	0.4	71.2	-2.3
2013	272	1527	11.91	6.14	22.3	70.7	-3.4	75.0	-2.3
2013	272	1528	12.12	6.07	18.7	76.4	2.5	73.7	-1.3
2013	272	1529	9.59	7.74	29.9	67.9	2.1	66.3	-2.2
2013	272	1530	9.65	7.78	42.8	83.1	-5.3	89.4	-2.3
2013	272	1531	9.81	7.64	42.8	61.3	-4.0	70.2	-2.3
2013	272	1532	10.57	7.06	41.8	50.9	-2.4	53.2	-2.3
2013	272	1533	11.16	6.78	30.9	51.2	-0.2	51.3	-2.3
2013	272	1534	10.54	7.12	30.0	54.1	2.8	51.2	-2.3
2013	272	1535	11.02	6.72	30.1	53.7	-0.8	54.5	-2.3
2013	272	1536	11.14	6.78	31.2	53.4	-5.6	59.0	-2.3
2013	272	1537	10.63	7.02	29.7	59.5	1.5	57.9	-2.3
2013	272	1538	11.50	6.40	26.5	61.5	3.8	57.6	-2.3
2013	272	1539	11.04	6.81	25.8	57.9	-3.7	61.8	-2.3
2013	272	1540	10.88	6.81	28.6	61.9	-1.6	63.5	-2.3
2013	272	1541	11.63	6.30	25.1	63.0	2.9	60.1	-2.3 -2.3
2013	272	1542	11.43	6.53	23.6	59.4	-5.8	65.1	-2.3 -2.3
2013	272	1543	11.17	6.63	24.8	65.8	-5.6 2.3	63.6	
2013	272	1544	11.10	7.04	38.3	73.5	2.3 -1.4		-2.3
2013	272	1545	10.32	8.07	98.2	73.5 182.7	-1. 4 -1.6	77.1	-2.3
2013	272	1546	10.32	7.93	96.2 88.8	150.0	-1.6 -2.2	185.1	-2.3
2013	272	1547	8.87	7.93 8.56	72.8			152.7	-2.3
2013	272	1547 1548	9.55	8.56 7.96		99.5	-4.6	104.9	-2.3
2010	212	1040	9.00	1.90	57.9	72.8	2.4	70.3	-2.3

09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	СО
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1549	9.50	8.06	47.7	54.6	0.0	54.6	-2.3
2013	272	1550	9.33	8.01	44.8	59.4	0.4	58.9	-2.3
2013	272	1551	10.36	7.31	39.2	59.2	2.3.	56.9	-2.3
2013	272	1552	10.30	7.49	33.6	53.1	-3.4	58.0	-2.2
2013	272	1553	0.80	0.38	68.4	65.3	-4.2	83.1	61.5
2013	272	1554	0.07	0.02	88.0	91.0	0.4	90.5	91.0
2013	272	1555	0.06	0.00	89.0	91.0	0.5	90.5	91.1
2013	272	1556	0.07	-0.01	53.3	65.3	-3.5	69.0	68.2
2013	272	1557	0.05	-0.02	44.4	45.5	0.4	45.2	44.5
2013	272	1558	1.73	1.84	40.0	42.9	0.0	42.8	43.1
2013	272	1559	10.00	9.43	2.9	1.7	-2.5	4.9	4.3
2013	272	1600	10.02	9.48	0.8	0.0	0.0	0.0	-2.3
2013	272	1601	10.03	9.49	0.6	0.0	0.0	0.0	-2.3
2013	272	1602	10.04	9.50	0.5	0.0	0.0	0.0	-1.6
2013	272	1603	14.38	5.47	0.9	5.0	-0.4	5.4	0.2
2013	272	1604	21.18	0.03	0.1	0.3	0.2	0.0	2.1
2013	272	1605	21.19	0.02	0.0	0.0	0.0	0.0	2.3
2013	272	1606	21.20	0.01	0.0	0.0	0.0	0.0	2.3
2013	272	1607	21.20	0.01	0.0	0.0	0.0	0.0	2.3
2013	272	1608	21.20	0.01	0.0	0.0	0.0	0.0	2.2
2013	272	1609	21.20	0.00	0.0	0.0	0.0	0.0	2.2
2013	272	1610	21.21	0.00	0.1	0.0	0.0	0.0	2.2
2013	272	1611	21.21	0.00	0.0	0.0	0.0	0.0	2.2
2013	272	1612	21.21	0.00	0.0	0.0	0.0	0.0	2.2
2013	272	1613	21.21	0.00	-0.1	0.0	0.0	0.0	2.2
2013	272	1614	21.21	0.00	0.0	0.0	0.0	0.0	2.2
2013	272	1615	21.21	0.00	0.0	0.0	0.0	0.0	2.2
2013	272	1616	21.22	-0.01	-0.1	0.0	0.0	0.0	2.1
2013	272	1617	21.22	-0.01	0.0	0.0	0.0	0.0	2.1
2013	272	1618	21.22	-0.01	0.0	0.0	0.0	0.0	2.1
2013	272	1619	21.22	-0.01	-0.1	0.0	0.0	0.0	2.1
2013	272	1620	21.22	-0.01	-0.1	0.0	0.0	0.0	2.1
2013	272	1621	21.22	-0.01	0.0	0.0	0.0	0.0	2.1
2013	272	1622	21.22	-0.01	-0.1	0.0	0.0	0.0	2.1
2013	272	1623	21.22	-0.01	-0.1	0.0	0.0	0.0	2.1
2013	272	1624	21.22	-0.01	-0.1	0.0	0.0	0.0	2.1
2013	272	1625	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013,	272	1626	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1627	21.22	-0.01	-0.1	0.0	0.0	0.0	2.1
2013	272	1628	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1629	21.22	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1630	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1631	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1632	21.22	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1633	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1634	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1635	21.22	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1636	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1637	21.22	-0.01	-0.2	0.0	0.0	0.0	1.9
2013	272	1638	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1639	21.22	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1640	21.22	-0.01	-0.2	0.0	0.0	0.0	1.9
2013	272	1641	21.22	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1642	21.22	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1643	21.23	-0.01	-0.1	0.0	0.0	0.0	2.0
2013	272	1644	21.23	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1645	21.23	-0.01	-0.2	0.0	0.0	0.0	2.0
		-	-				-	5.0	

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03/23/1	,								
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	СО
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1646	21.23	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1647	21.22	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1648	21.23	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1649	21.23	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1650	21.23	-0.01	-0.2	0.0	0.0	0.0	1.9
2013	272	1651	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1652	21.23	-0.01	-0.3	0.0	0.0	0.0	2.0
2013	272	1653	21.23	-0.01	-0.2	0.0	0.0	0.0	2.0
2013	272	1654	21.22	-0.01	-0.2	0.0	0.0	0.0	1.9
2013	272	1655	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1656	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1657	21.22	-0.01	-0.3	0.0	0.0	0.0	2.0
2013	272	1658	21.23	-0.01	-0.3	0.0	0.0	0.0	2.0
2013	272	1659	21.22	-0.01	-0.3	0.0	0.0	0.0	2.0
2013	272	1700	21.22	-0.01	-0.3	0.0	0.0	0.0	2.0
2013	272	1701	21.22	-0.01	-0.3	0.0	0.0	0.0	2.0
2013	272	1702	21.23	-0.01	-0.3	0.0	0.0	0.0	2.0
2013	272	1703	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1704	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1705	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1706	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1707	21.23	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1708	21.23	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1709	21.23	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1710	21.23	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1711	21.23	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1712	21.22	-0.01	-0.3	0.0	0.0	0.0	1.9
2013	272	1713	21.22	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1714	21.22	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1715	21.23	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1716	21.23	-0.01	-0.4	0.0	0.0	0.0	1.9
2013	272	1717	21.23	-0.01	-0.5	0.0	0.0	0.0	1.9
2013	272	1718	21.22	-0.01	-0.4	0.3	0.0	0.1	2.1
2013	272	1719	21.22	-0.01	-0.4	0.1	0.0	0.0	2.0
2013	272	1720	21.04	0.20	-0.4	0.1	-0.3	1.0	2.0
2013	272	1721	12.20	5.98	1.4	59.1	-3.0	65.8	0.5
2013	272	1722	11.91	6.07	4.2	76.9	1.0	75.8	0.1
2013 2013	272 272	1723	13.22	5.26	5.6	77.1	-3.0	80.7	0.3
2013	272 272	1724 1725	9.59	8.13	20.5	82.7	-1.3	84.1	0.3
2013	272	1726	9.72 10.53	7.81 7.09	39.7	106.0	-3.7	110.4	-0.1
2013	272	1727	10.96	6.90	27.5 19.0	57.0	-3.7	60.7	0.0
2013	272	1728	10.95	6.89	17.5	58.3 63.1	-3.3	61.7	-0.1
2013	272	1729	11.50	6.38	16.0	63.1	1.4	61.9	-0.1
2013	272	1730	11.51	6.52	14.4	65.6	-5.2 -0.2	68.7	-0.1
2013	272	1731	11.17	6.66	15.0	68.3	1.4	65.8 67.0	0.1
2013	272	1732	11.66	6.27	15.7	66.1	-5.0	71.4	0.2
2013	272	1733	11.83	6.27	16.2	70.6	4.6	66.0	0.3 0.4
2013	272	1734	11.38	6.50	16.1	67.4	-5.5	73.4	0.4
2013	272	1735	11.47	6.38	14.6	74.7	2.3	72.2	0.6
2013	272	1736	12.22	5.89	13.2	72.1	-1.6	73.7	0.5
2013	272	1737	11.91	6.18	12.5	74.5	1.2	73.7 73.5	0.5
2013	272	1738	11.86	6.13	12.7	74.7	-1.7	76.8	0.4
2013	272	1739	12.13	5.97	16.8	70.7	-2.1	72.5	0.5
2013	272	1740	10.85	7.09	21.2	64.5	4.5	59.9	0.6
2013	272	1741	9.80	7.70	25.4	55.2	-2.8	57.8	0.2
2013	272	1742	10.65	7.04	23.6	54.0	-2.5	56.6	0.2
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09/29/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1743	11.23	6.76	19.8	60.9	4.0	56.7	0.3
2013	272	1744	10.77	6.99	. 21.0	60.0	-3.0	62.9	0.5
2013	272	1745	11.21	6.61	20.5	63.6	-2.0	65.5	0.3
2013	272	1746	11.67	6.42	18.3	67.5	5.3	62.3	0.3
2013	272	1747	11.10	6.71	18.8	66.0	-2.9	69.0	0.3
2013	272	1748	11.68	6.26	18.4	67.6	-4.2	72.1	0.3
2013	272	1749	11.77	6.33	16.8	71.8	4.4	67.3	0.3
2013	272	1750	11.23	6.61	18.9	69.4	-4.0	73.5	0.3
2013	272	1751	10.28	7.23	28.1	59.1	-0.3	59.3	0.3
2013	272	1752	9.80	7.60	35.7	47.7	3.2	44.3	0.3
2013	272	1753	9.33	7.81	33.4	45.1	-0.7	45.7	0.3
2013	272	1754	11.50	6.33	23.6	62.3	-3.7	66.1	0.2
2013	272	1755	12.17	6.08	19.6	72.4	3.4	69.0	0.4
2013	272	1756	10.88	7.17	20.4	65.2	-4.3	69.4	0.3
2013	272	1757	9.56	8.03	31.1	57.5	-1.9	59.3	-0.1
2013	272	1758	9.64	7.98	29.0	55.7	-0.1	55.6	0.0
2013	272	1759	9.49	7.86	27.7	60.4	0.6	59.7	-0.2
2013	272	1800	10.49	7.31	23.8	59.9	1.2	58.7	0.0
2013	272	1801	10.09	7.47	22.6	53.7	-2.9	56.6	0.0
2013	272	1802	10.77	6.93	22.0	53.0	-2.0	55.0	0.0
2013	272	1803	11.29	6.70	18.7	55.5	3.2	52.3	0.0
2013	272	1804	10.73	6.98	18.5	53.9	-4.4	58.3	0.1
2013	272	1805	10.97	6.73	18.8	57.5	0.9	56.7	0.0
2013	272	1806	11.70	6.36	16.3	58.3	2.8	55.3	0.0
2013	272	1807	11.08	6.70	16.4	56.7	-5.6	62.6	0.1
2013	272	1808	11.31	6.47	15.9	62.9	1.2	61.6	0.0
2013	272	1809	11.92	6.12	14.9	63.9	-0.7	64.7	0.1
2013	272	1810	11.48	6.46	14.5	67.1	1.3	66.1	0.1
2013	272	1811	11.84	6.19	15.4	68.2	-0.8	68.9	0.2
2013	272	1812	10.43	7.44	23.9	59.0	-3.5	64.1	0.4
2013	272	1813	10.02	7.61	25.8	49.0	-2.9	52.0	0.1
2013	272	1814	10.74	7.01	24.6	57.9	1.7	56.2	0.0
2013	272	1815	11.38	6.68	24.2	56.4	1.7	54.7	0.0
2013	272	1816	10.87	6.96	26.3	54.5	-4.4	58.8	-0.1
2013	272	1817	10.97	6.82	25.4	62.0	2.8	59.2	-0.1
2013	272	1818	11.78	6.23	23.5	59:7	-5.6	66.1	0.0
2013	272	1819	11.48	6.55	22.2	65.8	4.1	61.6	0.0
2013	272	1820	10.75	6.97	26.5	62.0	-3.3	65.2	0.0
2013	272	1821	10.16	7.31	42.3	47.2	-1.9	49.0	0.1
2013	272	1822	9.30	7.93	42.4	45.6	-1.6	47.1	0.2
2013	272	1823	10.02	7.30	41.2	47.6	-0.4	48.0	0.1
2013	272	1824	11.76	6.31	27.4	61.2	2.7	58.5	0.1
2013	272	1825	11.44	6.45	23.4	62.7	-5.5	68.6	0.2
2013	272	1826	11.52	6.37	23.0	71.6	3.5	68.1	0.1
2013	272	1827	12.69	5.66	23.4	70.7	-4.9	76.2	0.4
2013	272	1828	10.96	6.99	23.0	74.9	2.3	72.4	8.0
2013	272	1829	10.68	7.06	25.2	68.5	-3.9	72.5	0.1
2013	272	1830	11.28	6.59	24.0	71.4	-0.8	72.2	0.1
2013	272	1831	10.29	7.42	36.0	63.0	4.0	59.0	0.2
2013	272	1832	9.21	7.89	45.4	54.1	-2.1	56.3	0.2
2013	272	1833	10.02	7.46	44.8	54.6	1.3	53.2	0.1
2013	272	1834	9.15	8.02	48.8	53.5	-3.7	57.2	0.2
2013	272	1835	9.83	7.48	50.0	54.6	-3.3	57.8	0.2
2013	272	1836	11.10	6.80	37.6	59.6	5.0	54.4	0.2
2013	272	1837	10.87	6.91	36.2	63.8	-4.2	68.2	0.1
2013	272	1838	11.00	6.76	35.0	69.7	2.3	67.1	0.1
2013	272	1839	11.74	6.33	30.2	64.8	-3.4	68.2	0.1

09/29/13	;								
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1840	11.10	6.78	29.1	68.0	0.4	67.7	0.1
2013	272	1841	10.98	6.80	30.2	70.2	0.3	70.0	0.0
2013	272	1842	11.66	6.31	29.3	68.9	-4.4	73.4	0.1
2013	272	1843	11.69	6.49	31.2	72.5	0.6	71.9	0.2
2013	272	1844	9.92	7.73	33.1	63.4	-1.2	64.6	0.3
2013	272	1845	9.91	7.66	42.1	56.6	0.5	56.0	0.0
2013	272	1846	10.12	7.65	40.1	53.0	1.5	51.5	0.1
2013	272	1847	9.59	7.87	43.3	51.4	1.1	52.6	0.1
2013	272	1848	10.57	7.22	41.9	51.4	-2.8	54.3	0.0
2013	272	1849	9.87	7.74	42.0	53.1	-0.4	53.6	0.1
2013	272	1850	10.11	7.44	42.7	58.2	8.0	57.3	0.1
2013	272	1851	10.89	7.03	39.7	58.4	-2.1	60.6	0.1
2013	272	1852	10.19	7.45	39.3	61.2	-2.5	63.6	0.1
2013	272	1853	10.54	7.12	38.8	65.8	1.5	64.1	0.1
2013	272	1854	10.90	7.01	36.0	64.5	1.2	63.2	0.1
2013	272	1855	10.29	7.33	36.6	64.8	-3.6	68.3	0.1
2013	272	1856	10.70	6.99	36.0	68.1	1.1	67.0	0.1
2013	272	1857	11.16	6.80	33.1	66.7	0.3	66.4	0.1
2013	272	1858	10.53	7.14	32.1	67.4	-2.7	70.3	0.2
2013	272	1859	11.81	6.34	31.8	68.8	-2.0	70.9	0.4
2013	272	1900	9.27	8.63	56.6	90.3	-3.6	95.5	0.4
2013	272	1901	9.14	8.63	70.0	78.7	0.1	78.6	0.0
2013	272	1902	9.34	8.17	60.2	56.0	-0.4	56.3	-0.1
2013	272	1903	10.57	7.41	45.0	53.7	-1.1	54.8	0.0
2013	272	1904	10.03	7.65	40.2	55.1	-1.6	56.5	0.0
2013	272	1905	10.95	6.95	36.6	57.1	-1.9	58.9	0.1
2013	272	1906	10.85	7.11	32.3	62.0	2.3	59.6	0.1
2013	272	1907	10.58	7.14	33.1	63.9	-0.8	64.7	0.0
2013	272	1908	11.48	6.56	30.3	63.1	-5.0	68.1	0.1
2013	272	1909	11.01	6.93	29.6	65.9	2.0	63.9	0.2
2013	272	1910	10.96	6.83	30.8	69.2	2.2	66.8	0.1
2013	272	1911	11.61	6.51	28.6	66.6	-1.1	67.6	0.2
2013 2013	272	1912	10.97	6.86	27.6	67.4	-4.1	71.4	0.3
2013	272 272	1913 1914	11.57	6.38	26.7	70.2	-0.5	70.4	0.2
2013	272		11.75 11.22	6.38	24.5	70.5	1.7	68.8	0.3
2013	272	1915 1916	10.82	6.69 7.18	27.2 33.9	70.6 65.8	-5.9	76.7	0.3
2013	272	1917	8.99	8.62	56.9	78.4	-4.5 0.7	70.7	0.9
2013	272	1918	9.33	8.13	50.9 51.6	55.2	0.7	80.2 55.0	0.3 0.1
2013	272	1919	10.26	7.61	41.6	58.0	0.2	55.0 57.6	0.1
2013	272	1920	9.81	7.77	39.9	57.2	-1.7	58.7	0.1
2013	272	1921	11.00	6.95	35.4	53.6	-3.3	56.7	0.1
2013	272	1922	10.62	7.27	31.7	57.7	2.4	55.3	0.2
2013	272	1923	10.78	7.00	31.8	60.7	1.1	59.6	0.3
2013	272	1924	11.33	6.76	28.2	58.9	-0.1	58.9	0.3
2013	272	1925	10.78	7.02	27.5	62.0	-4.1	66.1	0.3
2013	272	1926	11.44	6.51	27.1	64.8	-2.0	66.8	0.3
2013	272	1927	11.41	6.64	24.5	66.6	1.0	65.7	0.4
2013	272	1928	10.95	6.85	24.8	67.2	-3.9	71.1	0.4
2013	272	1929	11.55	6.38	24.4	68.3	-0.6	69.0	0.4
2013	272	1930	11.44	6.59	22.1	70.5	4.0	66.5	0.4
2013	272	1931	3.82	2.62	49.0	79.6	19.5	59.9	37.9
2013	272	1932	0.07	0.03	85.8	90.4	0.3	89.9	95.1
2013	272	1933	0.06	0.00	89.4	90.5	0.5	90.1	92.3
2013	272	1934	0.06	-0.01	68.6	81.6	5.0	76.5	82.2
2013	272	1935	0.04	-0.02	44.3	45.7	0.6	45.4	47.7
2013	272	1936	0.04	-0.02	44.8	45.0	0.4	44.8	46.9
-									

00,20,20									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	272	1937	0.04	-0.03	45.1	45.0	0.5	44.5	46.9
2013	272	1938	3.63	3.63	32.1	34.6	1.0	33.5	39.3
2013	272	1939	10.00	9.45	0.4	0.3	-0.2	0.4	2.2
2013	272	1940	10.02	9.48	-0.4	0.0	0.0	0.0	0.0
2013	272	1941	7.00	4.27	27.7	46.7	4.1	48.6	34.1
2013	272	1942	0.03	-0.03	100.6	233.6	-0.7	234.5	100.3
2013	272	1943	0.01	-0.04	100.6	238.3	0.9	237.5	100.3
2013	272	1944	0.00	-0.05	100.6	207.2	-3.0	226.4	100.3
2013	272	1945	-0.01	-0.05	95.0	93.6	1.2	93.1	96.0
2013	272	1946	-0.02	-0.05	94.0	91.9	0.4	91.5	93.2
2013	272	1947	-0.02	-0.05	87.2	91.9	6.7	85.4	90.8
2013	272	1948	-0.02	-0.05	46.2	51.1	4.9	46.1	54.1
2013	272	1949	-0.03	-0.05	45.8	45.8	0.4	45.5	47.4
2013	272	1950	-0.03	-0.05	45.7	45.4	0.4	45.5	47.5
2013	272	1951	18.18	18.01	5.9	9.8	-1.8	12.1	16.5
2013	272	1952	20.15	19.42	-1.5	0.0	0.0	0.0	-0.6
2013	272	1953	16.38	15.40	-1.5	0.0	-0.1	0.0	-0.6
2013	272	1954	10.08	9.60	-1.6	0.0	-0.1	0.0	0.3
2013	272	1955	10.07	9 59	-1 7	0.0	-0.1	0.0	0.4

Run 123-2 09/30/13													
Time (1-min)	NOx (ppm)	(ppm Cor.)	iOx) (lb/hr)	CO (ppm)	(ppm Cor.)	O (lb/hr)	SO2 (ppm)	S (ppm Cor.)	O2 (lb/hr)	O2 (%)	O2 (% Cor.)	CO2 (%)	CO2 (% Cor.)
923 924	51.5 53.4	63.2 55.2	0.32 0.33	3.3 3.4	3.1 3.2	0.01 0.01	14.3 10.9	13.4 10.1	0.11 0.08	11.00	10.97	6.55	8.76
926 928	49.2 62.7	50.8 54.5	0.30 0.33	22.9 26.5	22.4 25.0	0.08	8.6 6.5	7.8 5.8	0.08	11.43	11.40 14.18	6.24 4.54	8.43 4.66
927 928	38.8 33.2	38.1 34.3	0.23 0.21	84.0 100,3	82.6 98.6	0.30	5.0	4.3	0.04	13.26 16.42	13.24 16.41	5.19 3.06	5.34 3.13
929 930	45.9 47.9	47.4	0.28	62.9	61.7	0.36	2.9 3.1	2.3 2.5	0.02 0.02	18,74 11.68	16.73 11.66	2.84 6.54	2.90 6.74
931	60.1	49.5 51.8	0.30 0.31	3.3 2.7	3.1 2.5	0.01 0.01	5.4 6.6	4.7 6,9	0.04 0.05	9.21 9.34	9.18 9.31	8.04 7.94	8.29 8.19
932 933	49.7 49.8	51.4 51.5	0.31 0.31	2.5 2.7	2.3 2.5	0.01 0.01	7.9 8.8	7.2 8.0	0.06 0.07	9.59 9.98	9.68 9.96	7.76 7.47	8.00 7.70
934 935	49.8 60.2	51.5 51.9	0.31 0.31	2.7 2.7	2.5 2.6	0.01 0.01	8.9 8.8	8.1 8.1	0.07 0.07	10.22 10.30	10.19 10.27	7.29 7.23	7.61 7.46
936 937	51.6 53.6	63.4 65.4	0.32 0.33	2.7 2.6	2.5 2.4	0.01 0.01	8.8 8.6	8.0 7.7	0.07 0.08	10.30	10.27 10.36	7.21 7.14	7.43 7.38
938 939	54.6 67.1	56.5 59.0	0.34 0.35	2.6 2.5	2.4	0.01 0.01	8.4 8.2	7.6 7.6	0.06 0.08	10.38	10.33 10.36	7.16 7.10	7.37 7.32
940 941	64.8 68.4	67.0 60.4	0.40 0.36	4.1 3.9	3.9 3.7	0.01 0.01	8.8 9.7	8.0 8.9	0.07	12.01 11.08	11.99 11.05	6.12 6.94	6.30 7.16
842 843	74.6 88.0	77.1 91.0	0.46 0.54	6.0 5.9	4.7 5.6	0.02	37.7 36.0	36.1 33.6	0.30 0.28	7.86 7.77	7.82 7.73	9,49 9,34	9.79 9.64
944 945	80.6 77.3	83.3 79.9	0.60 0.48	4.6 3.8	4.4 3.6	0.02 0.01	33.7 32.3	32.2 30.8	0.27 0.28	7.45 7.44	7.41 7.40	9.44	9.74 9.70
948 947	77.7 64.9	80.3 67.1	0.48 0.40	3.2 2.9	3.0 2.7	0.01 0.01	31.4 28.5	30.0 27.2	0.25 0.23	7.43 7.50	7.39 7.48	9.38 9.29	9.68 9.59
948 949	63.7 61.6	66.6 63.3	0.33 0.32	2.7 2.6	2.6 2.3	0.01 0.01	24.9 23.0	23.6 21.8	0.20 0.18	7.83 8.14	7.79 8.10	9.06 8.85	9.35 9.13
960 961	51.1 48.4	52.8 50.0	0.32 0.30	2.7 2.6	2.5 2.3	0.01 0.01	19.3 18.2	18.2 17.2	0.15 0.14	7.75 8.42	7.71	9.11 8.66	9.40 8.93
952 953	48.3 45.4	49.9 47.0	0.30 0.28	1.7	1.6 1.8	0.01 0.01	17.9 18.1	16.9 15.1	0.14 0.13	8.14 9.05	8.10 9.02	8.80 8.21	9.08 8.47
954 955	48.2 51.6	49.9 53.2	0.30 0.32	1.9 1.8	1.8 1.6	0.01 0.01	13.3 13.8	12.4 12.8	0.10 0.11	8.62 9.27	8.59 9.24	8.46 8.06	8.73 8.31
956 957	64.2 95.8	86,4 99.0	0.40 0.69	3.1 1.8	2,9 1,6	0.01 0.01	14.3 25.6	13.4 24.3	0.11	9.44 8.62	9.41 8.48	8.22 8.89	8,48 9.17
958 959	81.3 60.0	84.0 62.0	0.50 0.37	2.0 2.2	1.8 2.0	0.01 0.01	23.3	22.1 19,4	0.18 0.18	8.30 8.09	8.26 8.05	8.95 9.04	9.23 9.33
1000 1001	63.7 49.6	66.6 61.3	0.33 0.31	2.2 2.1	2.1 2.0	0.01 0.01	18.5	17.4 16.1	0.14 0.13	8.61 8.03	8.67 9.00	8.63 8.32	8.90 8.68
1002 1003	48.1 48.1	49.7 49.7	0.30 0.30	2.2 1.8	2.0 1.6	0.01 0.01	16.2 15.0	16.2	0.13 0.12	9.47 9.08	9.44 9.06	8.03 8.25	8.28 8.51
1004 1006	46.7 48.1	48.3 49.7	0.29 0.30	2.3 1.6	2.1 1.4	0.01 0.01	12.0 12.6	11.1 11.7	0.09	9.67 9.64	9.64 9.61	7.86 7.85	8.11 8.09
1008 1007	60.8 49.6	52.5 61.3	0.31 0.31	1.6 1.9	1.4 1.7	0.01	12.0 10.9	11.1 10.0	0.09	9.37 9.96	9.34 9.93	8.00 7.61	8.25 7.85
1008 1009	52.3 51.9	54.1 53.6	0.32 0.32	1.4 1.7	1.2 1.5	0.00 0.01	10.7 9.2	9.9 8.4	0.08	10.03 9.75	10.00 9.72	7.62 7.72	7.75 7.96
1010 1011	61.1 54.9	52.8 58.7	0.32 0.34	1.7 1.3	1.6 1.1	0.01 0.00	8.9 9.5	8.1 8.7	0.07 0.07	10.25 9.91	10.22 9.88	7.36 7.52	7.69 7.76
1012 1013	58.4 74.2	60.4 76.7	0.36 0.46	4.1 1.8	3.9 1.7	0.01 0.01	9.5 20.0	8.7 18.9	0.07 0.16	10.78 8.48	10.73	7.68 9.18	7.82 9.47
1014 1015	63.3 62.4	66.1 64.2	0.33 0.32	2.3 1.6	2.1 1.4	0.01 0.01	16.8 14.6	15.8 13.7	0.13 0.11	8.16 8.62	8.11 8.59	9.13 8.74	9.42 9.02
1018 1017	52.9 52.5	54.7 54.3	0.33 0.32	1.4 1.2	1.2 1.1	0.00 0.00	11.7 11.1	10.8 10.3	0.09 0.09	9.13 8.80	9.10 8.77	8.31 8.44	8.67 8.71
1018 1019	50.8 52.0	52.6 53.7	0.31 0.32	1.6 1.4	1.3 1.2	0.00 0.00	9.3 8.2	8.6 7.6	0.07 0.06	9.46 9.80	9.43 9.77	8.06 7.77	8.31 8.01
1020 1021	63.6 63.8	55.3 55.6	0.33 0.33	1,4 1,3	1.2 1.1	0.00 0.00	7.6 6.9	6.8 6.2	0.08 0.05	9.85 10.09	9.92 10,06	7.65 7.61	7.89 7.74
1022 1023	66.4 64.3	57.2 56.1	0.34 0.34	1.4 1.4	1.2 1.3	0.00	6.1 6.2	5.3 4.6	0.04 0.04	9.48 10.23	9,45 10.20	7.93 7.41	8.18 7.64
1024 1026	65.1 64.2	67.0 66.0	0.34 0.33	1.3	1.3 1.1	0.00 0.00	6.1 6.3	5.4 5.6	0.04 0.06	10.28 10.41	10.25 10.38	7.37 7.27	7.80 7.49
1026 1027 1028	56.5 55.5	58.5 57.3	0.36 0.34	1.2 1.2	1.0 1.0	0.00	5.7 5.1	5.0 4.5	0.04 0.04	9.90 10.65	9.87 10.52	7.68 7.27	7.82 7.49
1029	58.6 86.9 105.9	60.6 89.8 109.5	0.36 0.54 0.65	3.6 1.0	3,4 0.8	0.01	6.9 14.8	6.1 13.6	0.05 0.11	10.16 9.08	10.13 9.05	7.79 8.44	8.03 8.71
1031 1032	95.1 81.6	99.4 84.4	0.69	0.9 1.0 1.4	0.7 0.9	0.00	19.7 25.1	18.7 23.8	0.16 0.20	8.84 8.80	8.81 8.87	8.61 8.63	8.88 8.80
1033 1034	66.8 63.8	69.1 65.9	0.41 0.39	1.6	1.2 1.4 1.3	0.00 0.01 0.00	29.0 30.0 30.7	27.6 28.6	0.23	9.02 8.72	8.99 8.69	8.41 8.62	8.67 8.89
1035 1036	53.3 56.9	55.1 58.8	0.33 0.36	1.1	0.9 0.8	0.00	28.0 19.8	29.3 26.7 18.7	0.24 0.22 0.16	8.24 9.01 10.28	8.20 8.98	8.84 8.28	9.12 8.54
1037 1038	63.7 60.9	55.6 62.9	0.33	0,9	0.7 0.7	0.00	17.1 14.8	16.0 13.9	0.13 0.12	10.26 10.40 10.32	10.25	7.48 7.34	7.69 7.57
1039 1040	49.9 47.7	61.6 49.3	0.31 0.29	1.3	1.1 1.0	0.00	14.1 14.0	13.2 13.1	0.11 0.11	9.76 9.74	10.29 9.72	7.33 7.78	7.56 8.02
1041 1042	60.1 48.3	51.8 49.9	0.31 0.30	1.1	0.9	0.00	16.1 13.9	14.1 12.9	0.12 0.11	9.87 9.91	9.71 9.84 9.88	7.79 7.66	8.03 7.89
1043 1044	51.4 56.8	63.2 68.7	0.32 0.35	0.8 1.7	0.6 1.5	0.00 0.01	13.8 21.0	12.8 19.9	0.11 0.17	9.71 9.12	9.68 9.09	7.62 7.74 8.68	7.88 7.98 8.95
1045 1046	69,5 49.8	71.9 51.5	0.43 0.31	1.0	0.8	0.00	28.1 21.3	26.7 20.2	0.22 0.17	8.48 8.98	8.44 8.95	9.19 8.63	9.48 8.90
1047 1048	43.0 49.4	44.5 61.1	0.27 0.31	0.8	0.7 0.7	0.00	15.4 12.1	14.4	0.12 0.09	9.60 10.14	9.67 10.11	8.16 7.65	8.42 7.89
1049 1060	65.3 56.7	67.2 68.6	0.34 0.36	0.8 0.7	0.7 0.6	0.00	12.2	11.3 9.5	0.09	10.85	10.62 11.01	7.24 6.94	7.46
1051 1052	55.5 47.5	67.4 49.1	0.34	0.7	0.6 0.6	0.00	10.1	9.3 11.5	0.08 0.10	10.47 9.38	10.44 9.35	7.35 8.00	7.16 7.68 8.26
1063 1064	49.8 49.7	51.5 51.4	0.31 0.31	0.8 0.6	0.5 0.4	0.00	13.1	12.2 11.4	0.10 0.09	9.54 9.51	9.51 9.48	7.87 7.87	8.12 8.12
1055 1056	49.8 60.9	51.4 52.7	0.31 0.31	0.6	0.6 0.6	0.00	12.0 11.3	11.1	0.09	9.76 9.93	9.72 9.90	7.70 7.68	7.94 7.82
1057 1058	52.9 54.0	54.6 65.8	0.33	0.6 0.6	0.4 0.4	0.00	10.9	10.0 10.0	0.08 0.08	10.02 10.22	9.99 10.19	7.61 7.35	7.82 7.74 7.58
1059 1100	56.3 55.4	68.2 67.3	0.35 0.34	0,6 0.6	0.4 0.5	0.00	10.5	9.7 9.0	80.0 80.0	10.30 11.36	10.27 11.32	7.30 6.87	7.52 7.07
1101 1102	49.2 47.1	60.8 48.7	0.30 0.29	0.4 0.4	0.3	0.00	13.6 22.2	12.6 21.0	0.11 0.17	9.67 8.94	9.64 8.91	8.07 8.47	8.32 8.74
1103 1104	48.2 49.7	49.9 61.4	0.30 0.31	0.4	0.3 0.2	0.00	22.9 25.3	21.7 24.0	0.18 0.20	8.83	8.80 8.83	8.51 8.41	8.78 8.67
1106 1106	46.9 47.7	48.4 49.3	0.29 0.30	0.3 0.3	0.2 0.1	0.00	23.4 23.1	22.2 21.9	0.18 0.18	9.07 9.12	9.04 9.09	8.27 8.20	8.63 8.46
1107 1108	48.8 50.1	50.5 51.8	0.30 0.31	0.3 0.2	0.2 0.0	0.00 0.00	22.0 22.4	20.9 21.2	0.17 0.18	9.23 9.19	9.20 9.16	8.12 8.12	8.37 8.37
1109 1110	49.3 49.9	51.0 61.6	0.30 0.31	0.1 0.1	0.0	0.00	20.6 19.1	19.6 18.0	0.18 0.16	9.37 9.54	9.34 9.61	8.00 7.88	8.26 8.13
1111 1112	51.3 52.0	53.0 53.7	0.32 0.32	0.1 0.1	0.0 0.0	0.00	19.0 19.2	18.0 18.1	0.15 0.16	9.50 9.57	9.47 9.64	7.89 7.83	8.14 8.07
1113 1114	53.2 52,6	56.0 54.3	0.33 0.32	0.1 0.0	-0.1 -0.1	0.00	17.7 18.6	16.7 15.6	0.14 0.13	9.56 9.68	9.63 9.65	7.84 7.77	8.08 8.01
1116 1116	61.8 60.6	63.5 62.6	0.32 0.37	0.1 0.7	0.0 0.5	0.00	15.0 19.8	14.1 18.7	0.12 0.18	9.93 10.04	9.90	7.59 7.79	7.83 8.03
1117 1118	109.8 98.1	113.5 101.4	0.68 0.61	1.4	1.2	0.00	44.3 61.9	42.5 59.6	0.35 0.60	9.49 8.47	9.46 8.43	8.42 9.04	8.69 9.33
1119 1120	71.1 66.1	73.5 67.0	0.44 0.34	0.3 0.1	0.2 -0.1	0.00	64.6 61.5	62.3 59.3	0.62 0.49	8.10 8.84	8.06 8.81	9.07 8.49	9.36 8.76
1121 1122	67.5 61.4	69.5 63.4	0.36 0.38	0.0	-0.1 -0.2	0.00	64.7 63.1	62.8 51.1	0.44	9.36 9.64	9.33 9.61	8.19 8.01	8.45 8.26
1123 1124	61.3 62.7	63.4 64.8	0.38 0.39	-0.1 0.0	-0.2 -0.2	0.00 0.00	49.4 49.4	47.A 47.A	0.39 0.39	9.60 9.64	9.67 9.61	7.99 7.93	8.24 8.18
1126 1128 1127	58.4 66.7	60.3 68.6	0.38 0.35	0.0	-0.1 -0.2	0.00	48.9 41.1	45.0 39.4	0.37 0.33	9.78 10.04	9.76 10.01	7.83 7.61	8.07 7.85
1127 1128	67.1 55.8	59.0 57.5	0.35 0.34	-0.1 0.0	-0.2 -0.2	0.00	34.2 28.8	32.7 27.4	0.27 0.23	10.48 10.66	10.43 10.63	7.33 7.32	7.66 7.65
Ave	56.8	58.7	0.35	3.8	3.6	0.01	18.5	17.6	0.16	9.67	9.64	7.86	8.11

Table 5 Continuous Emissions Measurements Results Run I5-2 09/30/13

Time	00/00/10	T												
1.52									1			1	1	1
1922	(1-11111)	. (pp.ii)	(рріп оог.)	(15/111)	(ppiii)	(ppin cor.)	(ID/Nr)	(ppm)	(ppm Cor.)	(lb/hr)	(%)	(% Cor.)	(%)	(% Cor.)
1925 1806					-1.5	-1.2	0.00	18.4	17.0	0.14	10.56	10.55	7.36	7.59
1946								21.5	20.0	0.17	10.75	10.74		
1286 79.4 82.8 8.0.6 -1.8 -1.5 -0.01 39.6 37.0 0.22 28.9 8.97 8.98 8.97												9.26	9.15	9.44
1926														
1986 1986														
1989													1	
1999					1									
1900														
1902 50.5 52.7 0.32														
1902 53.0 54.3 0.33 4.7 4.4 0.00 18.4 16.9 0.44 19.83 10.62 7.49 77.2 77.2 77.8 77.2 77.2 77.8 77.2 77.2 77.8 77.2	1301	50.5	52.7											
1930 1931 1932	1302	53.0	55.3	0.33	-1.7									
1986 63.3 68.6 60.3 -1.7 -1.4 -0.01 -16.9 -16.4 -16.4 -0.13 -10.17 -10.16 -7.74 -7.89 -10.18 -1							-0.01	16.9	15.5	0.13				
1990										0.13	10.17	10.16	7.74	7.98
1930 63.3 68.6 0.33 1.8 1.5 0.00 13.1 11.7 0.10 10.75 10.74 7.39 7.20 10.00 13.0 67.0 68.8 0.22 4.2 0.0 0.00 23.8 23.2 0.019 0.26 0.24 0.77 1.31 1.5 0.00 13.5 11.6 0.01 13.7 10.7 7.37 7.32 7.32 13.1 1			1		1									
1309			I											
1390												I I		
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1403 62.1 64.8 0.39 -0.1 0.1 0.00 37.8 36.1 0.30 10.28 10.27 7.66 7.90 1404 62.2 64.9 0.39 0.3 0.5 0.00 37.4 35.7 0.30 9.87 9.86 7.88 8.13 1405 62.8 65.5 0.39 1.7 1.9 0.01 33.6 32.0 0.27 9.95 9.94 7.79 8.03 1406 64.0 66.7 0.40 0.5 0.7 0.00 33.5 31.9 0.27 10.32 10.31 7.49 7.72 1407 62.3 65.0 0.39 0.7 0.9 0.00 30.1 28.6 0.24 10.74 10.73 7.26 7.49 1408 62.7 65.4 0.39 1.1 1.3 0.00 28.3 26.8 0.22 10.43 10.42 7.50 7.73 1409 62.5 65.2 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>														
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1405 62.8 65.5 0.39 1.7 1.9 0.01 33.6 32.0 0.27 9.95 9.94 7.79 8.03 1406 64.0 66.7 0.40 0.5 0.7 0.00 33.5 31.9 0.27 10.32 10.31 7.49 7.72 1407 62.3 65.0 0.39 0.7 0.9 0.00 30.1 28.6 0.24 10.74 10.73 7.26 7.49 1408 62.7 65.4 0.39 1.1 1.3 0.00 28.3 26.8 0.22 10.43 10.42 7.50 7.73 1409 62.5 65.2 0.39 1.3 1.5 0.01 29.7 28.1 0.23 10.30 10.29 7.53 7.77	1404	62.2	64.9											
1406 64.0 66.7 0.40 0.5 0.7 0.00 33.5 31.9 0.27 10.32 10.31 7.49 7.72 1407 62.3 65.0 0.39 0.7 0.9 0.00 30.1 28.6 0.24 10.74 10.73 7.26 7.49 1408 62.7 65.4 0.39 1.1 1.3 0.00 28.3 26.8 0.22 10.43 10.42 7.50 7.73 1409 62.5 65.2 0.39 1.3 1.5 0.01 29.7 28.1 0.23 10.30 10.29 7.53 7.77	I .							33.6	32.0					
1408 62.7 65.4 0.39 1.1 1.3 0.00 28.3 26.8 0.22 10.43 10.42 7.50 7.73 1409 62.5 65.2 0.39 1.3 1.5 0.01 29.7 28.1 0.23 10.30 10.29 7.53 7.77												10.31		
1409 62.5 65.2 0.39 1.3 1.5 0.01 29.7 28.1 0.23 10.30 10.29 7.53 7.77								,						
A. 2011 0.20 10.20 1.7.71														
Ave 61.9 64.5 0.39 -1.4 -1.2 0.00 27.7 26.1 0.22 10.40 10.39 7.61 7.85				00			5.51	20.1	20, 1	0.23	10.30	10.29	1.53	1.11
1 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Ave	61.9	64.5	0.39	-1.4	-1.2	0.00	27.7	26.1	0.22	10.40	10,39	7.61	7.85
		I.									, ,,,,,	10.00	7.01	7.00

Table 6 Continuous Emissions Measurements Results Run 178-2

Time	NOx	NO:		co	cc)	802	SO2		02	02	CO2	CO2
(1-min)	(ppm)	(ppm Cor.)	(lb/hr)	(ppm)	(ppm Cor.)	(lb/hr)	(ppm)	(ppm Cor.)	(lb/hr)	(%)	(% Cor.)	(%)	(% Co
1508	61.7	64.2	0.38	-0.1	-0.1	0.00	3.9	2.6	0.02	12.32	12.31	6.16	6.34
1507 1508	57.3 56.2	59.7 58.6	0.36 0.35	-1.7 -2.0	-1.7 -2.0	-0.01 -0.01	12.2 23.0	10.9 21.7	0.09 0.18	9.06 9.40	9,03 9,38	8.87 8.34	9.13 8.59
1509 1510	53.7 52.6	55.9 54.7	0.33 0.33	-1.9 -1.9	-1.9 -1.9	-0.01 -0.01	24.6	23.2	0.19	10.07	10.06	7.95	8.18
1611	55.5	57.7	0.35	-2.0	-2.0	-0.01	23.6 21.6	22.2 20.1	0.18 0.17	9.74 10.28	9.72	8.03 7.66	8.27 7.77
1512 1513	64.6 68.9	66,8 61.3	0.34 0.37	-1.9 -2.0	-1.9 -2.0	-0.01 -0.01	16.2 16.0	13.9 14.7	0.12 0.12	10.91 10,51	10.90 10.50	7.23 7.40	7.44 7.61
1514	66.3	69.0	0.41	-2.0	-2.0	-0.01	17.0	15.7	0.13	10.86	10.84	7.09	7.29
1616 1618	63.5 69.9	68.1 72.8	0.40 0.44	-2.0 -1.9	-2.0 -1.9	-0.01 -0.01	15.8 14.8	14.5 13.5	0.12 0.11	11.60 11.05	11.69	6.84 7.01	6.82 7.21
1517	69.1	71.9	0.43	-2.1	-2.1	-0.01	14.9	13.5	0.11	10.95	10.94	7.01	7.21
1518 1519	69.7 72.3	72.6 76.3	0.43 0.46	-2.1 -2.0	-2.1 -2.0	-0.01 -0.01	13.6 12.0	12.2 10.7	0.10 0.09	11.71 11.52	11.70 11.61	6.48 6.68	6.64 6.87
1520 1521	71,4 76,1	74.3 79.2	0.44	-2.1	-2.1	-0.01	12.2	10.8	0.08	11.26	11.25	6.78	8.97
1522	65.4	68.1	0.47 0.41	-2.1 -1.6	-2.1 -1.6	-0.01 -0.01	12.4 12.2	11.1 10.9	0.09	11.54 12.51	11.63 12.60	6.52 6.22	6.71 6.39
1623 1624	56.2 55.6	58.5 57.9	0.35 0.35	-1.9 -2.3	-1.9 -2.3	-0.01 -0.01	23.7 30.8	22.3 29.4	0.19 0.24	8.73 9.23	8.71 9.21	9.06 8.61	9.33 8.86
1625	62.1	54.2	0.32	-2.3	-2.3	-0.01	30.4	29.0	0.24	9.22	9.20	8.68	8.94
1526 1527	49.6 54.1	51.6 58.3	0.31 0.34	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	30.2 28.2	28.8 26.8	0.24	9.11 10.07	9.09 10.06	8.59 7.86	8.84 8.08
1628 1629	53.7	65.9	0.33	-2.3	-2.3	-0.01	24.3	22.9	0.19	10.07	10.06	7.93	8.16
1530	62.8 64.9	65.0 57.2	0.33 0.34	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	22.1 22.2	20.7 20.8	0.17 0.17	9.86 10.41	9.84 10.40	7.96 7.52	8.19 7.74
1631 1632	63.7 54.1	55.9 56.3	0.33 0.34	-2.3	-2.3	-0.01	22.7	21.4	0.18	10.48	10.45	7.60	7.82
1633	56.2	68.6	0.34	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	19.6 20.9	18.2 19.6	0.15 0.16	9.94 10.25	9.92 10.24	7.87 7.69	8.10 7.81
1634 1635	52.7 55.2	64.9 67.5	0.33 0.34	-2.3 -2.3	-2.3	-0.01	21.2	19.8	0.16	10.79	10.78	7.33	7.54
1636	67.7	60.1	0.36	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	21.8 21.6	20.4 20.2	0.17 0.17	10.15 10.71	10.14 10.70	7.70 7.25	7.92 7.46
1537 1538	52.8 66.1	54.9 58.4	0.33 0.35	-2.3 -2.3	-2.3 -2.2	-0.01 -0.01	18.8 20.3	17.5	0.15	10.84	10.83	7.27	7.48
1639	86.4	89.9	0.54	-2.0	-2.2	-0.01	34.8	19.0 33.3	0.16 0.28	10.80 9.44	10.79 9.42	7.22 8.51	7.43 8.76
1540 1541	103.4 88.0	107.8 91.6	0.64	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	48.0 65.0	48.5 53.4	0.39 0.45	10.00	9.98	8.21	8.46
1542	72.0	74.9	0.45	-2.3	-2.3	-0.01	49.6	48.0	0.40	8.92 8.92	8.90 8.90	8.88 8.67	9.14 8.93
1543 1544	59.5 51.0	62.0 53.0	0.37 0.32	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	42.5 41.0	41.0 39.6	0.34 0.33	9.11 8.81	9.09 8.79	8.60 8.62	8.85 8.87
1646	46.4	48.3	0.29	-2.3	-2.3	-0.01	35.5	34.1	0.28	9.74	9.72	8.04	8.28
1548 1547	46.8 46.4	48.7 48.3	0.29 0.29	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	29.0 27.8	27.5 26.4	0.23 0.22	9.16 9.44	9.14 9.42	8.45 8.12	8.70 8.36
1548	44.2	48.0	0.28	-2.3	-2.3	-0.01	24.9	23.6	0.20	10.14	10.13	7.76	7.98
1549 1660	47.5 48.3	49.4 50.2	0.30 0.30	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	25.4 27.0	24.0 26.6	0.20 0.21	9.49 10.31	9.47 10.30	8.14 7.50	8.38 7.72
1651 1662	49.2 49.5	51.2 51.5	0.31 0.31	-2.3 -2.3	-2.3	-0.01	26.8	24.4	0.20	10.01	9.99	7.81	8.04
1663	47.9	49.9	0.30	-2.3	-2.3 -2.3	-0.01 -0.01	26.5 23.0	25.1 21.6	0.21 0.18	9.98 10.79	9.96 10.78	7.69 7.22	7.91 7.43
1554 1555	60.8 61.7	63.3 64.2	0.38 0.38	-2.1 -1.7	-2.1 -1.7	-0.01	33.9	32.4	0.27	9.71	9.69	8.04	8.28
1666	67.8	70.6	0.42	-2.3	-2.3	-0.01 -0.01	34.7 39.0	33.2 37.5	0.28 0.31	9.12 8.80	9.10 8.78	8.72 8.67	8.98 8.93
1557 1658	67.3 61.6	69.7 63.7	0.36 0.32	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	34.2 35.1	32.8 33.6	0.27 0.28	9.71 9.06	9.69 9.04	8.10 8.63	8.34 8.78
1569	50.8	52.9	0.32	-2.3	-2.3	-0.01	31.7	30.3	0.25	9.88	9.84	7.87	8.78
1600 1601	49.3 51.5	51.3 53.6	0.31	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	28.2 25.1	24.8 23.7	0.21 0.20	10.09 9.77	10.08 9.76	7.83 7.92	8.08 8.15
1602	49.8	51.8	0.31	-2.3	-2.3	-0.01	24.9	23.5	0.20	10.80	10.89	7.16	7.37
1603 1604	62.4 63.4	64.6 65.6	0.33 0.33	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	25.7 26.9	24.3 25.5	0.20 0.21	10.09 11.01	10.08 11.00	7.69 6.99	7.91 7.19
1605 1606	63.8 55.8	58.0 58.1	0.34 0.36	-2.3	-2.3	-0.01	23,4	22.0	0.18	10.74	10.73	7.28	7.49
1607	54.6	56.8	0.34	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	22.8 21.6	21.6 20.2	0.18 0.17	10.68 11.37	10.57 11.36	7.25 8.78	7.46 6.97
1608 1609	59.5 59.4	61.9 . 61.8	0.37	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	18.8 16.7	17.6	0.15	10.66	10.65	7.27	7.48
1610	64.5	68.7	0.34	-2.3	-2.2	-0.01	20.7	15.4 19.4	0.13 0.18	10.93 10.96	10.92 10.96	6.98 7.20	7.18 7.41
1611	68.5 64.1	60.9 68.3	0.36 0.34	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	28.8 33.3	27.4 31.9	0.23 0.27	9.00	8.98 9.47	8.51 8.06	8.76 8.29
1613	43.6	45.3	0.27	-2.3	-2.3	-0.01	28.3	26.9	0.22	10.17	10.16	7.71	7.93
1614 1615	47.8 54.0	49.8 56.2	0.30 0.34	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	28.8 29.1	27.4 27.7	0.23	10.12 11.06	10.11 11.05	7.63 6.95	7.85 7.14
1616 1617	55.4 58.9	57.7 61.3	0.35 0.37	-2.3 -2.3	-2.3 -2.3	-0.01	29.4	28.0	0.23	10.82	10.81	7.22	7.43
1618	59.5	61.9	0.37	-2.3	-2.3 -2.3	-0.01 -0.01	33.9 30.5	32.4 29.1	0.27 0.24	10.58 11.54	10.57 11.53	7.27 6.67	7.48 6.88
1619 1620	66.2 67.8	68.9 70.5	0.41	-2.3 -2.3	-2.3 -2.3	-0.01	35.1	33.7	0.28	10.71	10.70	7.22	7.43
1621	64.6	67.2	0.40	-2.3	-2.3	-0.01 -0.01	36.7 41.0	35.2 39.5	0.29	11.09	11.08 11.49	6.8B 6.72	7.07 8.91
1622 1623	67.6 71.1	70.2 74.0	0.42	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	36.7 24.6	35.3 23.3	0.29 0.19	10.86 11.40	10.85 11.39	7.08 6.65	7.28 6.84
1624	66.0	68.7	0.41	-2.3	-2.3	-0.01	18.7	17.4	0.14	11.29	11.28	6.86	7.05
1626 1628	66.9 64.6	69.7 67.2	0.42	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	19.4 21.2	18.0 19.8	0.16 0.17	10.84 11.83	10.83 11.82	7.06 8.53	7.26 6.71
1827 1628	74.1	77.1	0.46	-2.3	-2.3	-0.01	33.3	31.9	0.27	9.17	9.16	8.64	8.90
1629	75.3 48.2	78.4 60.2	0.47 0.30	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	44.9 37.9	43.4 36.4	0.36	8.76 9.78	8.73 9.76	8.76 8.10	9.02 8.34
1630 1631	48.1 60.3	60.1 62.4	0.30 0.31	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	31.7 30.7	30.3 29.3	0.25	9,39	9.37	8.29	8.63
1632	48.3	50.2	0.30	-2.3	-2.3	-0.01	26.8	25.4	0.24	10.16 10.35	10.14	7.69 7.67	7.91 7.89
1633 1634	61.0 61.5	53.1 53.6	0.32 0.32	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	27.0 25.1	25.6 23.8	0.21 0.20	9.84 10.75	9.82 10.74	7.88 7.30	8.11 7.61
1635 1636	63.7	55.8	0.33	-2.3	-2.3	-0.01	22.9	21.5	0.18	10.15	10.14	7.76	7.99
1637	54.1 53.4	56.3 55.6	0.34 0.33	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	23.9 20.1	22.6 18.7	0.19 0.16	10.46 10.90	10.46 10.89	7.41 7.23	7.62 7.44
1638 1639	67.3 57.3	59.6 59.6	0.36 0.36	-2.3 -2.3	-2.3	-0.01	22.2	20.8	0.17	10.45	10.44	7.39	7.60
1640	61.1	63.6	0.38	-2.3	-2.3 -2.3	-0.01 -0.01	19.7 17.9	18.3 16.6	0.15 0.14	11.32 10.58	11.31 10.57	6.88 7.35	7.08 7.56
1641 1642	61.0 68.0	63.6 60.4	0,38 0.36	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	19.1	17.8	0.15	11.17	11.16	6.87	7.07
1643	66.9	59.2	0.35	-2.3	-2.3	-0.01	20.7 26.0	19.3 24.6	0.16 0.20	11.35 9.99	11.34 9.97	6.95 7.76	7.15 7.98
1644 1645	60.6 64.4	63.1 67.0	0.38 0.40	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	27.6 24.8	26.2 23.4	0.22 0.19	10.97 10.74	10.96 10.73	7.03 7.28	7.23 7.49
1646	67.2	69.8	0.42	-2.3	-2.3	-0.01	26.1	24.7	0.21	10.99	10.98	6.97	7.17
1647 1648	64.6 67.1	67.2 69.8	0.40	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	21.7	20.4 19.4	0.17 0.16	11.77 10.98	11.76 10.97	6.64 7.04	6.73 7.24
1649	62.9	65.6	0.39	-2.3	-2.3	-0.01	21.9	20.6	0.17	11.00	10.99	8.98	7.18
1650 1651	64.1 64.3	66.7 67.0	0.40 0.40	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	20.1 18.7	18.7 17.4	0.16 0.14	11.68 11.23	11.67 11.22	6.66 6.89	6.73 7.09
1652 1653	64.9	67.5	0.40	-2.3	-2.3	-0.01	18.8	17.4	0.14	11.23	11.22	6.84	7.03
1654	63.7 66.1	66.3 68.8	0.40 0.41	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	18.7 18.3	17.3 17.0	0.14	11.32 11.74	11.31	6.77 6.45	6.96 6.63
1655 1656	81.4 66.6	63.9 69.3	0.38 0.41	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	16.9 15.6	16.6 14.2	0.13	11.88	11.87	6.44	6.62
1657	66,3	69.0	0.41	-2.3	-2.3	-0.01	16.6 16.1	14.8	0.12 0.12	11.57 11.56	11.56 11.55	6.59 6.68	6.77 6.77
1658 1669	70.6 68.3	73.4 71.1	0.44 0.43	-2.2 -2.1	-2.2	-0.01	17.7	16.3	0.14	12.46	12.45	6.01	6.17
1700	70.6	73.6	0.44	-2.3	-2.1 -2.3	-0.01 -0.01	30.3 48.6	28.9 47.1	0.24 0.39	9.41 8.43	9.39 8.41	8.33 8.86	8.68 9.11
1701 1702	53.2 52.5	65.3 54.6	0.33 0.33	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	50.0 48.3	48.6 46.8	0.40 0.39	9.55 8.69	9.63 8.67	8.11	8.35
1703	62.6	64.6	0.33	-2.3	-2.3	-0.01	48.5	47.0	0.39	9.30	9.28	8.72 8.21	8.98 8.45
1704 1705	47.0 46.9	49.0 48.8	0.29 0.29	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	44.9 46.3	43.4 44.8	0.36 0.37	9.16	9.14	8.42	8.67
1706	46.3	48.2	0.29	-2.3	-2.3	-0.01	46.9	46.4	0.38	9.00 9.78	8.98 9.78	8.41 7.84	8.66 8.17
1707 1708	46.9 46.9	48.8 48.8	0.29 0.29	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	49.1 61.6	47.6 60.0	0.40 0.42	8.99	8.97	8.49	8.74
1709	47.5	49.4	0.30	-2.3	-2.3	-0.01	48.0	46.5	0.39	9.23 9.25	9.21 9.23	8.24 8.36	8.48 8.61
1710 1711	51.8 53.8	63.9 56.0	0.32 0.33	-2.3 -2.3	-2.3 -2.3	-0.01 -0.01	49.3 47.2	47.8 45.7	0.40 0.38	8.70 9.42	8.68 9.40	8.63 8.14	8.89 8.38
	J-1-								~.~0	V.76 1	v.90	0.19	5.38

09/30/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	800	0.01	0.01	95.7	91.9	0.4	91.4	93.7
2013	273	801	0.01	0.01	96.2	91.7	0.4	91.4	93.0
2013	273	802	1.44	1.89	84.1	91.8	5.2	86.0	90.2
2013	273	803	20.03	19.39	4.4	13.8	9.9	2.5	18.1
2013	273	804	20.18	19.45	0.1	0.0	-0.1	0.0	-0.1
2013	273	805	20.19	19.46	0.1	0.0	-0.1	0.0	0.2
2013	273	806	20.20	19.47	0.0	0.0	-0.1	0.0	0.2
2013	273	807	20.20	19.47	0.0	0.0	0.0	0.3	0.1
2013	273	808	12.67	11.62	42.0	46.8	-4.0	87.2	28.3
2013	273	809	0.04	0.07	100.6	235.9	-0.1	235.9	100.3
2013	273	810	0.02	0.04	100.6	236.6	0.5	235.9	100.3
2013	273	811	0.02	0.04	100.6	236.8	0.9	236.0	
2013	273	812	0.02	0.03	96.6	159.8			100.3
2013	273	813	0.00	0.02	90.5		23.5	136.2	99.2
2013	273	814	0.00			91.4	0.4	90.9	92.3
2013	273	815		0.02	90.5	91.4	0.4	91.0	92.2
2013	273 273		0.00	0.02	89.7	91.4	1.6	89.8	92.3
		816	0.02	0.01	40.3	53.2	0.5	52.6	59.2
2013	273	817	-0.01	0.01	44.6	45.4	0.4	44.6	47.4
2013	273	818	2.18	2.38	37.8	38.2	-3.0	42.3	44.5
2013	273	819	10.08	9.62	0.8	1.3	0.1	1.1	5.5
2013	273	820	10.09	9.63	0.0	0.0	-0.1	0.0	1.0
2013	273	821	13.94	5.51	0.6	0.0	-0.1	0.0	1.3
2013	273	822	20.13	0.08	8.0	0.0	-0.1	0.0	3.2
2013	273	823	20.13	0.06	0.4	0.0	-0.1	0.0	3.2
2013	273	824	20.13	0.06	0.4	-0.1	-0.1	0.0	3.4
2013	273	825	20.13	0.05	0.3	-0.1	-0.1	0.0	3.3
2013	273	826	20.13	0.06	0.4	-0.1	-0.1	0.0	3.5
2013	273	827	20.14	0.05	0.4	-0.1	-0.1	0.0	3.4
2013	273	828	20.14	0.05	0.3	0.0	-0.1	0.0	3.4
2013	273	829	20.14	0.05	0.4	0.0	-0.1	0.0	3.2
2013	273	830	20.14	0.05	0.4	0.0	-0.1	-0.1	3.2
2013	273	831	20.14	0.05	0.4	0.0	-0.1	0.0	3.1
2013	273	832	20.14	0.05	0.4	0.0	-0.1	0.0	3.0
2013	273	833	20.14	0.05	0.5	-0.1	-0.1	0.0	3.5
2013	273	834	20.14	0.05	0.5	0.0	-0.1	0.0	3.1
2013	273	835	20.14	0.05	0.4	0.0	-0.1	0.0	3.1
2013	273	836	20.13	0.05	0.5	0.0	-0.1	0.0	3.2
2013	273	837	20.13	0.05	0.4	-0.1	-0.1	0.0	3.2
2013	273	838	20.13	0.05	0.4	0.0	-0.1	0.0	2.9
2013	273	839	20.13	0.05	0.4	0.0	-0.1	0.0	2.8
2013	273	840	20.13	0.05	0.5	-0.1	-0.1	0.0	2.9
2013	273	841	20.13	0.05	0.4	0.0	-0.1	0.0	2.9
2013	273	842	20.12	0.05	0.5	0.0	-0.1	0.0	2.8
2013	273	843	20.12	0.05	0.4	0.0	-0.1	0.0	3.3
2013	273	844	20.12	0.05	0.4	0.0	-0.1	0.0	2.8
2013	273	845	20.12	0.05	0.4	0.0	-0.1	0.0	2.7
2013	273	846	20.13	0.05	0.5	0.0	-0.1	-0.1	2.8
2013	273	847	20.13	0.05	0.5	0.0	-0.1	0.0	2.8
2013	273	848	20.13	0.05	0.5	0.0	-0.1	0.0	2.9
2013	273	849	20.14	0.05	0.6	0.0	-0.1	0.0	3.1
2013	273	850	20.14	0.05	0.5	0.0	-0.1 -0.1	-0.1	
2013	273	851	20.14	0.05	0.6	0.0	-0.1 -0.1		3.3
2013	273	852	20.14	0.05	0.5			0.0	3.2
2013	273 273	853	20.14			0.0	-0.1	-0.1	3.1
2013	273 273			0.05	0.6	0.0	-0.1	0.0	3.1
2013		854 855	20.14	0.05	0.6	0.0	-0.1	0.0	3.0
	273	855 856	20.14	0.05	0.7	0.0	-0.1	0.0	2.9
2013	273	856	20.14	0.05	0.6	0.0	-0.1	0.0	3.1

09/30/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	СО
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	857	20.14	0.05	0.6	0.0	-0.1	0.0	3.4
2013	273	858	20.15	0.05	0.6	0.0	-0.1	0.0	3.4
2013	273	859	20.15	0.06	0.6	0.0	-0.1	0.0	3.1
2013	273	900	20.15	0.06	0.6	0.0	-0.1	0.0	3.8
2013	273	901	20.16	0.06	0.6	0.0	-0.1	0.0	4.0
2013	273	902	20.16	0.05	0.7	-0.1	-0.1	0.0	3.3
2013	273	903	20.16	0.05	0.6	0.0	-0.1	0.0	3.1
2013	273	904	20.16	0.05	0.6	0.0	-0.1	0.0	3.6
2013	273	905	20.15	0.05	0.7	0.0	-0.1	0.0	3.3
2013	273	906	20.15	0.05	0.7	-0.1	-0.1	0.0	3.4
2013	273	907	20.15	0.05	0.7	0.0	-0.1 -0.1	0.0	3.4
2013	273	908	20.14	0.04	0.6	0.0	-0.1	0.0	3.8
2013	273	909	18.49	1.49	1.1	4.5	0.2	4.2	3.3
2013	273	910	11.23	6.23	3.7	45.5	5.0	42.0	3.6
2013	273	911	10.24	9.18	0.9	12.8	-0.2	13.2	
2013	273	912	10.24	9.81	0.9	0.0			2.0
2013	273	913	10.03	9.82	0.0	0.0	-0.1	0.0	0.8
2013	273	914	9.75	9.37	2.2		-0.1	0.0	0.9
2013	273	915	0.26	0.20		-0.1	-2.0	2.1	1.5
2013	273	916	0.28	0.20	76.3	81.3	8.1	73.0	68.7
2013	273	917	0.09		86.7	89.4	-0.1	89.4	91.3
2013	273	917	0.08	0.05	88.6	89.4	0.1	89.4	91.4
2013	273 273	916 919		0.04	90.5	89.5	0.4	89.5	91.4
2013			0.07	0.03	73.2	78.8	5.5	73.4	81.7
	273	920	0.06	0.02	46.0	44.7	0.1	44.5	47.7
2013	273	921	3.70	2.41	45.2	46.8	0.6	46.1	40.9
2013	273	922	10.85	6.61	19.1	52.7	-0.4	53.0	5.9
2013	273	923	11.00	6.55	14.3	51.5	-1.1	52.6	3.3
2013	273	924	11.43	6.24	10.9	53.4	-2.1	55.5	3.4
2013	273	925	14.20	4.54	8.6	49.2	-8.4	57.5	22.9
2013	273	926	13.26	5.19	6.5	52.7	-4.5	57.3	25.5
2013	273	927	16.42	3.06	5.0	36.8	-0.2	36.9	84.0
2013	273	928	16.74	2.84	2.9	33.2	-4.8	38.0	100.3
2013	273	929	11.68	6.54	3.1	45.9	1.3	44.7	62.9
2013	273	930	9.21	8.04	5.4	47.9	-0.6	48.4	3.3
2013	273	931	9.34	7.94	6.6	50.1	0.3	49.9	2.7
2013	273	932	9.59	7.76	7.9	49.7	0.0	49.7	2.5
2013	273	933	9.98	7.47	8.8	49.8	-0.6	50.4	2.7
2013	273	934	10.22	7.29	8.9	49.8	-0.9	50.6	2.7
2013	273	935	10.30	7.23	8.8	50.2	-0.3	50.6	2.7
2013	273	936	10.30	7.21	8.8	51.6	-1.8	53.4	2.7
2013	273	937	10.39	7.14	8.5	53.5	-1.5	54.9	2.6
2013	273	938	10.36	7.15	8.4	54.6	-1.8	56.3	2.6
2013	273	939	10.39	7.10	8.2	57.1	-1.5	58.4	2.5
2013	273	940	12.01	6.12	8.8	64.8	4.2	60.4	4.1
2013	273	941	11.08	6.94	9.7	58.4	-3.9	62.1	3.9
2013	273	942	7.86	9.49	37.7	74.6	-0.3	74.9	5.0
2013	273	943	7.77	9.34	35.0	88.0	0.4	87.4	5.9
2013	273	944	7.45	9.44	33.7	80.6	1.1 ·	79.3	4.6
2013	273	945	7.44	9.40	32.3	77.3	-2.1	79.5	3.8
2013	273	946	7.43	9.38	31.4	77.7	-1.4	78.8	3.2
2013	273	947	7.50	9.29	28.5	64.9	1.8	63.0	2.9
2013	273	948	7.83	9.06	24.9	53.7	-1.1	54.6	2.7
2013	273	949	8.14	8.85	23.0	51.6	-0.3	51.8	2.5
2013	273	950	7.75	9.11	19.3	51.1	1.1	50.0	2.7
2013	273	951	8.42	8.66	18.2	48.4	-0.3	48.4	2.5
2013	273	952	8.14	8.80	17.9	48.3	-0.4	48.5	1.7
2013	273	953	9.05	8.21	16.1	45.4	-3.5	48.9	2.0
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09/30/13							/		
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	954	8.62	8.46	13.3	48.2	1.3	49.5	1.9
2013	273	955	9.27	8.06	13.8	51.5	-0.3	51.8	1.8
2013	273	956	9.44	8.22	14.3	64.2	0.8	63.3	3.1
2013	273	957	8.52	8.89	25.6	95.8	0.1	95.6	1.8
2013	273	958	8.30	8.95	23.3	81.3	-1.0	82.2	2.0
2013	273	959	8.09	9.04	20.6	60.0			
2013	273	1000	8.61	8.63	20.6 18.5		-2.5	62.6	2.2
2013	273	1000	9.03	8.32		53.7	-1.3	55.0	2.2
2013	273	1001	9.03 9.47		17.1	49.6	-1.8	51.3	2.1
2013	273	1002		8.03	16.2	48.1	-1.0	49.0	2.2
2013	273	1003	9.08	8.25	15.0	48.1	-1.4	49.4	1.8
			9.67	7.86	12.0	46.7	-1.4	48.1	2.3
2013	273	1005	9.64	7.85	12.6	48.1	-2.7	50.7	1.6
2013	273	1006	9.37	8.00	12.0	50.8	-2.0	52.6	1.6
2013	273	1007	9.96	7.61	10.9	49.6	-1.8	51.3	1.9
2013	273	1008	10.03	7.52	10.7	52.3	0.1	52.0	1.4
2013	273	1009	9.75	. 7.72	9.2	51.9	0.2	51.5	1.7
2013	273	1010	10.25	7.36	8.9	51.1	-2.3	53.1	1.7
2013	273	1011	9.91	7.52	9.5	54.9	-1.8	56.6	1.3
2013	273	1012	10.76	7.58	9.5	58.4	-3.4	61.8	4.1
2013	273	1013	8.48	9.18	20.0	74.2	3.9	70.2	1.8
2013	273	1014	8.15	9.13	16.8	53.3	-1.1	54.3	2.3
2013	273	1015	8.62	8.74	14.6	52.4	2.3	50.0	1.6
2013	273	1016	9.13	8.31	11.7	52.9	-2.5	55.3	1.4
2013	273	1017	8.80	8.44	11.1	52.5	-0.7	53.3	1.2
2013	273	1018	9.46	8.06	9.3	50.8	-3.2	54.0	1.5
2013	273	1019	9.80	7.77	8.2	52.0	-2.5	54.4	1.4
2013	273	1020	9.95	7.65	7.5	53.5	1.0	52.5	1.4
2013	273	1021	10.09	7.51	6.9	53.8	-0.7	54.5	1.3
2013	273	1022	9.48	7.93	6.1	55.4	0.6	54.6	1.4
2013	273	1023	10.23	7.41	5.2	54.3	1.0	53.2	1.4
2013	273	1024	10.28	7.37	6.1	55.1	1.9	53.0	1.4
2013	273	1025	10.41	7.27	6.3	54.2	-2.2	56.1	1.3
2013	273	1026	9.90	7.58	5.7	56.5	-1.1	57.7	1.2
2013	273	1027	10.55	7.27	5.1	55.5	-2.9	58.3	1.2
2013	273	1028	10.16	7.79	6.9	58.6	2.3	56.3	
2013	273	1029	9.08	8.44	14.6				3.6
2013	273	1030	8.84	8.61	19.7	86.9 105.9	2.8	83.9	1.0
2013	273	1031	8.90	8.53			-1.5	107.5	0.9
2013	273	1031	9.02	8.41	25.1 29.0	96.1	-2.3	98.4	1.0
2013	273	1032	8.72			81.6	0.5	81.1	1.4
2013	273	1033		8.62	30.0	66.8	-5.2	72.0	1.6
			8.24	8.84	30.7	63.8	0.7	63.0	1.4
2013	273	1035	9.01	8.28	28.0	53,3	1.2	52.1	1.1
2013	273	1036	10.28	7.46	19.8	56.9	1.3	55.7°	1.0
2013	273	1037	10.40	7.34	17.1	53.7	-4.2	57.7	0.9
2013	273	1038	10.32	7.33	14.8	60.9	0.2	60.5	0.9
2013	273	1039	9.75	7.78	14.1	49.9	-2 .7	52.5	1.3
2013	273	1040	9.74	7.79	14.0	47.7	-2.2	49.8	1.1
2013	273	1041	9.87	7.65	15.1	50.1	1.5	48.5	1.1
2013	273	1042	9.91	7.62	13.9	48.3	-2.5	50.8	1.0
2013	273	1043	9.71	7.74	13.8	51.4	1.5	49.9	8.0
2013	273	1044	9.12	8.68	21.0	56.8	-1.4	58.0	1.7
2013	273	1045	8.48	9.19	28.1	69.5	-3.1	72.5	1.0
2013	273	1046	8.98	8.63	21.3	49.8	1.6	48.1	0.9
2013	273	1047	9.60	8.16	15.4	43.0	-1.7	44.6	0.8
2013	273	1048	10.14	7.65	12.1	49.4	1.4	47.9	0.9
2013	273	1049	10.65	7.24	12.2	55.3	3.4	51.8	0.8
2013	273	1050	11.04	6.94	10.3	56.7	2.2	54.3	0.7
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09/30/13					9				
Year	Julian	Time	02	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	. (%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1051	10.47	7.35	10.1	55.5	2.2	53.3	0.7
2013	273	1052	9.38	8.00	12.4	47.5	1.2	46.3	0.6
2013	273	1053	9.54	7.87	13.1	49.8	1.5	48.5	0.6
2013	273	1054	9.51	7.87	12.2	49.7	0.4	49.2	0.6
2013	273	1055	9.75	7.70	12.0	49.8	-1.2	50.9	0.6
2013	273	1056	9.93	7.58	11.3	50.9	-1.8	52.6	0.7
2013	273	1057	10.02	7.51	10.9	52.9	-1.9	54.5	0.6
2013	273	1058	10.22	7.35	10.9	54.0	-1.6	55.6	0.6
2013	273	1059	10.30	7.30	10.5	56.3	-1.5	57.6	0.6
2013	273	1100	11.35	6.87	9.8	55.4	-3.8	59.2	0.6
2013	273	1101	9.67	8.07	13.6	49.2	-2.8	51.8	0.4
2013	273	1102	8.94	8.47	22.2	47.1	-0.1	47.2	0.4
2013	273	1103	8.83	8.51	22.9	48.2	-0.4	48.5	0.4
2013	273	1104	8.86	8.41	25.3	49.7	1.5	48.2	0.4
2013	273	1105	9.07	8.27	23.4	46.9	0.7	46.0	0.4
2013	273	1106	9.12	8.20	23.1	40.9 47.7	1.8		
2013	273	1107	9.23	8.12	22.0	48.8		45.8	0.3
2013	273	1107	9.19	8.12	22.4	50.1	1.2 1.5	47.5	0.3
2013	273	1109	9.37	8.00	20.6	49.3		48.6	0.2
2013	273	1110	9.54	7.88	19.1	49.3 49.9	0.9	48.3	0.1
2013	273	1111	9.50	7.89			0.3	49.5	0.1
2013	273	1112	9.50 9.57	7.83	19.0	51.3	0.7	50.6	0.1
2013	273 273	1112			19.2	52.0	1.2	50.8	0.1
2013	273 273		9.56	7.84	17.7	53.2	1.4	51.7	0.1
		1114	9.68	7.77	16.6	52.6	0.0	52.2	0.0
2013	273	1115	9.93	7.59	15.0	51.8	-1.1	52.7	0.1
2013	273	1116	10.04	7.79	19.8	60.5	1.4	59.1	0.7
2013	273	1117	9.49	8.42	44.3	109.8	0.1	109.6	1.4
2013	273	1118	8.47	9.04	61.9	98.1	-2.3	100.6	1.0
2013	273	1119	8.10	9.07	64.6	71.1	1.1	69.8	0.3
2013	273	1120	8.84	8.49	61.5	55.1	-0.5	55.5	0.1
2013	273	1121	9.36	8.19	54.7	57.5	1.5	56.1	0.0
2013	273	1122	9.64	8.01	53.1	61.4	-1.8	63.0	0.0
2013	273	1123	9.60	7.99	49.4	61.3	-2.9	64.2	-0.1
2013	273	1124	9.64	7.93	49.4	62.7	0.4	62.2	0.0
2013	273	1125	9.78	7.83	46.9	58.4	-2.7	61.1	0.0
2013	273	1126	10.04	7.61	41.1	56.7	-0.4	57.2	0.0
2013	273	1127	10.46	7.33	34.2	57.1	1.0	56.0	-0.1
2013	273	1128	10.56	7.32	28.8	55.6	-0.7	56.4	0.0
2013	273	1129	10.43	7.37	26.3	54.7	-2.5	57.0	0.0
2013	273	1130	10.57	7.23	26.4	56.7	0.7	55.8	0.0
2013	273	1131	10.67	7.16	26.1	57.4	0.4	56.9	0.0
2013	273	1132	8.96	8.57	12.3	19.3	-1.8	22.4	4.6
2013	273	1133	10.03	9.80	1.6	0.0	-0.1	0.0	-0.7
2013	273	1134	10.03	9.81	1.3	0.0	-0.1	0.0	-0.7
2013	273	1135	4.48	4.15	42.0	31.9	-3.6	44.3	28.2
2013	273	1136	0.10	0.10	90.0	88.1	-0.1	88.1	88.4
2013	273	1137	0.09	0.07	91.3	88.4	~~ 0.0	88.4	89.2
2013	273	1138	0.08	0.05	91.6	88.8	0.4	88.4	90.4
2013	273	1139	0.08	0.04	65.1	69.7	4.1	65.5	73.7
2013	273	1140	0.07	0.04	47.0	44.4	-0.1	44.0	46.4
2013	273	1141	0.07	0.03	47.0	44.4	-0.1	44.0	46.3
2013	273	1142	5.29	1.54	36.7	44.2	3.7	40.4	39.8
2013	273	1143	21.13	0.07	1.6	0.9	-2.0	3.2	3.3
2013	273	1144	21.17	0.06	0.9	0.0	-0.1	0.0	1.3
2013	273	1145	21.18	0.06	1.0	0.0	-0.1	0.0	1.3
2013	273	1146	21.19	0.05	0.9	0.0	-0.1	0.0	1.3
2013	273	1147	21.19	0.05	1.0	0.0	-0.1	0.0	1.2

09/30/13	3								
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	со
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1148	21.19	0.06	0.9	0.0	-0.1	0.0	1.3
2013	273	1149	21.20	0.06	0.9	0.0	-0.1	0.0	1.2
2013	273	1150	21.20	0.06	0.9	0.0	-0.1	0.0	1.1
2013	273	1151	21.20	0.06	0.9	0.0	-0.1	0.0	1.1
2013	273	1152	21.20	0.06	0.8	0.0	-0.1	0.0	1.2
2013	273	1153	21.20	0.05	0.8	0.0	-0.1	0.0	1.1
2013	273	1154	21.20	0.05	0.9	0.0	-0.1	0.0	1.1
2013	273	1155	21.20	0.05	0.8	0.0	-0.1	0.0	1.1
2013	273	1156	21.20	0.05	0.8	0.0	-0.1	0.0	1.1
2013	273	1157	21.20	0.05	0.9	0.0	-0.1	0.0	1.1
2013	273	1158	21.20	0.05	0.9	0.0	-0.1	0.0	1.0
2013	273	1159	21.20	0.05	0.9	0.0	-0.1	0.0	1.0
2013	273	1200	21.20	0.05	0.9	0.0	-0.1	0.0	0.9
2013	273	1201	21.20	0.05	0.9	0.0	-0.1	0.0	0.9
2013	273	1202	21.21	0.05	0.9	0.0	-0.1	0.0	0.9
2013	273	1203	21.21	0.05	0.9	0.0	-0.1	0.0	0.9
2013	273	1204	21.21	0.05	0.9	0.0	-0.1	0.0	0.9
2013	273	1205	21.21	0.05	0.9	-0.1	-0.1	0.0	0.9
2013	273	1206	21.20	0.05	0.9	0.0	-0.1	0.0	0.9
2013	273	1207	21.21	0.05	1.0	0.0	-0.1	0.0	0.9
2013	273	1208	21.21	0.05	0.9	0.0	-0.1	0.0	0.8
2013	273	1209	21.21	0.05	0.9	0.0	-0.1	0.0	0.8
2013	273	1210	21.21	0.04	0.9	0.0	-0.1	0.0	0.8
2013	273	1211	21.21	0.05	0.9	0.0	-0.1	0.0	0.7
2013	273	1212	21.21	0.05	0.9	0.0	-0.1	0.0	8.0
2013	273	1213	21.21	0.05	0.9	0.0	-0.1	0.0	0.8
2013	273	1214	21.21	0.05	1,0	0.0	-0.1	0.0	0.7
2013	273	1215	21.21	0.05	0.9	0.0	-0.1	0.0	0.7
2013	273	1216	21.20	0.05	0.9	0.0	-0.1	0.0	0.6
2013	273	1217	21.20	0.05	0.9	0.0	-0.1	0.0	0.6
2013	273	1218	21.21	0.04	0.9	0.0	-0.1	0.0	0.6
2013	273	1219	21.21	0.04	1.0	0.0	-0.1	0.0	0.6
2013	273	1220	21.21	0.04	0.9	0.0	-0.1	0.0	0.6
2013	273	1221	21.21	0.04	0.9	0.0	-0.1	0.0	0.6
2013	273	1222	21.21	0.04	0.9	0.0	-0.1	0.0	0.6
2013 2013	273	1223	21.21	0.04	1.0	0.0	-0.1	0.0	0.5
2013	273 273	1224	21.21	0.04	1.0	0.0	-0.1	0.0	0.5
2013	273 273	1225	21.21 21.21	0.04	0.9	0.0	-0.1	0.0	0.5
2013	273	1226 1227		0.05	0.9	0.0	-0.1	0.0	0.5
2013	273	1228	21.21 21.21	0.05 0.05	0.9 0.9	0.0 0.0	-0.1	0.0	0.5
2013	273	1229	21.21	0.03	0.9	0.0	-0.1	0.0	0.5
2013	273	1230	21.21	0.04	0.9	-0.1	-0.1	0.0	0.5
2013	273	1231	21.21	0.04	0.9	0.0	-0.1 -0.1	0.0	0.5
2013	273	1232	21.21	0.04	0.9	0.0	-0.1 -0.1	0.0	0.4
2013	273	1233	21.21	0.04	0.8	0.0	-0.1 -0.1	0.0	0.5
2013	273	1234	21.20	0.04	0.8	0.0	-0.1 -0.1	0.0	0.4
2013	273	1235	21.21	0.04	0.9	0.0	-0.1 -0.1	0.0 0.0	0.4 0.4
2013	273	1236	21.21	0.04	0.9	0.0	-0.1 -0.1	0.0	
2013	273	1237	21.21	0.04	0.8	0.0	-0.1 -0.1	0.0	0.4 0.4
2013	273	1238	21.21	0.04	0.8	0.0	-0.1 -0.1	0.0	0.4
2013	273	1239	21.21	0.04	0.9	0.0	-0.1	0.0	0.4
2013	273	1240	21.21	0.05	0.8	0.0	-0.1 -0.1	-0.1	0. 4 0.4
2013	273	1241	21.21	0.05	0.8	0.0	-0.1	0.0	0.4
2013	273	1242	21.21	0.03	0.8	0.0	-0.1	0.0	0.4
2013	273	1243	21.21	0.04	0.9	0.0	-0.1	0.0	0.4
2013	273	1244	21.21	0.04	0.9	0.0	-0.1	0.0	0.4
						5.5	3.1	5.0	5.5

09/30/13			,						
Year	Julian	Time	02	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1245	21.22	0.04	0.8	0.0	-0.1	0.0	0.4
2013	273	1246	21.21	0.04	0.9	0.0	-0.1	0.0	0.3
2013	273	1247	21.21	0.04	1.0	0.0	-0.1	0.0	0.3
2013	273	1248	15.09	4.36	4.2	27.0	2.0	28.5	0.0
2013	273	1249	10.47	7.47	13.5	58.7	-3.7	63.3	-1.3
2013	273	1250	10.49	7.42	16.9	62.1	0.4	61.7	-1.5 -1.5
2013	273	1251	10.56	7.36	18.4	62.2	-0.8	63.0	-1.5 -1.5
2013	273	1252	10.75	7.33	21.5	60.0	-4.6	64.7	-1.4
2013	273	1253	9.27	9.15	39.6	96.3	-1.4	100.4	-0.3
2013	273	1254	9.47	8.86	39.2	104.6	-2.2	100.4	-0.3 -1.3
2013	273	1255	8.98	8.96	39.5	79.4	-2.2 -3.3	82.7	
2013	273	1256	8.54	9.12	31.3	56.4	-3.3 -4.2		-1.8
2013	273	1257	8.78	8.81	28.6	50.4 51.5		60.6	-1.8
2013	273	1258	9.50	8.38			1.1	50.2	-1.8
2013	273	1259	9.30		30.4	48.8	0.4	48.3	-1.8
2013	273	1300		8.62	26.9	46.7	-1.3	47.9	-1.8
2013			9.39	8.33	23.9	49.7	0.3	49.4	-1.8
	273	1301	10.02	7.83	22.5	50.5	-2.3	52.6	-1.8
2013	273	1302	10.63	7.49	18.4	53.0	2.8	50.1	-1.7
2013	273	1303	10.23	7.77	16.9	50.1	-2.6	52.6	-1.7
2013	273	1304	10.17	7.74	16.9	53.3	-0.1	53.2	-1.7
2013	273	1305	10.53	7.45	15.4	53.6	-1.9	55.4	-1.8
2013	273	1306	11.00	7.17	14.7	54.1	0.4	53.8	-1.8
2013	273	1307	10.75	7.39	13.1	53.6	-0.7	54.2	-1.8
2013	273	1308	10.73	7.37	13.0	53.3	-3.8	57.5	-1.3
2013	273	1309	9.25	8.76	23.8	67.0	2.3	64.5	-0.2
2013	273	1310	9.32	8.66	32.7	57.9	-4.1	61.9	-1.7
2013	273	1311	9.62	8.40	29.2	52.3	1.3	51.0	-1.9
2013	273	1312	9.60	8.28	27.4	53.0	-2.6	55.6	-1.8
2013	273	1313	9.95	7.95	24.9	55.1	-0.1	55.2	-1.9
2013	273	1314	10.80	7.38	21.9	55.6	-1.0	56.4	-1.8
2013	273	1315	10.88	7.35	19.8	57.1	1.7	55.3	-1.8
2013	273	1316	10.63	7.42	18.3	56.8	-3.3	60.1	-1.8
2013	273	1317	10.79	7.25	17.8	59.8	-0.2	59.9	-1.8
2013	273	1318	11.44	6.81	16.3	58.9	-2.4	61.3	-1.7
2013	273	1319	11.32	6.95	16.0	61.5	1.7	59.7	-1.8
2013	273	1320	11.07	7.04	16.1	60.8	-4.9	65.4	-1.8
2013	273	1321	11.25	6.90	14.1	65.3	0.8	64.4	-1.8
2013	273	1322	11.46	6.69	14.0	64.5	-3.2	67.8	-1.8
2013	273	1323	11.88	6.45	12.7	66.3	0.8	65.7	-1.8
2013	273	1324	11.68	6.72	14.4	63.2	-3.2	66.6	-1.5
2013	273	1325	11.00	7.38	19.6	54.1	-2.0	56.0	-1.4
2013	273	1326	9.97	8.00	27.3	52.3	0.5	51.7	-1.8
2013	273	1327	10.64	7.44	26.4	52.9	-3.5	56.3	-1.9
2013	273	1328	11.02	7.25	23.2	56.2	2.2	54.0	-1.9
2013	273	1329	10.65	7.41	23.3	53.7	-5.0	58.7	-1.8
2013	273	1330	10.74	7.29	25.1	59.8	1.0	58.7	-1.8
2013	273	1331	11.16	6.94	25.7	57.6	-3.5	61.0	-1.8
2013	273	1332	11.52	6.79	22.3	59.9	3.5	56.3	-1.8
2013	273	1333	11.11	7.02	21.5	57.2	-2.9	59.9	-1.8 -1.8
2013	273	1334	11.14	6.95	20.5	59.2	-2.9 -1.6	60.7	-1.8 -1.8
2013	273	1335	11.26	6.86	21.6	61.6	1.3		
2013	273	1336	10.76	7.18	26.5	57.9		60.4	-1.8
2013	273	1337	9.67	7.16 7.94	36.9	57.9 47.2	-2.5 0.0	60.5	-1.8
2013	273	1337	9.67 8.98	8.39	35.9		0.0	47.2	-2.0
2013	273	1339	0.96 10.54	8.39 7.26		45.6	-1.8	47.2 50.0	-2.0
2013	273 273	1339 1340			27.6	50.8	-0.2	50.9	-1.9
2013	273 273		11.82	6.52	22.4	62.5	0.9	61.6	-1.6
2013	213	1341	9.33	8.70	37.9	64.3	0.4	64.1	-1.3

09/30/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1342	8.68	8.90	48.7	52.9	-2.6	55.5	-2.1
2013	273	1343	9.44	8.29	43.3	49.8	-1.9	51.4	-2.1
2013	273	1344	10.19	7.79	37.9	51.9	-0.5	52.3	-2.0
2013	273	1345	10.26	7.75	32.5	55.5	1.2	54.3	-1.9
2013 .	273	1346	10.28	7.65	30.3	56.6	-2.3	58.8	-2.0
2013	273	1347	10.52	7.47	28.2	59.9	-0.1	59.9	-1.9
2013	273	1348	10.65	7.35	26.9	62.9	1.2	61.7	-1.8
2013	273	1349	10.91	7.12	24.9	62.0	-3.3	65.3	-1.9
2013	273	1350	11.34	6.89	22.7	64.3	-0.4	64.6	-1.8
2013	273	1351	11.00	7.11	23.4	65.7	-0.4	65.9	-1.8
2013	273	1352	11.02	7.04	24.3	66.0	-3.6	69.7	-1.8
2013	273	1353	11.11	6.97	22.9	68.5	0.7	67.9	-1.8
2013	273	1354	11.29	6.81	21.6	67.3	-2.0	69.2	-1.8 -1.8
2013	273	1355	11.76	6.47	23.4	65.9	-2.0 -3.1	68.8	-1.8 -1.8
2013	273	1356	12.54	6.09	20.7	67.5	-3.1 1.4		
2013	273	1357	9.15	8.59	36.7	77.6		66.0	-0.9
2013	273	1358	10.30	7.77	67.8		0.5	76.9	-0.6
2013	273	1359	9.74	8.12		138.5	1.3	137.2	-1.8
2013	273	1400	9.74 9.35	8.33	73.5	121.1	-0.4	121.5	-1.6
2013	273	1401	9.35		67.6	89.6	1.7	90.7	-0.7
2013	273 273		9.37 10.09	8.23	48.9	59.0	-0.3	59.2	-0.9
2013	273 273	1402 1403		7.69	37.3	60.8	-3.0	63.6	-0.8
2013	273 273		10.28	7.66	37.8	62.1	1.7	60.3	-0.1
		1404	9.87	7.88	37.4	62.2	-1.0	63.1	0.3
2013	273	1405	9.95	7.79	33.6	62.8	-0.1	62.8	1.7
2013	273	1406	10.32	7.49	33.5	64.0	-0.3	64.1	0.5
2013	273	1407	10.74	7.26	30.1	62.3	-2.3	64.4	0.7
2013	273	1408	10.43	7.50	28.3	62.7	0.5	62.1	1.1
2013	273	1409	10.30	7.53	29.7	62.5	-1.8	64.2	1.3
2013	273	1410	10.58	7.27	27.0	62.9	1.0	61.6	1.2
2013	273	1411	11.23	6.87	24.4	59.9	-3.0	62.7	1.3
2013	273	1412	10.95	7.10	23.1	64.1	2.1	62.0	1.6
2013	273	1413	9.16	6.17	37.5	63.5	-7.0	78.1	5.4
2013	273	1414	0.09	0.10	83.8	83.2	-1.6	85.8	77.5
2013	273	1415	0.06	0.04	90.2	87.4	0.1	87.4	93.0
2013	273	1416	0.05	0.03	90.8	87.9	0.4	87.4	92.0
2013	273	1417	0.04	0.02	90.9	87.9	0.4	87.6	92.1
2013	273	1418	0.05	0.01	79.8	80.6	0.5	80.3	87.1
2013	273	1419	0.04	0.01	46.8	44.5	-0.3	44.8	49.6
2013	273	1420	0.03	0.01	46.4	43.9	0.0	43.5	47.0
2013	273	1421	0.04	0.01	46.5	43.9	0.0	43.5	46.8
2013	273	1422	4.20	4.37	31.8	36.4	7.4	28.7	38.5
2013	273	1423	9.99	9.80	2.4	0.3	-0.1	0.2	2.1
2013	273	1424	10.00	9.82	1.6	0.0	-0.1	0.0	0.1
2013	273	1425	12.72	6.38	3.1	26.1	-2.7	30.4	0.4
2013	273	1426	21.11	0.07	1.2	4.4	2.4	1.8	1.9
2013	273	1427	21.14	0.05	1.1	0.0	-0.1	0.0	2.0
2013	273	1428	21.15	0.05	1.0	-0.1	-0.1	0.0	1.9
2013	273	1429	21.15	0.05	1.0	0.0	-0.1	0.0	1.8
2013	273	1430	21.16	0.04	1.0	0.0	-0.1	0.0	1.6
2013	273	1431	21.16	0.04	1.0	0.0	-0.1	0.0	1.5
2013	273	1432	21.17	0.04	1.0	0.0	-0.1	0.0	1.4
2013	273	1433	21.17	0.04	1.0	0.0	-0.1	0.0	1.3
2013	273	1434	21.17	0.04	1.0	0.0	-0.1	0.0	1.3
2013	273	1435	21.17	0.04	0.9	0.0	-0.1	0.0	1.2
2013	273	1436	21.17	0.04	1.0	0.0	-0.1	0.0	1.1
2013	273	1437	21.17	0.04	1.0	0.0	-0.1	0.0	1.0
2013	273	1438	21.18	0.04	1.0	0.0	-0.1	0.0	0.9

09/30/13	1								
Year	Julian	Time	02	CO2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1439	21.18	0.04	1.0	0.0	0.0	0.0	0.9
2013	273	1440	21.18	0.04	1.0	0.0	-0.1	0.0	0.8
2013	273	1441	21.18	0.04	0.9	0.0	-0.1	0.0	0.8
2013	273	1442	21.18	0.04	1.0	0.0	-0.1	0.0	0.7
2013	273	1443	21.18	0.04	1.0	0.0	-0.1	0.0	0.6
2013	273	1444	21.18	0.04	1.0	0.0	-0.1	0.0	0.6
2013	273	1445	21.18	0.04	1.0	0.0	-0.1	0.0	0.6
2013	273	1446	21.18	0.04	1.0	0.0	-0.1	0.0	0.5
2013	273	1447	21.18	0.04	0.9	0.0	-0.1	0.0	0.5
2013	273	1448	21.18	0.03	1.0	0.0	-0.1	0.0	0.4
2013	273	1449	21.18	0.04	1.0	0.0	-0.1	0.0	0.4
2013	273	1450	21.19	0.03	1.0	0.0	-0.1	0.0	0.4
2013	273	1451	21.19	0.03	0.9	0.0	-0.1	0.0	0.3
2013	273	1452	21.19	0.04	0.9	0.0	-0.1	0.0	0.3
2013	273	1453	21.19	0.04	1.0	0.0	-0.1	0.0	0.2
2013	273	1454	21.18	0.04	0.8	0.0	0.0	0.0	0.2
2013	273	1455	21.18	0.04	0.9	0.0	-0.1	0.0	0.1
2013	273	1456	21.19	0.04	0.9	0.0	0.0	0.0	0.1
2013	273	1457	21.19	0.04	0.9	0.0	-0.1	0.0	0.1
2013	273	1458	21.19	0.03	0.9	0.0	-0.1	0.0	0.0
2013	273	1459	21.19	0.03	0.9	0.0	-0.1	0.0	-0.1
2013	273	1500	21.19	0.03	0.9	0.0	-0.1	0.0	-0.1
2013	273	1501	21.19	0.03	0.8	0.0	-0.1	0.0	-0.1
2013	273	1502	21.19	0.03	0.9	0.0	0.0	0.0	-0.2
2013	273	1503	21.19	0.03	0.9	0.0	-0.1	0.0	-0.2
2013	273	1504	21.19	0.03	0.9	0.0	-0.1	0.0	-0.2
2013	273	1505	19.69	1.18	1.0	1.1	-1.2	4.3	-0.3
2013	273	1506	12.32	6.16	3.9	61.7	-1.6	66.4	-0.1
2013 2013	273	1507	9.05	8.87	12.2	57.3	3.4	53.9	-1.7
2013	273 273	1508 1500	9.40	8.34	23.0	56.2	1.3	54.6	-2.0
2013	273 273	1509 1510	10.07	7.95	24.6	53.7	-0.3	54.0	-1.9
2013	273	1510	9.74 10.28	8.03 7.55	23.5	52.6	-2.7	55.2	-1.9
2013	273	1512	10.28	7.55	21.5 15.2	55.5 54.6	1.9	53.6	-2.0
2013	273	1513	10.51	7.23 7.40	16.0	58.9	-2.3 -2.2	56.9 61.2	-1.9 -2.0
2013	273	1514	10.85	7.09	17.0	66.3	1.9	64.2	-2.0 -2.0
2013	273	1515	11.60	6.64	15.8	63.5	-5.7	69.0	-2.0 -2.0
2013	273	1516	11.05	7.01	14.8	69.9	3.5	66.5	-2.0 -1.9
2013	273	1517	10.95	7.01	14.9	69.1	-3.2	72.6	-1. 9 -2.1
2013	273	1518	11.71	6.46	13.6	69.7	-3.8	73.8	-2.1
2013	273	1519	11.52	6.68	12.0	72.3	1.6	70.7	-2.0
2013	273	1520	11.26	6.78	12.2	71.4	-4.7	76.4	-2.1
2013	273	1521	11.54	6.52	12.4	76.1	2.6	73.6	-2 .1
2013	273	1522	12.51	6.22	12.2	65.4	-6.0	71.5	-1.6
2013	273	1523	8.73	9.06	23.7	56.2	-3.2	60.0	-1.9
2013	273	1524	9.23	8.61	30.8	55.6	1.3	54.4	-2.3
2013	273	1525	9.22	8.68	30.4	52.1	1.3	50.6	-2.3
2013	273	1526	9.11	8.59	30.2	49.6	-2.2	51.8	-2.3
2013	273	1527	10.07	7.85	28.2	54.1	-0.6	54.4	-2.3
2013	273	1528	10.07	7.93	24.3	53.7	1.2	52.5	-2.3
2013	273	1529	9.86	7.96	22.1	52.8	-2.8	55.4	-2.3
2013	273	1530	10.41	7.52	22.2	54.9	0.4	54.5	-2.3
2013	273	1531	10.46	7.60	22.7	53.7	-1.0	54.6	-2.3
2013	273	1532	9.94	7.87	19.6	54.1	-1.0	55.1	-2.3
2013	273	1533	10.25	7.59	20.9	56.2	0.6	55.3	-2.3
2013	273	1534	10.79	7.33	21.2	52.7	-4.2	56.6	-2.3
2013	273	1535	10.15	7.70	21.8	55.2	0.1	55.0	-2.3

09/30/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1536	10.71	7.25	21.6	57.7	1.2	56.5	-2.3
2013	273	1537	10.84	7.27	18.8	52.8	-1.7	54.3	-2.3
2013	273	1538	10.80	7.22	20.3	56.1	-0.1	56.3	-2.3
2013	273	1539	9.44	8.51	34.8	86.4	1.5	84.9	-2.0
2013	273	1540	10.00	8.21	48.0	103.4	-4.1	107.4	-2.3
2013	273	1541	8.92	8.88	55.0	88.0	1.2	86.7	-2.3
2013	273	1542	8.92	8.67	49.6	72.0	-2.2	74.4	-2.3
2013	273	1543	9.11	8.60	42.5	59.5	0.5	59.0	-2.3
2013	273	1544	8.81	8.62	41.0	51.0	0.0	51.0	-2.3
2013	273	1545	9.74	8.04	35.5	46.4	-1.4	48.0	-2.3
2013	273	1546	9.16	8.45	29.0	46.8	1.9	44.8	-2.3
2013	273	1547	9.44	8.12	27.8	46.4	-0.4	46.6	-2.3
2013	273	1548	10.14	7.75	24.9	44.2	-2.8	47.0	-2.3
2013	273	1549	9.49	8.14	25.4	47.5	1.3	46.1	-2.3 -2.3
2013	273	1550	10.31	7.50	27.0	48.3	-0.3	48.5	-2.3 -2.3
2013	273	1551	10.01	7.81	25.8	49.2	1.8	47.3	-2.3 -2.3
2013	273	1552	9.98	7.69	26.5	49.5	-1.2	50.6	-2.3 -2.3
2013	273	1553	10.79	7.22	23.0	49.9 47.9	-1.2 -3.5	51.2	-2.3 -2.3
2013	273	1554	9.71	8.04	33.9	60.8	0.8	62.5	-2.3 -2.1
2013	273	1555	9.12	8.72	33. 3 34.7	61.7			
2013	273	1556	9.12 8.80	8.67	39.0	67.8	-5.2 5.5	69.7	-1.7
2013	273	1557	9.71	8.10	39.0 34.2			62.2	-2.3
2013	273	1557	9.71	8.53	35.1	57.3 51.6	0.7	56.7	-2.3
2013	273	1559	9.86	7.87	31.7		2.5 0.3	49.1	-2.3
2013	273	1600		7.83		50.8		50.5	-2.3
2013	273	1600	10.09		26.2	49.3	-1.5	50.6	-2.3
2013	273 273		9.77	7.92	25.1	51.5	-1.2	52.6	-2.3
2013	273 273	1602	10.90	7.16	24.9	49.8	-3.5°	53.4	-2.3
		1603	10.09	7.69	25.7	52.4	0.5	51.9	-2.3
2013	273	1604	11.01	6.99	26.9	53.4	-0.1	53.3	-2.3
2013	273	1605	10.74	7.28	23.4	53.8	0.6	53.2	-2.3
2013	273	1606	10.58	7.25	22.8	55.8	-1.5	57.3	-2.3
2013	273	1607	11.37	6.78	21.6	54.6	-5.1	59.4	-2.3
2013	273	1608	10.66	7.27	18.8	59.5	3.1	56.3	-2.3
2013 2013	273 273	1609	10.93	6.98	16.7	59.4	0.0	59.5	-2.3
		1610	10.96	7.20	20.7	54.5	-3.8	58.4	-2.3
2013	273	1611	9.00	8.51	28.8	58.5	-2.7	61.2	-2.3
2013	273	1612	9.49	8.05	33.3	54.1	-0.6	55.3	-2.3
2013	273	1613	10.17	7.71	28.3	43.6	-0.6	44.4	-2.3
2013	273	1614	10.12	7.63	28.8	47.8	-1.6	49.3	-2.3
2013 2013	273 273	1615	11.06	6.95	29.1	54.0	0.9	53.0	-2.3
2013	273 273	1616	10.82	7.22	29.4	55.4	-1.1	56.6	-2.3
		1617	10.58	7.27	33.9	58.9	-3.6	62.6	-2.3
2013	273	1618	11.54	6.67	30.5	59.5	-3.2	62.6	-2.3
2013	273	1619	10.71	7.22	35.1	66.2	3.1	63.0	-2.3
2013	273	1620	11.09	6.88	36.7	67.8	0.5	67.2	-2.3
2013	273	1621	11.50	6.72	41.0	64.6	-6.0	70.6	-2.3
2013	273	1622	10.86	7.08	36.7	67.5	-1.6	69.0	-2.3
2013	273	1623	11.40	6.65	24.6	71.1	2.8	68.2	-2.3
2013	273	1624	11.29	6.85	18.7	66.0	-2.3	68.2	-2.3
2013	273	1625	10.84	7.06	19.4	66.9	-4.2	71.1	-2.3
2013	273	1626	11.83	6.53	21.2	64.6	0.2	64.3	-2.3
2013	273	1627	9.17	8.64	33.3	74.1	8.0	73.1	-2.3
2013	273	1628	8.75	8.76	44.9	75.3	0.9	74.5	-2.3
2013	273	1629	9.78	8.10	37.9	48.2	-2.0	50.2	-2.3
2013	273	1630	9.39	8.29	31.7	48.1	2.1	46.1	-2.3
2013	273	1631	10.15	7.69	30.7	50.3	1.2	49.2	-2.3
2013	273	1632	10.35	7.67	26.8	48.3	-2.5	51.0	-2.3

09/30/13									
Year	Julian	Time	O2	CQ2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1633	9.84	7.88	27.0	51.0	-2.6	53.8	-2.3
2013	273	1634	10.75	7.30	25.1	51.5	-0.7	52.2	-2.3
2013	273	1635	10.15	7.76	22.9	53.7	1.7	51.8	-2.3
2013	273	1636	10.46	7.41	23.9	54.1	0.0	53.9	-2.3
2013	273	1637	10.90	7.23	20.1	53.4	-3.9	57.2	-2.3
2013	273	1638	10.45	7.39	22.2	57.3	-3.9 -3.1	60.5	-2.3 -2.3
2013	273	1639	11.32	6.88	19.7	57.3	-3.1 -2.1		
2013	273	1640	10.58	7.35	17.9	61.1		59.3	-2.3
2013	273	1641					2.9	58.1	-2.3
2013	273 273		11.17	6.87	19.1	61.0	1.7	59.2	-2.3
		1642	11.35	6.95	20.7	58.0	-3.2	61.2	-2.3
2013	273	1643	9.99	7.75	26.0	56.9	1.5	55.2	-2.3
2013	273	1644	10.97	7.03	27.6	60.6	2.3	58.3	-2.3
2013	273	1645	10.74	7.28	24.8	64.4	1.1	63.3	-2.3
2013	273	1646	10.99	6.97	26.1	67.2	-3.3	70.5	-2.3
2013	273	1647	11.77	6.54	21.7	64.6	-4.7	69.4	-2.3
2013	273	1648	10.98	7.04	20.8	67.1	3.5	63.5	-2.3
2013	273	1649	11.00	6.98	21.9	62.9	-4.5	67.3	-2.3
2013	273	1650	11.68	6.55	20.1	64.1	-0.9	64.9	-2.3
2013	273	1651	11.23	6.89	18.7	64.3	0.0	64.3	-2.3
2013	273	1652	11.23	6.84	18.8	64.9	0.0	64.6	-2.3
2013	273	1653	11.32	6.77	18.7	63.7	-3.7	67.3	-2.3
2013	273	1654	11.74	6.45	18.3	66.1	0.9	65.2	-2.3
2013	273	1655	11.88	6.44	16.9	61.4	-5.2	66.5	-2.3
2013	273	1656	11.57	6.59	15.6	66.6	2.6	64.1	-2.3
2013	273	1657	11.56	6.58	16.1	66.3	-1.8	68.0	-2.3
2013	273	1658	12.46	6.01	17.7	70.5	1.1	69.4	-2.2
2013	273	1659	9.41	8.33	30.3	68.3	2.0	66.3	-2.1
2013	273	1700	8.43	8.85	48.6	70.6	-1.0	72.5	-2.3
2013	273	1701	9.55	8.11	50.0	53.2	-1.7	54.8	-2.3
2013	273	1702	8.69	8.72	48.3	52.5	1.6	50.8	-2.3 -2.3
2013	273	1702	9.30	8.21	48.5	52.5	0.3	50.8 52.0	
2013	273	1703	9.16	8.42	44.9	47.0	-1.1	48.2	-2.3
2013	273	1704	9.00		•				-2.3
2013	273 273			8.41	46.3	46.9	-2.1	49.1	-2.3
2013	273	1706	9.78	7.94	46.9	46.3	-0.2	46.7	-2.3
		1707	8.99	8.49	49.1	46.9	1.2	45.5	-2.3
2013	273	1708	9.23	8.24	51.5	46.9	0.0	46.8	-2.3
2013	273	1709	9.25	8.36	48.0	47.5	-2.5	49.8	-2.3
2013	273	1710	8.70	8.63	49.3	51.8	-0.7	52.3	-2.3
2013	273	1711	9.42	8.14	47.2	53.8	0.8	52.9	-2.3
2013	273	1712	8.90	8.59	45.8	54.4	-2 .7	57.2	-2.3
2013	273	1713	8.93	8.45	50.1	65.6	3.6	62.0	-2.3
2013	273	1714	9.07	8.50	46.6	65.6	-0.2	65.8	-2.3
2013	273	1715	8.73	8.58	52.1	70.1	3.1	67.1	-2.3
2013	273	1716	9.40	8.26	48.4	67.1	-1.1	68.2	-2.3
2013	273	1717	9.36	8.77	35.6	43.4	-4.8	50.9	-2.3
2013	273	1718	10.04	9.83	1.9	0.3	0.1	0.0	-2.3
2013	273	1719	10.04	9.84	1.3	0.0	0.0	0.0	-0.6
2013	273	1720	10.04	9.85	1.1	0.0	0.0	0.0	0.1
2013	273	1721	2.84	2.57	56.2	57.5	12.9	44.7	42.5
2013	273	1722	0.07	0.09	89.7	88.7	-0.1	88.5	91.1
2013	273	1723	0.06	0.06	90.4	89.0	0.3	88.6	91.2
2013	273	1724	0.05	0.04	90.3	88.4	-0.2	88.5	91.3
2013	273	1725	0.06	0.03	51.8	55.2	2.9	52.1	60.1
2013	273	1726	0.05	0.02	46.5	44.1	-0.1	44.0	46.6
2013	273	1727	0.04	0.02	46.4	44.0	· 0.0	44.0	46.5
2013	273	1728	1.58	0.02	43.7	42.2	-0.7		
2013	273 273	1729						44.0	45.6
2013	213	1729	19.91	11.43	4.0	2.1	-2.9	7.5	9.7

SMMI - Pogo Mine

09/30/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	СО
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	273	1730	20.11	19.87	0.7	0.0	0.0	0.0	-0.8
2013	273	1731	20.12	19.71	0.7	0.0	0.0	0.0	-0.9
2013	273	1732	20.13	19.73	0.6	0.0	0.0	0.0	-1.0
2013	273	1733	11.16	10.52	0.6	0.0	0.0	0.0	-0.5
2013	273	1734	10.08	9.78	0.5	0.0	-0.1	0.0	0.1
2013	273	1735	5.04	4.61	47.9	81.1	0.5	100.8	43.1
2013	273	1736	0.02	0.03	100.6	234.4	0.1	234.4	100.3
2013	273	1737	0.01	0.02	100.6	235.0	0.6	234.4	100.3
2013	273	1738	0.00	0.01	100.6	227.9	3.9	224.7	100.3
2013	273	1739	-0.01	0.00	94.4	95.8	-2.4	104.2	96.1
2013	273	1740	-0.01	0.00	92.1	90.7	0.4	90.5	92.0
2013	273	1741	-0.01	-0.01	92.0	90.6	0.4	90.5	92.0
2013	273	1742	-0.02	-0.01	57.5	59.6	1.3	58.2	66.0
2013	273	1743	-0.02	-0.01	46.3	45.0	0.2	44.5	46.8
2013	273	1744	-0.02	-0.01	46.2	44.0	0.2	44.5	40.0

Table 7 Continuous Emissions Measurements Result Run 129-3

Time	NOx	, NO		co	co		SO2	so		02	02	CO2	co
-min)	(ppm)	(ppm Cor.)	(lb/hr)	(ppm)	(ppm Cor.)	(lb/hr)	(ppm)	(ppm Cor.)	(ib/hr)	(%)	(% Cor.)	(%)	(% Co
869 900	60.1 61.9	51.1 53.0	0.31 0.32	4.3 1.8	4.1 1.4	0.02 0.01	2.1 2.3	1.6	0.01	12.76	12.70	6.47	5.68
901	39.6	40.3	0.24	0.7	0.6	0.00	4.4	1.9 4.0	0.02 0.03	12.83 10.22	12.78 10.17	5.75 7.63	5.96 7.92
902 903	40.1 45.8	41.0 46.7	0.26 0.28	0.7 0.0	0.6 -0.2	0.00	4.6 4.3	4.1 3.9	0.03	10.80 11.16	10.76 11.11	7.11 6.72	7.38 6.97
904	48.1	49.1	0.30	0.7	0.6	0.00	4.3	3.9	0.03	11.10	11.11	6.67	6.92
906 906	48.1 51,6	49.1 52.7	0.30 0.32	1.1	1.0	0.00 0.00	3.8 3.7	3.4 3.3	0.03	11.74 11.90	11.69 11.86	6.30 6.19	6.54
907	52.6	63.6	0.32	0.9	0.8	0.00	4.2	3.7	0.03	12.07	12.02	6.08	6.30
808 809	52.3 52.1	63.4 63.2	0.32 0.32	1.3 2.2	1.1 2.1	0.00	4.3	3.9 3.6	0.03	11.98 12.05	11.93 12.00	6.10 6.12	6.31
910	50.0	61.0	0.31	2.7	2.5	0.01	3.6	3.0	0.03	12.21	12.16	5.98	6.20
911 912	48.7 61.7	49.7 52.8	0.30 0.32	2.5 2.0	2.3 1.8	0.01 0.01	3.7	3.3 3.4	0.03 0.03	12.27 12.28	12.22 12.23	5.94 5.92	6.1 6.1
913	50.1	51.1	0.31	2.0	1.8	0.01	3.7	3.2	0.03	12.33	12.28	6.87	6.0
914 915	50.0 52.6	51.0 53.7	0.31 0.32	2.0 2.5	1.8 2.3	0.01 0.01	3.1	2.7 2.5	0.02 0.02	12.03 12.45	11.98 12.40	6.06 5.78	6.21 5.91
916 917	68.0 69.3	59.3 70.7	0.36 0.43	12.9	12.6	0.05	2.6	2.2	0.02	13.76	13.71	5.01	5.19
918	59.0	60.2	0.36	1.4	1.2 1.2	0.00	5.1 6.3	4.7 5.8	0.04 0.05	9.98	9.91	7.72 7.29	8.0 7.5
919 920	52.6 54.3	63.7 55.5	0.32 0.33	1.8 1.7	1.7 1.6	0.01 0.01	6.1	5.7	0.05	11.18	11.13	6.73	6.98
921	54.7	65.9	0.34	1.7	1.5	0.01	6.6 6.3	6.0 6.9	0.05 0.05	11.65 11.85	11.60 11.80	6.38 6.23	6.63
922	52.9 52.4	64.0 63.6	0.33 0.32	1.9 2.0	1.7 1.8	0.01 0.01	6.3 6.0	4.8 4.6	0.04	11.84 11.82	11.89 11.77	6.14 6.24	6.30
924	62.6	63.6	0.32	2.2	2.1	0.01	4.6	4.2	0.04	12.18	12.13	5.98	6.47 6.21
925	64.2 54.8	55.3 56.9	0.33 0.34	2.1 2.0	2.0 1.8	0.01 0.01	4.6	4.0 3.9	0.03	12.19 12.27	12.14	5.97 5.91	6.15
27	51.4	62.6	0.32	2.0	1.9	0.01	4.0	3.6	0.03	12.41	12.36	6.82	6.13 6.03
928 929	50.4 52.1	61.6 53.2	0.31 0.32	2.0 2.0	1.8 1.8	0.01 0.01	4.1 4.1	3.7 3.7	0.03	12.44 12.47	12.39 12.42	6.80 6.77	6.01 6.98
930	54.7	65.9	0.34	1.8	1.6	0.01	4.1	3.7	0.03	12.43	12.38	6.79	6.01
31	62.8 89.3	84.1 91.1	0,39 0.65	1.8 1.4	1.7 1.3	0.01	4.0 7.5	3.6 7.0	0.03 0.08	12.78	12.74	5.63	5.74
33	116.6	118.9	0.72	-0.2	-0.4	0.00	22.1	21.6	0.18	11.47 8.98	11.42 8.91	7.06 8.94	7.33 9.28
34	102.6 59.3	104.7 60.6	0.63 0.37	-0.2 0.1	-0.4 0.0	0.00	26.3 21.4	26.7 20.9	0.22 0.18	8.40 9.45	8.36 9.40	9.11 8.22	9,46
38	61.3	62.4	0.32	0.2	0.1	0.00	17.0	16.5	0.14	9.88	9,83	7.83	8.53 8.13
37	62.0 64.3	63.1 66.6	0.32 0.33	0.2 0.2	0.0 0.0	0.00	14.0 12.2	13.5 11.7	0.11 0.10	10.47 10.78	10.42 10.73	7.36 7.11	7.64
39	56.5	67.7	0.36	0.2	0.1	0.00	11.1	10.6	0.09	11.07	11.02	6.89	7.38 7.16
140 141	67.1 69.0	58.3 60.2	0.35 0.36	0.3 0.2	0.1 0.1	0.00 0.00	9.6 8.6	9.1 8.1	0.0B 0.07	11.28 11.48	11.23 11.41	6.71 6.55	6.96
42	69.3	60.6	0.37	0.3	0.2	0.00	7.9	7.4	0.06	11.54	11.49	6,49	6.80 6.73
43 44	60.0 69.4	61.2 60.6	0.37 0.37	0.3 0.4	0.1 0.2	0.00 0.00	7.6 7.2	7.2 6.7	0.06	11.67	11.52	6.46	6.70
45	60.3	61.5	0.37	0.3	0.1	0.00	6.5	6.0	0.06	11.70 11.69	11.65 11.64	6.37 6.37	6,61 6,61
46	60.9 62.5	62.1 63.8	0.37 0.38	0.6 0.3	0.3 0.1	0.00	6.4 6.4	6.0 6.0	0.05	11.73	11.68	6.34	- 6,68
48	107.7	109.9	0.66	0.7	0.6	0.00	17.9	17.4	0.05 0.15	11.95 10.61	11.90 10.58	6.20 7.70	6.43 7.89
60	218.7 173.7	223.1 177.2	1.35 1.07	1.2 2.2	1.1 2.0	0.00 0.01	60.6 62.5	49.7 61.7	0.42 0.43	9,73	9.68	8.34	8.66
51	140.3	143.2	0.86	1.5	1.3	0.00	47.7	48.9	0.39	9.56 9.28	9.51 9.23	8.32 8.43	8.64 8.75
52 53	138.5 120.1	141,3 122,6	0.85 0.74	-0.2 0.0	-0.4 -0.2	0.00	50.2	49.4	0.41	8.86	8.81	8.66	8.99
54	102.9	105.0	0.63	-0.3	-0.4	0.00	60.0 44.0	49.2 43.2	0.41 0.36	9.12 9.20	9.07 9.15	8,46 8,40	8.78 8.72
66 68	76.5 56.4	78.1 56.5	0.47 0.34	-0.3 -0.6	-0.6 -0.7	0.00 0.00	39.8 25.1	39.0 24.5	0.33 0.21	8.88 10.81	8.83 10.76	8.48 7.23	8.80
67	67.4	58.6	0.36	-0.6	-0.7	0.00	19.9	19.3	0.16	10.64	10,59	7.27	7.50 7.54
58 59	61.6 67.9	62.9 69.3	0.38 0.42	-0,3 -0.1	-0.6 -0.2	0.00 0.00	16.1 12.2	16.6 11.7	0.13 0.10	11.62 11.71	11.67 11.66	6.63 6.69	6.77 6.83
000	63.1	54.2	0.33	0.3	0.1	0.00	15.0	14.5	0.12	10.44	10.39	7.34	7.62
001	51.6 51.1	52.7 52.1	0.32 0.31	0.0 0.1	-0.1 0.0	0.00	16.7 15.4	16.1 14.8	0.14 0.12	10.62 10.92	10.47 10.87	7.22 6.99	7.49 7.28
i03	66.7	57.9	0.35	0.1	-0.1	0.00	13.3	12.8	0.11	11.24	11.19	6.77	7.02
104	68.1 61.0	69.5 62.3	0.42 0.38	0.6 0.9	0.4 0.7	0.00	18.1 29.4	17.5 28.8	0.16 0.24	10.72 8.97	10.67 8.92	7.49 8.62	7.77 8.95
800	61.9	63.2	0.38	-0.6	-0.7	0.00	25.3	24.7	0.21	9.57	9.62	8.27	8.68
108	64.3 65.8	65,6 87,1	0.40	-0.7 -0.6	-0.8 -0.6	0.00	23.0 18.0	22.4 17.5	0.19 0.16	10.03 10.87	9.98 10.92	7.77 7.21	8.06 7.48
109	65.6	66.9	0.40	-0.4	-0.6	0.00	16.8	16.3	0.14	10.86	10.81	7.16	7.43
)10)11	65.5 49.9	66.8 51.0	0.40 0.31	-0.4 0.1	-0.6 0.0	0.00	15.1 16.9	14.6 16.3	0.12 0.14	11.48 10.76	11.43 10.71	6.69 7.19	6.94 7.46
12	49.5	50.5	0.30	0.2	0.0	0.00	15.7	15.2	0.13	10.56	10.51	7.28	7.65
113	49.9 61.9	50.9 53.0	0.31 0.32	0.0 -0.3	-0.2 -0.4	0.00	15.5 14.9	14.9 14.4	0.13 0.12	10.65 10.85	10.60	7.19	7.46
115	51.3	52.3	0.32	0.0	-0.2	0.00	13.9	13.4	0.11	11.20	10.80 11.16	7.01 6.83	7.27 7.09
118	62.6 61.3	63.7 62.4	0.32 0.32	-0.1 -0.2	-0.3 -0.3	0.00	13.6 11.9	13.1 11.4	0.11 0.10	10.95 11.03	10.90 10.98	6.95 6.87	7.21 7.13
18	52.A	53.5	0.32	-0.3	-0.4	0.00	11.6	11.0	0.09	11.41	10.98 11.36	6.87 6.67	7.13 6.82
19	67.3 84.1	58.5 65.4	0,35 0.39	0.1 1.1	0.0 0.9	0.00 0.00	12.1 22.8	11.6 22.3	0.10 0.19	11.72 9.82	11.67 9.77	6.49 8.60	6.74 8.93
21	58.6	59.8	0,36	0.4	0.3	0.00	26.3	25.7	0.22	9.19	9.14	8.55	8.88
22	68.8 63.6	60.0 64.8	0.36 0.39	-0.6 -0.8	-0.8 -0.9	0.00	18.2 14.2	17.6 13.7	0.15 0.11	10.20 10.26	10.15 10.21	7.90 7.66	8.20
24	65.4	66.8	0.40	-0.6	-0.8	0.00	11.9	11.4	0.10	11.22	11.17	7.05	7.85 7.32
25 26	67.3 72.7	68.7 74.2	0.41 0.45	-0.7 -0.6	-0.8 -0.8	0.00	11.1 10.1	10.6 9.6	0.09	10.92 11.60	10.87 11.55	7.18 6.62	7.45 6.87
27	67.9	69.4	0.42	-0.4	-0.6	0.00	9.5	9.0	0.08	11.02	10.97	7.16	7.42
28 29	51.1 52.8	62.1 63.9	0.31 0.32	-0.6 -0.6	-0.6 -0.7	00,0	12.0 10.9	11.6 10.4	0.10 0.09	9.87 10.83	9.82 10.78	7.76 7.13	8.04 7.40
30	55.7	68.8	0.34	-0.6	-0.7	0.00	10.5	10.0	0.08	10.37	10.32	7.42	7.70
31 32	58.2 57.6	69.4 68.7	0.36 0.35	-0.7 -0.6	-0.8 -0.7	0.00	9.6	9.9 9.1	0.08 0.08	10.79 10.85	10.74 10.80	7.07 7.13	7.34 7.40
33	56.5	67.7	0.35	-0.6	-0.7	0.00	9.1	8.7	0.07	10.77	10.72	7.10	7.37
34 35	57.6 64.6	68.8 65.9	0.35 0.40	-0.7 -0.4	-0.8 -0.6	0.00	9.1 8.1	8.6 7.7	0.07 0.06	11.34 11.73	11.29 11.68	6.69 6.54	6.94 6.78
36	65.3	56.5	0.34	0.6	0.4	0.00	12.8	12.3	0.10	9.46	9.40	9.58	8.91
37 38	67.0 66.7	58.2 68.1	0.35 0.41	-0.9 -1.1	-1.0 -1.2	0.00	15.3 12.5	14.8 12.0	0.12 0.10	10.12 10.83	10.07 10.78	7.93 7.45	8.23 7.73
39	69.3	70.7	0.43	-1.0	-1.1	0.00	11.6	11.1	0.09	11.39	11,34	6.87	7.13
40 41	67.6 66.6	69.0 67.9	0.42 0.41	-0.9 -0.9	-1.1 -1.0	0.00	11.6 12.2	11.1 11.7	0.09 0.10	12.23 10.94	12.18 10.89	6.31 7.17	6.55 7.44
42	56.5	67.7	0.35	-1.1	-1.2	0.00	16,1	15.6	0.13	9.98	9.93	7.69	7.98
43 44	55.2 57.7	68.3 58.9	0.34 0.36	-1.2 -1.0	-1.3 -1.1	0.00	15.3 14.6	14.8 14.1	0.12 0.12	10.68 10.30	10.63 10.25	7.17 7.49	7.44 7.77
45	58.4	69.6	0.36	-1.1	-1.2	0.00	15.5	15.0	0.13	10.37	10.32	7.31	7.59
46 47	64.9 66.4	56.0 57.6	0.34 0.35	-1.0 -0.9	-1.1 -1.1	0.00 0.00	14.3 14.1	13.8 13.6	0.12 0.11	10.88	10.83	7.09	7.36
48	68.8	60.0	0.36	-1.1	-1.2	0.00	13.3	12.8	0.11	10.29 10.94	10.24 10.89	7.41 6.90	7.69 7.16
49 50	62.2 62.2	63.5 63.4	0.38 0.38	-1.0 -1.0	-1.1 -1.2	0.00 0.00	11.6 12.3	11.1	0.09	10.66	10.60	7.19	7.46
51	62.4	63.7	0.38	-0.6	-0.8	0.00	11.5	11.8 11.0	0.10 0.09	10.82 12.08	10.77 12.01	6.96 6.22	7.22 6.45
52 53	87.7 84.7	89.5 86.5	0.54 0.52	-0.4	-0.5	0.00	36.5	35.8	0.30	9.78	9.73	8.79	9.13
54	63.7	64.8	0.33	2.0 -0.5	1.8 -0.6	0.01	36.7 28.0	36.1 27.4	0.30 0.23	9.67 8.84	9.62 8.79	8.66 8.82	8.89 9.16
55	66.9	58.1	0.35	-1.6	-1.7	-0.01	21.9	21.3	0.18	10.30	10.25	7.67	7.96
56 57	64.0 70.6	65.3 72.1	0.39 0.43	-1,6 -1.6	-1.6 -1.6	-0.01 -0.01	18.0 16.5	17.4 15.9	0.16 0.13	10.38 11.12	10.33 11.07	7.65 6.97	7.94 7.23
58	68.9	70.3	0.42	-1.3	-1.4	-0.01	12.8	12.3	0.10	11.67	11.62	6.69	6.84
59 00	69.2 64.7	70.6 66.0	0.43	-1.2 -1.2	-1.4 -1.3	-0.01 0.00	12.0 12.7	11.6 12.2	0.10 0.10	11.27 11.62	11.22 11.57	6.86 6.61	7.11 6.86
01	51.3	62.4	0.32	-0.8	-0.9	0.00	15.7	16.2	0.13	10.34	10.29	7.52	7.80
02 03	51.6 49.9	62.7 61.0	0.32 0.31	-1.2 -1.1	-1.3 -1.2	0.00	17.2 16.2	18.6 15.7	0.14 0.13	10.39 10.80	10.34 10.75	7.38 7.18	7.66 7.45
04	61.0	52.1	0.31	-1.2	-1.3	0.00	16.1	15.6	0.13	10.38	10.33	7,40	7.68
05	63.9	66.0	0.33	-1.3	-1.4	-0.01	15.7	15.1	0.13	10.96	10.91	6.96	7.22

Table 8 Continuous Emissions M Run (23-3

7 Time													
(1-min)	NOx (ppm)	NC (ppm Cor.)	x (lb/hr)	CO (ppm)	(ppm Cor.)	(lb/hr)	SO2 (ppm)	SO2 (ppm Cor.)	! (lb/hr)	O2 (%)	O2 (% Cor.)	CO2 (%)	CO2 (% Cor.)
1159 1200	71.3 62.7	73.1 64.3	0.43 0.38	0.9	0.9	0.00	6.8	6.9	0.05	11.74	11.72	6.51	6.77
1201	73.2 64.1	76.1 66.8	0.46 0.39	1.1 1.4	1.1 1.4	0.00 0.00 0.01	9.5 17.4	8.6 16.6	0.07 0.14	10.83 9.93	9.90	7.36 8.38	7.66 8.71
1203 1204	63.6 49.7	64,9 51.0	0.33 0.30	0.9	0.9	0.00	21.0	20.1 20.2	0.17 0.17	9.36 9.36	9.33	9.07 8.70	9.43 9.05
1205 1206	43.3 46.5	44.A 47.6	0.26 0.28	0.4 0.2	0.4	0.00	21.5 18.0	20.6	0.17 0.14	8,44 9,74	8.41 9.71	9.12 8.27	9.48 8.60
1207 1208	47.1 61.7	48.3	0.29	0.1	0.1	0.00	14.7	13.8 10.8	0.11	9.65 10.76	9.62 10.73	8.14 7.50	8.47 7.80
1209	63.8	53.0 55.2	0.32	0.2 0.1	0.2 0.1	0.00	10.4 9.1	9.6 8.2	0.08 0.07	10.39 11.56	10.37 11.64	7.61 6.83	7.91 7.10
1210 1211	60.0 63.5	61.5 65.2	0.37 0.39	0.2 0.2	0.2 0.2	0.00	8.2 7.4	7.3 6.5	0.06 0.06	11.05 11.82	11.03 11.80	7.15 6.52	7.43 6.78
1212 1213	66.0 67.6	67.7 69.3	0.40 0.41	0.2	0.2 0.2	0.00 0.00	6.8 7.0	6.9 6.1	0.06	11.43 11.89	11.41	6.86 6.53	7.14 6.78
1214 1215	58.4 62.0	69.9 63.6	0.36 0.38	0.4	0.4 0.3	0.00	6.7 6.6	5.9 6.6	0.05 0.06	11.25 11.73	11.23 11.71	7.09 6.62	7,37 6,88
1216 1217	63.5 52.8	54.9 54.2	0.33 0.32	1.1 0.6	1,0 0.6	0.00	8.0 14.1	7.1 13.2	0.06 0.11	10.88 8.92	10.86 8.89	7.68 8.66	7.88 9.01
1218 1219	52.5 52.6	63.8 54.0	0.32 0.32	0.0 -0.1	0.0 -0.1	0.00	13.6 14.0	12.7 13.0	0.11 0.11	9.51 9.40	9.48 9.37	8.32 8.21	8.65 8.54
1220 1221	47.8 48.6	49.0 49.9	0.29 0.30	-0.1 -0.1	-0.1 -0.1	0.00	11.5 10.6	10.6 9.7	0.09	10.58 10.05	10.58 10.03	7.48 7.76	7.78 8.07
1222 1223	47.4 60.0	48.6 61.2	0.29 0.30	-0.1 0.0	-0.1 0.0	0.00	9.9	9.0 8.4	0.07 0.07	11.05 10.54	11.03	7.08	7.36
1224 1225	49.3 61.9	60.6 53.2	0.30 0.32	0.1	0.1	0.00	8.6	7.6	0.06	11.51	10.62 11.49	7.39 6.72	7.68 6.99
1226	50.9	52.2	0.31	0.0	0.0 0.0	0.00	8.1 7.8	7.3 6.9	0.06 0.08	10.71 11.82	10.69 11,60	7.24 6.58	7.63 6.86
1227 1228	54.0 54.7	56.4 58.1	0.33	0.1 0.1	0.1 0.1	0.00 0.00	7.5 7.2	6.6 6.3	0.05 0.05	10.98 11.81	10,96 11,79	7.03 6.38	7.31 6,64
1229 1230	53.9 54.2	65,3 65,6	0.33 0.33	0.2 0.2	0.2 0.2	0.00	6.6 6.4	5.7 6.6	0.05 0.05	11.50 11.98	11.48 11.86	6.69 6.25	6.95 6.50
1231 1232	53.2 61.8	54.6 63.4	0.32 0.38	0.3 1.4	0.3 1.4	0.00 0.01	6.2 8.6	5.3 7.7	0.04	11.78 11.03	11.76 11.01	6.53 7.05	6.79 7.33
1233 1234	48.3 49.3	49.5 50.5	0.29	0.1 0.0	0.1 0.0	0.00	17.1 21.0	16.2 20.1	0.13 0.17	9,60 9,37	9.57 9.34	8.26	8.69
1235 1236	60.9 66.6	62.2 68.1	0.31 0.35	0.0 -0.1	0.0	0.00	19.6	18.6	0.15	10.74	10.72	8.26 7.34	8.69 7.63
1237 1238	59.4 60.5	69.9 62.0	0.36 0.37	-0.1 -0.1	-0.1	0.00	18.4	18.1 17.5	0.15 0.14	10.15 11.19	10.13 11.17	7.70 6.96	8.01 7.22
1239	60.8	62.3	0.37	-0.1	-0.1 -0.1	0.00	17.2 17.3	18.3 18.4	0.14 0.14	10.70 11.38	10.68 11.34	7.29 6.73	7.58 7.00
1240 1241	66.9 60.2	58.4 61.7	0.35 0.37	0.1 0.0	0.1 0.0	0.00 0.00	15.3 15.9	14.4 15.0	0.12 0.12	11.39 11.31	11.37 11.29	6.83 6.73	7.10 6.99
1242 1243	67,8 62,0	69.2 63.5	0.35 0.38	0.0 -0.2	0.0 -0.2	0.00	14.3	13.4 13.8	0.11 0.11	11.85 11.18	11.83 11.16	6.48 6.84	6.74 7.11
1244 1245	62.4 64.5	64.0 66.1	0.38 0.39	-0.2 0.0	-0.2 0.0	0.00	13.9 13.2	12.9 12.2	0.11 0.10	12.02 11.34	12.00 11.32	6.29 6.72	6.54 6.99
1248 1247	65.2 64.1	68.9 65.7	0.40 0.39	-0.1 -0.1	-0.1 -0.1	0.00	13.0 12.2	12,1 11,3	0.10 0.09	12.19 11.67	12.17	6.11 6.52	6.35 6.78
1248 1249	61.3 61.0	62.9 62.6	0.37	1.2	1.2	0.00	15.2 25.3	14.3 24.4	0.12	11.46	11.44	7.03	7.31
1250	58.4	57.9	0.34	0.3	0.3	0.00	27.6	26.6	0.20	8.98 9.35	8.85 9.32	9.02 8.46	9,38 8,80
1251 1252	48.7 64.9	50.0 58.3	0.30 0.33	0.2 -0.4	0.2 -0.4	0.00 0.00	21.7 17.7	20.8 16.8	0.17 0.14	9.39 10.68	9.36 10.64	8,41 7,40	8.75 7.70
1253 1254	67.4 62.7	58.9 64.2	0.35 0.38	-0.4 -0.3	-0.4 -0.3	0.00	14.0 13.4	13.1 12.5	0.11 0.10	10.47 11.28	10.45 11.28	7.62 6.90	7.92 7.17
1256 1256	63.0 65.5	64.6 67.2	0.38 0.40	-0.2 -0.3	-0.2 -0.3	0.00	12.3 12.0	11.3 11.1	0.09	11.40 11.53	11.38 11.51	6.90 6.66	7.17 6.93
1267 1268	62.7 68.1	64.3 69.8	0.38 0.42	-0.3 -0.3	-0.3 -0.3	0.00	10.5 10.1	9.6 9.2	0.08	12.03 11.60	12.01 11.58	6.42 6.61	6.68 6.88
1269 1300	68.5 65.2	70.2 58.6	0.42 0.34	-0.4 -0.2	-0.4 -0.2	0.00	9.5 10.3	8.7 9.4	0.07 0.08	12.16 11.21	12.13 11.19	6.18 6.98	6.42 7.25
1301 1302	43.9 45.7	45.1 46.9	0.27 0.28	-0.2 -0.3	-0.2 -0.3	0.00	13.6 13.8	12.7	0.11	10.10	10.08	7.56	7.86
1303 1304	62.4 66.6	53.7 58.1	0.32	-0.4 -0.1	-0.4	0.00	13.8	12.9	0.11 0.11	10.62 10.42	10.60 10.40	7.29 7.41	7.58 7.71
1306	45,4	46.6	0.28	-0.7	-0.1 -0.7	0.00	19.9	15.5 18.9	0.13 0.18	10.52 9.08	10.50 9.05	7.64 8.66	7.94 8.90
1308 1307	63.1 64.0	54.4 55.4	0.32 0.33	-0.7 -0.6	-0.7 -0.6	0.00 0.00	16.6 13.8	16.7 12.9	0.13 0.11	10.93 10.98	10.91 10.94	7.19 7.25	7.48 7.54
1308 1309	56.8 56.5	58.3 57.9	0.35 0.34	-0.6 -0.6	-0.6 -0.5	0.00	12.7 11.7	11.8 10.8	0.10 0.09	11.40 11.68	11.38 11.68	6.78 6.77	7.05 7.04
1310 1311	61.0 65.2	62.6 66.8	0.37 0.40	-0.6 -0.6	-0.6 -0.5	0.00	11,8 11.1	10.9 10.2	0.09 0.08	11.35 12.05	11.33 12.03	6.80 6.41	7.07 6.67
1312 1313	69.7 52.5	71.4 63.8	0.42 0.32	-0.5 -0.6	-0.6 -0.6	0.00	10.5 15.4	9.6 14.5	0.08 0.12	11.19 9,88	11.17 9.86	6.98 7.81	7.25 8.12
1314 1316	50.6 50.4	61.8 61.7	0.31 0.31	-0.6 -0.8	-0.6 -0.8	0.00	17.3 17.9	18.4 17.0	0.14 0.14	9.24 10.12	9.21 10.10	8.28 7.56	8.61 7.86
1316 1317	61.9 67.0	63.5 68.7	0.38 0.41	-0.7 -0.7	-0.7 -0.7	0.00	12.6 11.2	11.7 10.3	0.10 0.09	11.28 11.64	11.26 11.62	6.94 6.57	7.22 6.83
1318 1319	62.9 66.6	84.5 68.2	0.38 0.41	-0.7 -0.6	-0.7 -0.6	0.00	9,6 9,3	8.7 8.4	0.07	11.57	11,66	6.73	7.00
1320 1321	63.8 82.3	65.4 84.4	0.39	-0.2 -0.7	-0.2 -0.7	0.00	15.0	14.1	0.12	11.93 10.24	11.91 10.22	6.38 8.16	8.63 8.49
1322 1323	89.6 82.0	91.9 84.1	0.56 0.50	-0.7 -0.7 -0.6	-0.7	0.00	32.7 45.1	31.7 44.0	0.28	8.72 9.18	9.15 0.10	9.04 8.69	9.40 9.04
1324	63.5	65.1	0.39	-0.6	-0.6 -0.6	0.00	48.8 43.5	47.8 42.5	0.40 0.35	9.42 8.76	9.39 8.73	8.44 8.86	8.78 9.21
1325 1326	62.5 46.4	53.9 47.6	0.32 0.28	-0.8 -1.0	-0.8 -1.0	0.00	42.5 34.0	41.4 33.0	0.34 0.27	9.24 9.05	9.21 9.02	8.37 8.53	8.70 8.87
1327 1328	47.9 48.3	49.1 49.6	0.29 0.29	-1.2 -1.2	-1.2 -1.2	0.00 0.00	30.2 28.6	29.2 26.7	0.24 0.21	10.18 9.62	10.16 9.49	7.74 8.16	8.05 8.48
1329 1330	60.2 60.6	61.6 61.8	0.31 0.31	-1.2 -1.2	-1.2 -1.2	0.00 0.00	24.9 22.9	23.9 22.0	0.20 0.18	10.71 9.95	10.69 9.92	7.31 7.84	7.60 8.16
1331 1332	52.0 51.1	53.3 52.4	0.32 0.31	-1.2 -1.2	-1.2 -1.2	0.00 0.00	20.8 18.4	19,8 17,5	0.16 0.14	10.97 10.39	10.95 10.37	7.09 7.66	7.37 7.86
1333 1334	53.6 53.2	55.0 54.6	0.33 0.32	-1.2 -1.2	-1.2 -1.2	0.00	18.0 15.6	15.1 14.6	0.12 0.12	11.07 10.77	11.05 10.75	6.98 7.29	7.25 7.68
1336 1336	65.1 69.6	58.6 71.3	0.34 0.42	-1.1 -0.7	-1.1 -0.7	0.00	15.9 27.4	15.0 26.4	0.12 0.22	11.48 9.26	11.46	6.76	7.02
1337	81.9 59.2	84.0 60.7	0.60 0.36	-0.9 -1.0	-0.9 -1.0	0.00	40.6 36.6	39.6	0.33	8.89	9.23 8.86	8.77 8.92	9.12 9.28
1339	49.1	50.4	0.30	-1.4	-1.4	0.00	33.4	35.5 32.4	0.29	9.41 8.68	9.38 8.66	8.65 8.92	9.00 9.28
1340 1341	44.2 45.8	45.3 46.9	0.27 0.28	-1.4 -1.5	-1.4 -1.6	-0.01 -0.01	29.8 28.8	28.8 27.8	0.24 0.23	9.45 9.52	9.42 9.49	8.62 8.28	8.86 8.61
1342 1343	44.2 46.2	45.3 47.4	0.27 0.28	-1.6 -1.6	-1.5 -1.5	-0.01 -0.01	23.3 22.1	22.4 21.1	0.19 0.17	9.97 9.97	9.94 9.94	8.07 7.91	8.39 8.23
1344 1345	44.2 45.9	45.3 47.1	0.27 0.28	-1.6 -1.6	-1.5 -1.5	-0.01 -0.01	19.1 18.5	18.1 17.6	0.15 0.15	10.29 10.47	10.27 10.45	7.80 7.61	8.11 7.81
1346 1347	45.1 49.4	46.3 60.6	0.28 0.30	-1.5 -1.6	-1.5 -1.5	-0.01 -0.01	16.2 16.1	16,3 16,2	0.13 0.13	10.68	10.54	7.66 7.22	7.86 7.61
1348 1349	49.4 62.2	50.7 53.5	0.30 0.32	-1.6 -1.5	-1.4	-0.01 -0.01	14.1	13.2 12.4	0.11 0.10	10.74	10.72	7.39	7.68
1350 1351	62.7 67.9	54.1 59.3	0.32 0.35	-1.4 -1.3	-1,4	-0.01	12.2	11.3	0.09	11.29	11.27	6.88 7.21	7.16 7.60
1352	72.6	74.4	0.44	-1.6	-1.3 -1.5	0.00 -0.01	13.7 27.2	12.8 26.2	0.11	11.50 9.43	11.48 9.40	6.87 8.43	7.14 8.77
1353 1354	95.1 94.7	97.5 97.1	0.68 0.68	-1.9 -1.8	-1.8 -1.8	-0.01 -0.01	51.8 60.1	60.7 69.0	0.42 0.49	9.60 9.81	9.67 9.78	8,39 8.20	8.73 8.63
1366 1366	93.2 91.8	96.6 94.1	0.57 0.56	-1.9 -1.8	-1.9 -1.8	-0.01 -0.01	69.6 68.1	68.4 67.0	0.48 0.47	9.61 9.63	9.68 9.60	8.29 8.32	8.62 8.65
1367 1368	90.7 87.2	93.0 89.4	0.66 0.63	-1.8 -1.7	-1.8 -1.7	-0.01 -0.01	54.8 51.9	53.7 50.8	0.44	9.61 9.68	9.68	8.24	8.67
1359	82.1 79.2	84.2 81.2	0.60	-1.6	-1.6	-0.01	47.6	46.6	0.39	9.78	9.65 9.76	8.17 8.08	8.60 8.40
	75.7	77.6	0.48	-1.6 -1.0	-1.6 -1.0	-0.01 0.00	63.9 46.1	52.8 45.0	0.44	9.38 9.35	9.35 9.32	8.32 8.31	8.65 8.64
1400 1401		76.4	0.45	-0.3	-0.3	0.00	42.6	41.6	0.34	9.97	9.94	7.96	8.27
1400 1401 1402 1403	73.6 73.7	75.6	0.45	0.3	0.2	0.00	44.0	42.9	0.36	9.67	9.54	8.14	8.47
1400 1401 1402 1403 1404 1406	73.7 72.6 71.2	75.6 74.3 73.0	0.45 0.44 0.43	1.3 2.5	1.3 2.4	0.00 0.01	49.7 40.7	48.7 39.6	0.38 0.40 0.33	9.67 9.62 9.60	9.54 9.49 9.47		
1400 1401 1402 1403 1404	73.7 72.6	76.6 74.3	0.45 0.44	1.3	1.3	0.00	49.7	48.7	0.38 0.40	9.67 9.62	9.49	8.14 8.18	8.47 8.51

Table 9 Continuous Emissions Measurements Results Run 15-3 10/01/13

10/01/13													
Time (1-min)	NOx (ppm)	NC (ppm Cor.)	Ox (lb/hr)	CO (ppm)	(ppm Cor.)	O (lb/hr)	SO2 (ppm)	SC (ppm Cor.))2 (lb/hr)	O2 (%)	O2 (% Cor.)	CO2 (%)	CO2 (% Cor.)
		1			-		(PP)	(ррш оои)	(15/11)	(70)	(% 001.)	(70)	(% 001.)
1506 1507	66.2	68.4	0.41	1.5	2.2	0.01	4.5	3.7	0.03	12.98	12.96	5.58	5.75
1507	74.1 52.1	76.6 53.8	0.46	2.1	2.8	0.01	5.3	4.5	0.04	12.78	12.76	5.80	5.99
1509	52.7	54.5	0.32 0.33	1.4 1.3	2.1	0.01	14.2	13.4	0.11	10.06	10.03	7.99	8.27
1510	52.8	54.6	0.33	1.3	2.0 1.7	0.01 0.01	21.4	20.4	0.17	8.86	8.82	8.83	9.15
1511	54.8	56.6	0.34	1.0	1.7	0.01	19.2 16.7	18.3 15.8	0.15	9.82	9.78	8.05	8.33
1512	52.4	54.2	0.33	0.9	1.6	0.01	15.7	14.8	0.13 0.12	9.65 10.61	9.61	8.21	8.50
1513	48.9	50.6	0.30	1.0	1.7	0.01	15.1	14.0	0.12	10.81	10.58 10.29	7.42 7.69	7.68
1514	53.1	54.9	0.33	0.9	1.6	0.01	13.8	12.9	0.12	11.16	11.13	6.96	7.96 7.20
1515	54.6	56.4	0.34	1.0	1.7	0.01	12.5	11.7	0.10	11.03	11.00	7.13	7.20
1516	60.7	62.7	0.38	0.9	1.6	0.01	11.7	10.9	0.09	11.51	11.48	6.64	6.86
1517	61.6	63.6	0.38	1.0	1.6	0.01	10.4	9.6	0.08	11.59	11.56	6.70	6.93
1518	69.9	72.2	0.43	0.9	1.6	0.01	10.4	9.6	0.08	11.41	11.38	6.68	6.90
1519	70.6	73.0	0.44	1.0	1.6	0.01	9.6	8.8	0.07	12.08	12.05	6.34	6.55
1520	72.3	74.7	0.45	1.0	1.7	0.01	10.0	9.2	0.08	11.47	11.44	6.62	6.84
1521	72.9	75.4	0.45	1.0	1.7	0.01	9.7	8.9	0.07	12.28	12.25	6.15	6.36
1522	70.1	72.5	0.44	0.9	1.6	0.01	9.0	8.2	0.07	11.58	11.55	6.56	6.78
1523	68.9	71.2	0.43	1.4	2.1	0.01	9.1	8.3	0.07	12.04	12.01	6.53	6.74
1524	75.9	78.5	0.47	1.2	1.8	0.01	18.3	17.4	0.15	9.06	9.02	8.78	9.10
1525 1526	56.8	58.7	0.35	0.7	1.4	0.00	18.8	17.9	0.15	9.63	9.59	8.04	8.32
1527	56.3	58.2	0.35	0.6	1.3	0.00	14.5	13.6	0.11	10.18	10.15	7.74	8.01
1527	53.4 55.5	55.2 57.4	0.33 0.34	0.6 0.6	1.3	0.00	12.5	11.7	0.10	10.80	10.77	7.13	7.37
1529	61.3	63.4	0.34	0.6 0.6	1.3 1.3	0.00 0.00	10.0	9.2 8.6	0.08	11.22	11.19	6.94	7.17
1530	60.5	62.5	0.38	0.6	1.3	0.00	9.4 8.7	8.6	0.07	11.23	11.20	6.78	7.01
1531	60.5	62.6	0.38	0.7	1.4	0.00	8.5	7.8	0.07 0.06	11.72 11.10	11.69	6.58	6.80
1532	65.6	67.8	0.41	0.6	1.3	0.00	7.8	7.0	0.06	11.10	11.07 11.94	6.87 6.37	7.10
1533	67.7	70.0	0.42	0.6	1.3	0.00	7.8	7.0	0.06	11.97	11.94	6.61	6.58 6.83
1534	68.5	70.8	0.43	0.6	1.2	0.00	7.6	6.8	0.06	12.19	12.16	6.19	6.39
1535	65.8	68.1	0.41	0.6	1.3	0.00	7.3	6.6	0.05	11.64	11.61	6.51	6.72
1536	72.0	74.4	0.45	0.6	1.2	0.00	7.3	6.5	0.05	11.85	11.82	6.29	6.50
1537	73.0	75.5	0.45	0.6	1.3	0.00	6.7	6.0	0.05	12.42	12.39	6.01	6.20
1538	68.3	70.6	0.42	0.6	1.3	0.00	6.6	5.8	0.05	11.94	11.91	6.26	6.46
1539	69.6	72.0	0.43	1.2	1.9	0.01	6.5	5.7	0.05	12.89	12.87	5.68	5.87
1540	57.8	59.7	0.36	1.1	1.8	0.01	8.0	7.2	0.06	10.41	10.38	7.66	7.93
1541	54.2	56.1	0.34	0.2	0.9	0.00	11.4	10.6	0.09	10.30	10.27	7.60	7.86
1542	54.6	56.4	0.34	0.3	1.0	0.00	10.6	9.8	0.08	10.17	10.14	7.68	7.95
1543	57.3	59.2	0.36	0.4	1.1	0.00	8.9	8.1	0.07	11.55	11.52	6.62	6.84
1544	57.3	59.2	0.36	0.5	1.2	0.00	7.1	6.3	0.05	11.40	11.37	6.75	6.98
1545	62.4	64.5	0.39	0.6	1.2	0.00	7.3	6.5	0.05	12.07	12.04	6.19	6.40
1546	64.3	66.5	0.40	0.5	1.2	0.00	6.9	6.1	0.05	11.69	11.66	6.53	6.74
1547 1548	67.4 71.2	69.7 73.6	0.42	0.5	1.2	0.00	7.3	6.5	0.05	11.98	11.95	6.20	6.41
1549	67.7	70.0	0.44	0.6 0.6	1.3	0.00	6.3	5.6	0.05	12.37	12.34	6.05	6.25
1550	66.5	68.8	0.42 0.41	0.6	1.3 1.3	0.00 0.00	6.1 6.3	5.3 5.6	0.04	12.10	12.07	6.15	6.35
1551	59.3	61.3	0.37	0.8	1.4	0.01	7.2	6.4	0.05 0.05	12.63 11.55	12.61 11.52	5.76 6.65	5.94
1552	45.6	47.1	0.28	0.8	1.4	0.01	9.1	8.3	0.07	10.33	10.30	7.30	6.87 7.55
1553	44.6	46.1	0.28	0.8	1.5	0.01	9.2	8.4	0.07	11.09	11.06	6.88	7.11
1554	44.7	46.2	0.28	0.7	1.4	0.01	9.1	8.3	0.07	10.33	10.30	7.32	7.57
1555	55.5	57.4	0.34	0.9	1.6	0.01	7.6	6.8	0.06	12.54	12.52	5.91	6.10
1556	67.4	69.7	0.42	0.9	1.5	0.01	12.2	11.4	0.10	9.45	9.41	8.42	8.72
1557	71.6	74.0	0.44	0.3	1.0	0.00	18.8	17.9	0.15	9.70	9.66	8.18	8.47
1558	46.2	47.8	0.29	0.3	1.0	0.00	15.1	14.2	0.12	9.58	9.54	8.25	8.54
1559	44.9	46.4	0.28	0.3	1.0	0.00	13.0	12.1	0.10	10.79	10.76	7.29	7.54
1600	46.3	47.9	0.29	0.4	1.1	0.00	10.9	10.0	0.08	10.72	10.69	7.38	7.64
1601	52.6	54.3	0.33	0.4	1.1	0.00	10.2	9.4	0.08	11.52	11.49	6.68	6.90
1602	57.5	59.5	0.36	0.5	1.2	0.00	8.6	7.8	0.07	11.54	11.51	6.75	6.98
1603	61.3	63.3	0.38	0.4	1.1	0.00	8.3	7.5	0.06	11.84	11.81	6.40	6.61
1604	62.8	64.9	0.39	0.5	1.2	0.00	7.5	6.7	0.06	11.84	11.81	6.51	6.73
1605 1606	64.4 64.5	66.6	0.40	0.5	1.2	0.00	7.5	6.7	0.06	12.04	12.01	6.24	6.44
1605	65.7	66.7 67.9	0.40	0.5	1.2	0.00	6.8	6.1	0.05	12.14	12.11	6.28	6.48
1608	67.5	69.8	0.41 0.42	0.5 0.5	1.2 1.2	0.00	6.7	5.9	0.05	12.09	12.06	6.17	6.37
1609	65.7	68.0	0.42	0.5	1.2 1 2	0.00	6.3 6.5	5.5 5.7	0.05	12.40	12.37	6.08	6.27
1610	63.1	65.2	0.41	0.5	1.2 1.1	0.00 0.00	6.5 6.2	5.7 5.4	0.05	12.01	11.98	6.21	6.42
1611	62.2	64.3	0.39	0.5	1.4	0.00	6.2	5.4 5.4	0.05 0.04	12.85	12.83	5.71	5.89
1612	63.3	65.5	0.39	1.0	1.6	0.01	13.7	12.9	0.04	12.26 10.15	12.23 10.12	6.15	6.35
1613	51.6	53.4	0.32	0.6	1.2	0.00	19.9	19.0	0.11	9.06		7.99	8.27
1614	48.6	50.3	0.30	0.1	0.8	0.00	19.4	18.5	0.15	10.27	9.02 10.24	8.73 7.82	9.04
1615	50.6	52.3	0.31	0.0	0.7	0.00	18.7	17.8	0.15	9.81	9.77	.8.01	8.09 8.29
1616	48.6	50.2	0.30	0.0	0.7	0.00	17.2	16.3	0.14	10.87	10.84	7.34	7.59
1617	48.6	50.3	0.30	0.1	0.7	0.00	18.0	17.1	0.14	10.34	10.84	7.56	7.82
1618	50.7	52.4	0.31	0.1	0.8	0.00	15.9	15.0	0.14	11.17	11.14	7.08	7.82 7.32
1619	52.8	54.6	0.33	0.1	0.8	0.00	16.4	15.5	0.13	10.86	10.83	7.06 7.14	7.32 7.38
1620	54.4	56.3	0.34	0.1	0.8	0.00	15.6	14.8	0.12	11.27	11.24	6.98	7.22
1621	56.4	58.3	0.35	0.1	0.7	0.00	15.8	14.9	0.12	11.24	11.21	6.84	7.07
1622	57.6	59.6	0.36	0.2	0.9	0.00	15.3	14.4	0.12	11.45	11.42	6.82	7.05
1623	58.1	60.0	0.36	0.1	0.8	0.00	16.3	15.4	0.13	11.56	11.53	6.59	6.81
1624	59.0	61.0	0.37	0.1	8.0	0.00	13.9	13.0	0.11	11.52	11.49	6.74	6.97
1625	58.5	60.5	0.36	0.1	0.8	0.00	14.9	14.0	0.12	11.76	11.73	6.44	6.65
Ave	59.9	61.9	0.37	0.6	1.3	0.00	11.1	10.3	0.09	11.24	11.21	6.91	7.14

10/01/13							•		
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	809	0.00	0.04	90.9	92.6	0.1	92.5	83.2
2013	274	810	4.23	4.73	75.1	85.2	4.7	80.3	84.8
2013	274	811	20.15	19.60	1.5	0.1	-2.0	3.7	10.6
2013	274	812	20.17	19.63	0.0	0.0	-0.1	0.0	-0.7
2013	274	813	20.11	19.42	3.3	-0.1	-0.1	0.0	0.1
2013	274	814	0.74	0.31	99.8	180.2	-4.2	220.2	87.5
2013	274	815	0.00	0.04	100.6	237.7	0.8	236.8	100.3
2013	274	816	0.00	0.02	100.6	237.1	1.0	235.9	100.3
2013	274	817	-0.01	0.02	100.6	237.3	1.1	236.1	100.3
2013	274	818	-0.01	0.01	100.6	237.6	1.3	236.5	100.3
2013	274	819	-0.02	0.01	100.6	223.3	1.1	228.8	100.3
2013	274	820	-0.03	0.01	93.4	92.2	-1.3	100.5	94.4
2013	274	821	-0.03	0.00	91.3	92.0	0.5	91.4	90.0
2013	274	822	-0.03	0.00	91.3	91.9	0.4	91.5	89.9
2013	274	823	-0.03	-0.01	70.2	71.9	-3.4	78.1	77.2
2013	274	824	-0.03	-0.01	45.7	45.4	0.4	44.9	45.5
2013	274	825	7.19	7.56	24.6	25.9	-3.0	30.3	31.4
2013	274	826	20.06	19.49	0.1	0.0	-0.1	-0.1	-1.2
2013	274	827	20.09	19.52	-0.1	0.0	0.0	0.0	-2.2
2013	274	828	12.07	11.37	0.0	0.0	-0.1	0.0	-2.0
2013	274	829	10.08	9.86	-0.1	-0.1	-0.1	0.0	-1.6
2013	274	830	15.26	5.00	-0.1	0.1	-0.3	0.3	-1.0 -1.1
2013	274	831	10.63	6.61	2.4	21.3	-3.8	28.7	5.9
2013	274	832	10.08	9.74	-1.3	0.5	-0.1	0.3	-0.8
2013	274	833	10.07	9.76	-1.5	0.0	-0.1	0.0	-0.8 -1.8
2013	274	834	10.07	9.77	-1.0	-0.1	-0.1	0.0	-1.0
2013	274	835	10.07	9.77	0.1	0.0	-0.1	0.0	0.1
2013	274	836	5.05	4.68	38.7	38.6	11.5	26.9	24.4
2013	274	837	0.07	0.08	87.8	90.3	-0.1	90.4	88.8
2013	274	838	0.05	0.04	88.8	90.6	0.4	90.4	90.2
2013	274	839	0.04	0.03	68.6	70.4	-2.4	73.5	76.6
2013	274	840	0.04	0.02	45.5	44.9	0.1	44.9	46.1
2013	274	841	0.51	0.34	44.2	45.0	0.2	44.8	45.3
2013	274	842	12.64	5.34	13.0	47.9	-0.3	48.1	12.9
2013	274	843	12.54	5.55	6.1	47.3	-1.8	49.1	3.5
2013	274	844	12.72	5.51	4.3	49.1	3.3	45.6	4.6
2013	274	845	12.83	5.43	3.4	45.8	-2.1	48.0	4.3
2013	274	846	12.88	5.40	3.1	44.1	-4.8	49.6	4.5
2013	274	847	12.91	5.38	3.2	46.6	-0.3	47.0	3.8
2013	274	848	12.88	5.39	3.3	49.2	3.3	45.9	2.7
2013	274	849	12.75	5.44	3.2	47.7	-0.9	48.7	2.5
2013	274	850	12.59	5.61	3.3	47.0	-1.6	48.5	3.2
2013	274	851	12.83	5.42	3.0	46.8	-1.2	48.0	3.4
2013	274	852	12.81	5.44	2.8	46.8	-2.3	49.0	3.3
2013	274	853	12.88	5.39	2.4	48.4	2.8	45.4	3.7
2013	274	854	12.84	5.42	2.3	46.7	-1.6	48.2	3.3
2013	274	855	12.87	5.39	2.4	47.8	-1.0	48.6	2.4
2013	274	856	12.51	5.61	2.3	46.8	-2.5	49.3	2.5
2013	274	857	12.82	5.45	2.1	48.8	3.4	45.2	3.7
2013	274	858	12.87	5.40	2.1	44.3	-4.9	49.6	3.7
2013	274	859	12.75	5.47	2.1	50.1	4.0	45.9	4.3
2013	274	900	12.83	5.75	2.3	51.9	-1.0	53.0	1.6
2013	274	901	10.22	7.63	4.4	39.5	0.1	39.4	0.7
2013	274	902	10.80	7.11	4.5	40.1	-2.1	42.1	0.7
2013	274	903	11.16	6.72	4.3	45.8	-0.9	46.7	0.0
2013	274	904	11.27	6.67	4.3	48.1	-0.7	48.8	0.7
2013	274	905	11.74	6.30	3.8	48.1	-2.5	50.5	1.1
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10/01/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	906	11.90	6.19	3.7	51.6	1.7	50.0	1.1
2013	274	907	12.07	6.08	4.2	52.5	1.3	51.2	0.9
2013	274	908	11.98	6.10	4.3	52.3	-0.1	52.5	1.3
2013	274	909	12.05	6.12	4.0	52.1	1:1	50.9	2.2
2013	274	910	12.21	5.98	3.5	50.0	-1.2	51.1	2.7
2013	274	911	12.27	5.94	3.7	48.7	-2.8	51.5	2.5
2013	274	912	12.28	5.92	3.8	51.7	2.1	49.6	2.0
2013	274	913	12.33	5.87	3.7	50.1	-1.7	51.8	2.0
2013	274	914	12.03	6.06	3.1	50.0	-2.3	52.1	2.0
2013	274	915	12.05	5.78	3.1	50.0 52.6			
2013	274	916	13.76				1.0	51.5	2.5
2013	274	917	9.96	5.01	2.6	58.0	-6.0	66.6	12.9
				7.72	5.1	69.3	-1.8	70.9	1.4
2013	274	918	10.44	7.29	6.3	59.0	-0.9	60.0	1.3
2013	274	919	11.18	6.73	6.1	52.6	-1.9	54.4	1.8
2013	274	920	11.65	6.38	6.5	54.3	1.1	53.4	1.7
2013	274	921	11.85	6.23	6.3	54.7	-0.1	54.8	1.7
2013	274	922	11.94	6.14	5.3	52.9	-2.0	54.7	1.9
2013	274	923	11.82	6.24	5.0	52.4	-2.2	54.5	2.0
2013	274	924	12.18	5.98	4.6	52.5	-1.1	53.4	2.2
2013	274	925	12.19	5.97	4.5	54.2	0.9	53.1	2.1
2013	274	926	12.27	5.91	4.4	54.8	2.5	52.2	2.0
2013	274	927	12.41	5.82	4.0	51.4	-2.0	53.2	2.0
2013	274	928	12.44	5.80	4.1	50.4	-3.8	54.2	2.0
2013	274	929	12.47	5.77	4.1	52.1	-2.1	54.3	2.0
2013	274	930	12.43	5.79	4.1	54.7	2.1	52.5	1.8
2013	274	931	12.79	5.53	4.0	62.8	2.2	60.6	1.8
2013	274	932	11.47	7.06	7.5	89.3	6.6	82.9	1.4
2013	274	933	8.96	8.94	22.1	116.5	3.8	112.4	-0.2
2013	274	934	8.40	9.11	26.3	102.6	-2.9	106.5	-0.2
2013	274	935	9.45	8.22	21.4	59.3	-2.3	61.5	0.1
2013	274	936	9.88	7.83	17.0	51.3	-0.2	51.5	0.2
2013	274	937	10.47	7.36	14.0	52.0	-0.2	52.1	0.2
2013	274	938	10.78	7.11	12.2	54.3	-0.8	55.0	0.2
2013	274	939	11.07	6.89	11.1	56.5	-0.9	57.5	0.2
2013	274	940	11.28	6.71	9.5	57.1	-1.9	59.1	0.2
2013	274	941	11.46	6.55	8.6	59.0	-0.2	59.1	0.3
2013	274	942	11.54	6.49	7.9	59.3	0.4	58.8	0.2
2013	274	943	11.57	6.46	7.6	60.0	1.6	58.4	0.3
2013	274	944	11.70	6.37	7.2	59.4			
2013	274	945	11.69	6.37	6.5		1.4	58.1	0.4
2013	274	946	11.73	6.34	6.4	60.3	1.2	59.1	0.3
2013						60.9	1.5	59.2	0.5
	274	947	11.95	6.20	6.4	62.5	2.5	60.1	0.3
2013	274	948	10.61	7.70	17.9	107.7	-5.4	127.8	0.7
2013	274	949	9.73	8.34	50.5	218.7	9.8	222.5	1.2
2013	274	950	9.56	8.32	52.5	173.7	15.3	162.4	2.2
2013	274	951	9.28	8.43	47.7	140.3	-0.6	142.6	1.5
2013	274	952	8.86	8.66	50.2	138.5	2.5	135.9	-0.2
2013	274	953	9.12	8.46	50.0	120.1	-3.6	125.4	0.0
2013	274	954	9.20	8.40	44.0	102.9	-3.5	106.3	-0.3
2013	274	955	8.88	8.48	39.8	76.5	-2.8	78.9	-0.3
2013	274	956	10.81	7.23	25.1	55.4	-3.5	58.9	-0.6
2013	274	957	10.64	7.27	19.9	57.4	-5.9	63.2	-0.5
2013	274	958	11.62	6.53	16.1	61.6	-4.1	65.7	-0.3
2013	274	959	11.71	6.59	12.2	67.9	4.7	63.0	-0.1
2013	274	1000	10.44	7.34	15.0	53.1	-1.4	54.4	0.3
2013	274	1001	10.52	7.22	16.7	51.6	0.5	51.0	0.0
2013	274	1002	10.92	6.99	15.4	51.1	-1.0	51.9	0.1

10/01/13									
Year	Julian	Time	02	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	1003	11.24	6.77	13.3	56.7	1.4	55.3	0.1
2013	274	1004	10.72	7.49	18.1	68.1	-0.4	68.5	0.6
2013	274	1005	8.97	8.62	29.4	61.0	-0.6	61.6	0.9
2013	274	1006	9.57	8.27	25.3	61.9	3.3	58.5	-0.5
2013	274	1007	10.03	7.77	23.0	64.3	2.2	62.0	-0.7
2013	274	1008	10.97	7.21	18.0	65.8	3.0	62.7	-0.5
2013	274	1009	10.86	7.16	16.8	65.5	-4.9	70.5	-0.4
2013	274	1010	11.48	6.69	15.1	65.5	-1.8	67.5	-0.4
2013	274	1011	10.76	7.19	16.9	49.9	-1.2	51.2	0.1
2013	274	1012	10.56	7.28	15.7	49.5	0.0	49.3	0.2
2013	274	1013	10.65	7.19	15.5	49.9	-1.7	51.5	0.0
2013	274	1014	10.85	7.01	14.9	51.9	0.1	51.8	-0.3
2013	274	1015	11.20	6.83	13.9	51.3	-1.4	52.7	0.0
2013	274	1016	10.95	6.95	13.6	52.6	-0.1	52.7	-0.1
2013	274	1017	11.03	6.87	11.9	51.3	-1.7	53.0	-0.2
2013	274	1018	11.41	6.57	11.5	52.4	-1.3	53.5	-0.3
2013	274	1019	11.72	6.49	12.1	57.3	1.8	55.4	0.1
2013	274	1020	9.82	8.60	22.8	64.1	-3.0	66.9	1.1
2013	274	1021	9.19	8.55	26.3	58.6	1.0	57.4	0.4
2013	274	1022	10.20	7.90	18.2	58.8	1.7	57.0	-0.6
2013	274	1023	10.26	7.66	14.2	63.5	-0.5	63.9	-0.8
2013	274	1024	11.22	7.05	11.9	65.4	-4.3	70.0	-0.6
2013	274	1025	10.92	7.18	11.1	67.3	-5.6	73.0	-0.7
2013	274	1026	11.60	6.62	10.1	72.7	0.4	72.3	-0.6
2013	274	1027	11.02	7.15	9.5	67.9	2.8.	65.2	-0.4
2013	274	1028	9.87	7.75	12.0	51.1	-3.2	54.1	-0.5
2013	274	1029	10.83	7.13	10.9	52.8	-5.0	57.7	-0.6
2013	274	1030	10.37	7.42	10.5	55.7	-0.3	56.0	-0.5
2013	274	1031	10.79	7.07	10.4	58.2	2.0	55.9	-0.7
2013	274	1032	10.85	7.13	9.6	57.5	1.7	55.9	-0.5
2013	274	1033	10.77	7.10	9.1	56.5	-1.6	58.2	-0.6
2013	274	1034	11.34	6.69	9.1	57.6	-2.2	59.7	-0.7
2013	274	1035	11.73	6.54	8.1	64.6	3.2	61.3	-0.4
2013	274	1036	9.45	8.58	12.8	55.3	-1.1	56.3	0.5
2013	274	1037	10.12	7.93	15.3	57.0	-0.1	57.0	-0.9
2013	274	1038	10.83	7.45	12.5	66.7	4.9	61.9	-1.1
2013	274	1039	11.39	6.87	11.6	69.3	1.3	67.8	-1.0
2013	274	1040	12.23	6.31	11.6	67.6	-6.0	73.8	-0.9
2013	274	1041	10.94	7.17			1.0	65.5	-0.9
2013	274	1042	9.98	7.69	16.1	56.5	-0.9	57.5	-1.1
2013	274	1043	10.68	7.17			-4.7	59.8	-1.2
2013	274	1044	10.30	7.49	14.6	57.7	2.1	55.5	-1.0
2013	274	1045	10.37	7.31	15.5	58.4	1.9	56.6	-1.1
2013	274	1046	10.88	7.09	14.3	54.9	-1.7	56.7	-1.0
2013	274	1047	10.29	7.41	14.1	56.4	-3.4	59.7	-0.9
2013	274	1048	10.94	6.90	13.3	58.8	-1.6	60.3	-1.1
2013	274	1049	10.65	7.19	11.6	62.2	4.3	57.9	-1.0
2013	274	1050	10.82	6.96	12.3	62.2	1.1	61.2	-1.0
2013	274	1051	12.06	6.22	11.5	62.4	-3.3	65.7	-0.6
2013	274	1052	9.78	8.79	36.5	87.7	-6.9	95.5	-0.4
2013	274	1053	9.67	8.56	36.7	84.7	-2.5	87.4	2.0
2013	274	1054	8.84	8.82	28.0	53.7	-1.3	54.9	-0.5
2013	274	1055	10.30	7.67	21.9	56.9	-2.4	59.2	-1.5
2013	274	1056	10.38	7.65	18.0	64.0	2.9	61.2	-1.5
2013	274	1057	11.12	6.97	16.5	70.6	2.4	68.2	-1.5
2013	274	1058	11.67	6.69	12.8	68.9	0.0	68.8	-1.3
2013	274	1059	11.27	6.86	12.0	69.2	-5.3	74.6	-1.2
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10/01/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	1100	11.62	6.61	12.7	64.7	-0.1	64.7	-1.2
2013	274	1101	10.34	7.52	15.7	51.3	1.8	49.5	-0.8
2013	274	1102	10.39	7.38	17.2	51.6	-0.1	51.7	-1.2
2013	274	1103	10.80	7.18	16.2	49.9	-3.1	53.1	-1.1
2013	274	1104	10.38	7.40	16.1	51.0	-2.6	53.6	-1.2
2013	274	1105	10.96	6.96	15.7	53.9	0.2	53.6	-1.3
2013	274	1106	10.85	7.10	14.6	54.7	2.0	52.8	-1.1
2013	274	1107	11.59	6.52	14.5	60.1	-1.5	61.4	-0.9
2013	274	1108	12.12	6.39	10.8	67.9	-1.8	69.8	0.4
2013	274	1109	10.93	7.16	11.2	67.2	-5.6	73.2	-1.4
2013	274	1110	11.29	6.90	11.8	64.9	-0.7	65.5	-1.5
2013	274	1111	9.14	6.75	15.1	59.9	5.1	54.8	0.2
2013	274	. 1112	9.91	9.67	3.8	4.9	-1.4	6.2	2.9
2013	274	1113	10.04	9.74	0.9	0.0	-0.1	0.0	0.1
2013	274	1114	10.04	9.74	0.8	0.0	-0.1	0.0	0.2
2013	274	1115	1.93	1.64	61.7	53.4	-3.7	66.9	50.4
2013	274	1116	0.07	0.06	86.7	89.5	0.0	89.5	90.2
2013	274	1117	0.05	0.03	87.5	89.8	0.4	89.5	90.3
2013	274	1118	0.05	0.02	87.8	89.9	0.4	89.5	90.4
2013	274	1119	0.04	0.01	89.9	89.9	0.4	89.5	90.4
2013	274	1120	0.04	0.01	90.3	89.9	0.4	89.5	90.4
2013	274	1121	0.04	0.00	56.3	58.7	2.9	55.8	62.6
2013	274	1122	0.04	0.00	46.4	44.4	0.4	44.5	46.1
2013	274	1123	0.03	-0.01	46.1	44.5	0.3	44.2	46.0
2013	274	1124	0.03	-0.01	46.0	44.4	0.3	44.0	46.0
2013	274	1125	14.25	2.28	14.9	25.6	-2.6	31.0	20.1
2013	274	1126	21.20	0.03	0.6	0.0	-0.1	0.0	2.1
2013	274	1127	21.22	0.03	0.6	0.0	-0.1	0.0	2.1
2013	274	1128	21.23	0.03	0.5	0.0	-0.1	0.0	2.0
2013 2013	274	1129	21.24	0.03	0.5	0.0	-0.1	0.0	2.0
2013	274 274	1130	21.24	0.02	0.5	0.0	-0.1	0.0	2.0
2013	274	1131 1132	21.24 21.24	0.02	0.5	0.0	-0.1	0.0	1.9
2013	274	1132	21.24	0.02 0.02	0.6 0.5	0.0 0.0	-0.1	0.0	2.0
2013	274	1134	21.25	0.02	0.5 0.5	0.0	-0.1 -0.1	0.0	2.0
2013	274	1135	21.25	0.02	0.5	0.0	-0.1 -0.1	0.0	1.9
2013		1136	21.25		0.4	0.0	-0.1	0.0 0.0	1.9
2013	274	1137					-0.1 -0.1	0.0	1.8 1.8
2013	274	1138					-0.1 -0.1		1.8
2013	274	1139		0.00	0.4 0.6	-0.1	-0.1	0.0	1.8
2013	274		21.25	0.02	0.5		-0.1		1.8
2013	274	1141		0.02	0.5		-0.1	0.0	1.8
2013	274	1142	21.25	0.02	0.5	0.0	-0.1	0.0	1.8
2013	274	1143	21.25	0.02	0.4	0.0	-0.1	0.0	1.8
2013	274			0.02	0.6	0.0	-0.1	0.0	1.7
2013	274	1145	21.25 21.25	0.02	0.5	0.0	-0.1	0.0	1.7
2013	274	1146	21.25	0.02	0.5	0.0	-0.1	0.0	1.7
2013	274	1147	21.25	0.02	0.5	0.0	-0.1	0.0	1.7
2013	274	1148	21.25	0.02	0.5	-0.1	-0.1	0.0	1.7
2013	274	1149	21.26	0.02	0.5	0.0	-0.1	0.0	1.7
2013	274	1150	21.26	0.02		0.0	-0.1	0.0	1.7
2013	274	1151	21.26	0.02		0.0	-0.1	0.0	1.7
2013	274	1152	14.81	4.47		33.0	11.2	26.3	3.1
2013	274	1153	11.76	6.48		69.6	4.9		1.4
2013	274	1154	11.49	6.76			2.5	64.8	0.6
2013	274	1155	11.57	6.57		68.2	-1.8		0.6
2013	274	1156	11.90			67.1	-5.6		0.6

10/01/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	СО
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	1157	11.55	6.59	6.1	69.4	-4.7	74.1	0.6
2013	274	1158	12.33	6.13	6.5	67.3	-6.4	74.0	0.7
2013	274	1159	11.74	6.51	6.8	71.3	2.2	68.9	0.9
2013	274	1200	10.83	7.36	9.5	62.7	-3.3	65.9	0.9
2013	274	1201	9.93	8.38	17.4	73.2	0.7	72.3	1.1
2013	274	1202	8.65	9.07	21.0	64.1	5.4	58.6	1.4
2013	274	1203	9.36	8.70	21.2	53.5	2.3	51.1	0.9
2013	274	1204	8.44	9.12	21.5	49.7	1.0	48.8	0.9
2013	274	1205	9.74	8.27	18.0	43.3	-3.7	46.9	0.4
2013	274	1206	9.65	8.14	14.7	46.5	-2.4	48.8	0.4
2013	274	1207	10.75	7.50	11.7	47.1	-5.0	52.1	0.1
2013	274	1208	10.39	7.61	10.4	51.7	-2.5	54.0 ·	0.1
2013	274	1209	11.56	6.83	9.1	53.8	-2.0	55.9	0.2
2013	274	1210	11.05	7.15	8.2	60.0	3.7	56.2	
2013	274	1211	11.82	6.52	7.4	63.5	3.7	60.3	0.2
2013	274	1212	11.43	6.86	6.8	66.0	3.2 4.5	61.6	0.2
2013	274	1213	11.49	6.53	7.0	67.6			0.2
2013	274	1214	11.25	7.09	7.0 6.7	58.4	4.9	62.7	0.2
2013	274	1215	11.73	6.62	6.5		2.8	55.6	0.4
2013	274	1216	10.88	7.58	8.0	62.0 53.5	-1.6	63.6	0.3
2013	274	1217	8.92	8.66	14.1	53.5 52.8	-6.6 0.4	61.1	1.1
2013	274	1217	9.51	8.32	13.6		-0.1	52.9	0.6
2013	274	1219	9.40	8.21	14.0	52.5	-2.0	54.5	0.0
2013	274	1220	10.58	7.48		52.6	-2.0	54.6	-0.1
2013	274	1221	10.05	7. 4 6 7.76	11.5	47.8	-2.8	50.5	-0.1
2013	274	1221	11.05	7.78	10.6 9.9	48.6	1.7	46.7	-0.1
2013	274	1223	10.54	7.06		47.4	-1.1	48.5	-0.1
2013	274	1223	11.51	6.72	9.3	50.0	1.6	48.2	0.0
2013	274	1225	10.71	7.24	8.5	49.3	0.0	49.3	0.1
2013	274	1226	11.62	6.58	8.1	51.9 50.0	3.6	48.2	0.0
2013	274	1227	10.98	7.03	7.8	50.9	1.4	49.4	0.0
2013	274	1227	11.81	6.38	7.5 7.2	54.0	4.6	49.5	0.1
2013	274	1229	11.50	6.69	7.2 6.5	54.7 53.0	3.9	50.9	0.1
2013	274	1230	11.98	6.25	6.4	53.9	1.1	52.4	0.2
2013	274	1231	11.78	6.53	6.2	54.2 53.2	0.0	54.3	0.2
2013	274	1232	11.78	7.05			-3.7	56.8	0.3
2013	274	1233	9.60	8.26	8.6 17.1	61.8	-4.3	65.8	1.4
2013	274	1234	9.37	8.26	21.0	48.3 49.3	-3.1	51.1	0.1
2013	274	1235	10.74	7.34	19.6	50.9	0.2	49.1	0.0
2013	274	1236	10.74	7.70	19.0	56.6	0.3	50.3	0.0
2013	274	1237	11.19	6.95	18.4	58.4	3.3 3.0	53.3	-0.1
2013	274	1238	10.70	7.29	17.2	60.5	3.8	55.4 56.7	-0.1
2013	274	1239	11.36	6.73	17.2	60.8		56.7 50.1	-0.1
2013	274	1240	11.39	6.83	17.3	56.9	1.6 -4.0	59.1	-0.1
2013	274	1241	11.33	6.73	15.9	60.2	-4.0 -4.2	60.8	0.1
2013	274	1242	11.85	6.48	14.3			64.6	0.0
2013	274	1242	11.18	6.84	14.3	57.8	-6.1	64.0	0.0
2013	274	1243	12.02	6.29		62.0	-0.2	62.0	-0.2
2013	274				13.9	62.4	1.6	60.7	-0.2
2013	274	1245 1246	11.34	6.72 6.11	13.2	64.5	4.9	59.4	0.0
2013	274 274	1246	12.19 11.67	6.11 6.52	13.0	65.2	5.5	59.6	-0.1
2013 2013 ·	274 274	1247	11.67	6.52	12.2	64.1	2.8	61.1	-0.1
2013	274		11.46	7.03	15.2	61.3	3.3	57.9	1.2
2013		1249	8.98	9.02	25.3	61.0	-2.7	63.7	0.6
2013	274	1250	9.35	8.46	27.6	56.4	1.4	54.8	0.3
2013	274	1251	9.39	8.41	21.7	48.7	1.6	47.1	0.2
2013	274	1252	10.66	7.40	17.7	54.9	2.7	52.3	-0.4
2013	274	1253	10.47	7.62	14.0	57.4	0.9	56.5	-0.4

10/01/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	1254	11.28	6.90	13.4	62.7	1.4	61.3	-0.3
2013	274	1255	11.40	6.90	12.3	63.0	-5.4	68.6	-0.2
2013	274	1256	11.53	6.66	12.0	65.5	-5.1	70.5	-0.3
2013	274	1257	12.03	6.42	10.5	62.7	-6.0	68.6	-0.3
2013	274	1258	11.60	6.61	10.1	68.1	2.5	65.5	-0.3
2013	274	1259	12.15	6.18	9.5	68.5	2.8	65.7	-0.4
2013	274	1300	11.21	6.98	10.3	55.2	-4.2	59.4	-0.2
2013	274	1301	10.10	7.56	13.6	43.9	-2.7	46.6	-0.2
2013	274	1302	10.62	7.29	13.8	45.7	-0.8	46.4	-0.3
2013	274	1303	10.42	7.41	13.8	52.4	2.4	49.8	-0.4
2013	274	1304	10.52	7.64	16.4	56.6	1.6	54.9	-0.1
2013	274	1305	9.08	8.56	19.9	45.4	2.5	43.0	-0.7
2013	274	1306	10.93	7.19	16.6	53.1	0.9	51.9	-0.7
2013	274	1307	10.96	7.25	13.8	54.0	-2.6	56.3	-0.6
2013	274	1308	11.40	6.78	12.7	56.8	-3.2	60.0	-0.6
2013	274	1309	11.58	6.77	11.7	56.5	-6.1	62.6	-0.6
2013	274	1310	11.35	6.80	11.8	61.0	-3.6		-0.6 -0.6
2013	274	1311	12.05	6.41	11.3	65.2		64.4	
2013	274	1311	11.19	6.98	10.5	69.7	-0.4	65.3	-0.5
2013	274	1312	9.88	7.81			4.3	65.5	-0.5
2013	274	1314	9.24	8.28	15.4	52.5	1.0	51.4	-0.6
2013	274 274	1314	10.12	6.26 7.56	17.3	50.5	1.4	49.1	-0.6
2013	274 274				17.9	50.4	-0.1	50.3	-0.8
2013		1316	11.28	6.94	12.6	61.9	-1.6	63.4	-0.7
	274	1317	11.64	6.57	11.2	67.0	-0.8	67.6	-0.7
2013	274	1318	11.57	6.73	9.5	62.9	-5.4	68.2	-0.7
2013	274	1319	11.93	6.38	9.3	66.6	-5.2	71.8	-0.6
2013	274	1320	10.24	8.16	15.0	63.8	-6.7	70.5	-0.2
2013	274	1321	8.72	9.04	32.7	82.3	-8.5	93.3	-0.7
2013	274	1322	9.18	8.69	45.1	89.6	-7.0	98.2	-0.7
2013	274	1323	9.42	8.44	48.8	82.0	-0.4	82.9	-0.6
2013	274	1324	8.76	8.86	43.5	63.5	0.1	63.4	-0.6
2013	274	1325	9.24	8.37	42.5	52.5	-1.1	53.6	-0.8
2013	274	1326	9.05	8.53	34.0	46.4	-0.2	46.5	-1.0
2013	274	1327	10.18	7.74	30.2	47.9	1.8	46.2	-1.2
2013	274	1328	9.52	8.15	26.6	48.3	0.6	47.6	-1.2
2013	274	1329	10.71	7.31	24.9	50.2	1.8	48.2	-1.2
2013	274	1330	9.95	7.84	22.9	50.5	1.2	49.1	-1.2
2013	274	1331	10.97	7.09	20.8	52.0	2.4	49.5	-1.2
2013	274	1332	10.39	7.55	18.4	51.1	-0.9	51.8	-1.2
2013	274	1333	11.07	6.98	16.0	53.6	0.7	52.7	-1.2
2013	274	1334	10.77	7.29	15.6	53.2	-1.6	54.7	-1.2
2013	274	1335	11.48	6.75	15.9	55.1	-1.1	56.1	-1.1
2013	274	1336	9.26	8.77	27.4	69.5	5.8	63.8	-0.7
2013	274	1337	8.89	8.92	40.6	81.9	4.1	78.6	-0.9
2013	274	1338	9.41	8.65	36.5	59.2	-4.4	64.9	-1.0
2013	274	1339	8.68	8.92	33.4	49.1	-1.9	51.1	-1.4
2013	274	1340	9.45	8.52	29.8	44.2	-1.5	45.8	-1.4
2013	274	1341	9.52	8.28	28.8	45.8	0.5	45.2	-1.5
2013	274	1342	9.97	8.07	23.3	44.2	-2.9	47.0	-1.5
2013	274	1343	9.97	7.91	22.1	46.2	-0.9	47.1	-1.5
2013	274	1344	10.29	7.80	19.1	44.2	-2.7	46.8	-1.5
2013	274	1345	10.47	7.51	18.5	45.9	-0.8	46.7	-1.6
2013	274	1346	10.56	7.56	16.2	45.1	-3.6	48.7	-1.5
2013	274	1347	10.86	7.22	16.1	49.4	0.0	49.2	-1.6
2013	274	1348	10.74	7.39	14.1	49.4	-3.4	52.5	-1.5
2013	274	1349	11.29	6.88	13.3	52.2	-0.5	52.6	-1.5
2013	274	1350	10.93	7.21	12.2	52.7	-2.5	55.1	-1.4

10/01/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	1351	11.50	6.87	13.7	57.9	1.1	56.8	-1.3
2013	274	1352	9.43	8.43	27.2	72.6	-2.8	75.8	-1.5
2013	274	1353	9.60	8.39	51.8	95.1	-0.1	95.2	-1.9
2013	274	1354	9.81	8.20	60.1	94.7	-1.6	96.1	-1.8
2013	274	1355	9.61	8.29	59.5	93.2	-1.4	94.7	-1.9
2013	274	1356	9.53	8.32	58.1	91.8	-1.5	93.0	-1.8
2013	274	1357	9.61	8.24	54.8	90.7	1.7	88.9	-1.8
2013	274	1358	9.68	8.17	51.9	87.2	-0.2	87.1	-1.7
2013	274	1359	9.79	8.08	47.6	82.1	-1.7	83.8	-1.6
2013	274	1400	9.38	8.32	53.9	79.2	-4.8	83.9	-1.6
2013	274	1401	9.35	8.31	46.1	75.7	-5.5	81.6	-1.0
2013	274	1402	9.97	7.95	42.6	73.5	-4.4	78.0	-0.3
2013	274	1403	9.57	8.14	44.0	73.7	-0.7	74.4	0.3
2013	274	1404	9.52	8.18	49.7	72.5	-4.9	77.8	1.3
2013	274	1405	9.50	8.19	40.7	71.2	-1.9	72.8	2.5
2013	274	1406	9.61	8.10	35.3	65.6	-4.3	70.4	2.7
2013	274	1407	9.42	8.26	34.8	63.9	3.9	59.8	2.7
2013	274	1408	8.52	7.38	40.1	56.2	2.9	53.2	1.6
2013	274	1409	9.83	9.65	6.2	8.6	2.0	6.4	2.1
2013	274	1410	10.02	9.73	1.1	0.0	-0.1	0.0	-1.8
2013	274	1411	10.03	9.74	0.9	0.0	-0.1	0.0	-0.1
2013	274	1412	7.21	6.77	18.5	6.9	-3.6	20.1	8.5
2013	274	1413	0.07	0.09	86.4	88.0	-0.3	88.7	83.8
2013	274	1414	0.05	0.03	88.9	89.5	0.3	89.0	90.1
2013	274	1415	0.04	0.01	89.5	89.5	0.4	89.0	90.1
2013	274	1416	0.04	0.00	80.6	86.1	7.1	79.0	86.0
2013	274	1417	0.03	-0.01	46.6	44.9	0.5	44.4	48.5
2013	274	1418	0.03	-0.01	45.9	44.5	0.4	44.0	45.9
2013	274	1419	8.32	3.92	25.5	53.9	0.5	53.3	26.8
2013	274	1420	19.86	0.74	2.0	17.5	3.6	14.1	1.6
2013 2013	274	1421	21.20	0.02	0.6	0.0	-0.1	0.0	2.1
2013	274 274	1422	21.21	0.01	0.6	0.0	-0.1	0.0	2.2
2013	274 274	1423 1424	21.22	0.01	0.6	0.0	-0.1	0.0	2.2
2013	274 274	1424	21.23 21.23	0.01	0.5	0.0	-0.1	0.0	2.1
2013	274	1425	21.23	0.01 0.01	0.6	0.0	-0.1	0.0	2.2
2013	274	1427		0.01	0.6	0.0 0.0	-0.1 -0.1	0.0	2.2
2013	274	1428			0.5		-0.1 -0.1	0.0 0.0	2.2
2013	274	1429			0.5		-0.1 -0.1		2.2 2.2
2013	274	1430		0.01			0.0		2.2
2013	274	1431		0.01	0.5		-0.1		
2013	274	1432	21.24	0.01			0.0	0.0	
2013	274	1433	21.25	0.01	0.5		-0.1	0.0	
2013	274	1434	21.25	0.01	0.5	0.0	-0.1	0.0	2.1
2013	274	1435	21.24	0.01	0.5	0.0	-0.1 -0.1	0.0	2.1
2013	274	1436	21.25	0.01	0.5	0.0	-0.1	0.0	2.1
2013	274	1437	21.25	0.01	0.5 0.5	0.0	0.0	0.0	2.0
2013	274	1438	21.25	0.01	0.5	0.0	-0.1	0.0	2.1
2013	274	1439	21.25	0.01	0.4	0.0	-0.1	0.0	2.0
2013	274	1440	21.25	0.00	0.5	0.0	-0.1	0.0	2.0
2013	274	1441	21.25	0.01	0.4	0.0	-0.1	0.0	2.0
2013	274	1442	21.25	0.00		0.0	-0.1		2.0
2013	274	1443	21.25	0.00		0.0	-0.1 -0.1		2.0
2013	274	1444	21.25	0.00		0.0	-0.1		
2013	274	1445		0.00	0.4	0.0	-0.1 -0.1		
2013	274	1446	21.25	0.00	0.4	0.0	-0.1		
	274	1447	21.25	0.00		0.0	- 0.1		
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10/01/13									
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	1448	21.25	0.00	0.5	0.0	-0.1	0.0	1.9
2013	274	1449	21.25	0.00	0.5	0.0	-0.1	0.0	1.9
2013	274	1450	21.25	0.00	0.5	0.0	-0.1	0.0	1.9
2013	274	1451	21.25	0.00	0.4	0.0	-0.1	0.0	1.9
2013	274	1452	21.25	0.00	0.4	0.0	-0.1	0.0	1.9
2013	274	1453	21.25	0.00	0.4	0.0	-0.1	0.0	1.8
2013	274	1454	21.25	0.00	0.4	0.0	-0.1	0.0	1.9
2013	274	1455	21.25	0.01	0.5	0.0	-0.1	0.0	2.0
2013	274	1456	21.24	0.01	0.4	0.0	-0.1	0.0	2.2
2013	274	1457	21.23	0.01	0.4	0.0	-0.1	0.0	2.6
2013	274	1458	21.22	0.02	0.4	0.0	-0.1	0.0	2.7
2013	274	1459	21.22	0.01	0.5	0.0	-0.1	0.0	2.8
2013	274	1500	21.23	0.01	0.4	0.0	-0.1	0.0	2.9
2013	274	1501	21.23	0.01	0.4	0.0	-0.1	0.0	2.9
2013	274	1502	21.23	0.01	0.4	0.0	-0.1	0.0	2.9
2013	274	1503	20.96	0.25	0.5	0.4	0.0	0.4	2.9
2013	274	1504	11.45	6.58	2.2	40.7	-6.7	50.6	2.4
2013	274	1505	10.89	6.84	4.6	56.0	-1.8	57.8	1.5
2013	274	1506	12.98	5.58	4.5	66.2	3.8	62.2	1.5
2013	274	1507	12.78	5.80	5.3	74.1	3.2	70.7	2.1
2013	274	1508	10.06	7.99	14.2	52.1	-3.2	55.2	1.4
2013	274	1509	8.86	8.83	21.4	52.7	-4.0	56.8	1.3
2013	274	1510	9.82	8.05	19.2	52.8	-1.2	. 53.9	1.1
2013	274	1511	9.65	8.21	16.7	54.8	-3.0	57.7	1.0
2013	274	1512	10.61	7.42	15.7	52.4	-2.3	54.5	0.9
2013	274	1513	10.32	7.69	15.1	48.9	-5.4	54.3	1.0
2013	274	1514	11.16	6.96	13.8	53.1	-3.0	56.1	0.9
2013	274	1515	11.03	7.13	12.5	54.6	-4.3	58.8	1.0
2013	274	1516	11.51	6.64	11.7	60.7	-3.9	64.4	0.9
2013	274	1517	11.59	6.70	10.4	61.6	-2.3	63.8	1.0
2013	274	1518	11.41	6.68	10.4	69.9	3.0	66.8	0.9
2013	274	1519	12.08	6.34	9.6	70.6	5.1	65.4	1.0
2013	274	1520	11.47	6.62	10.0	72.3	2.4	70.0	1.0
2013	274	1521	12.28	6.15	9.7	72.9	6.1	66.7	1.0
2013	274	1522	11.58	6.56	9.0	70.1	-0.6	70.7	0.9
2013	274	1523	12.04	6.53	9.1	68.9	0.3	68.7	1.4
2013	274		9.06		18.3		-1.7	78.8	1.2
2013	274	1525	9.63	8.04			0.0		
2013	274	1526	10.18	7.74			-0.8	57.0	0.6
2013	274	1527	10.80	7.13	12.5	53.4	-1.7	55.0	0.6
2013	274	1528	11.22	6.94	10.0	55.5	-1.0	56.5	0.6
2013	274	1529	11.23	6.78	9.4	61.3	1.7	59.4	0.6
2013	274	1530	11.72	6.58	8.7	60.5	4.6	55.8	0.7
2013	274	1531		6.87	8.5	60.5	0.5	59.9	0.6
2013	274	1532	11.97	6.37	7.8	65.6	4.7	60.8	0.6
2013	274	1533		6.61	7.8	67.7	1.4	66.2	0.6
2013	274	1534	12.19	6.19	7.6	68.5	3.4	65.0	0.6
2013	274	1535	11.64	6.51	7.3	65.8	-5.7	71.8	0.6
2013	274	1536	11.85	6.29	7.3	72.0	1.0	70.0	0.6
2013	274	1537	12.42	6.01	6.7	73.0	5.5	67.2	0.6
2013	274		11.94	6.26		68.3	-5.0	73.6	0.6
2013	274		12.89	5.68	and the second s	69.6	-0.4	70.1	
2013	274	1540	10.41		8.0	57.8	-4.2	62.1	
2013	274	1541	10.30	7.60		54.2	-1.8	56.0	0.2
2013	274	1542	10.17	7.68	10.6	54.6	-4.0	58.4	0.3
2013	274	1543	11.55	6.62	8.9	57.3		60.3	0.4
2013	274	1544	11.40	6.75	<i>1.</i> T	57.3	-5.4	62.6	0.5

Year Julian Time O2 CO2 SO2 NOx NO2 NO Day (min) (%) (%) (ppm) (ppm) (ppm) (ppm) 2013 274 1545 12.07 6.19 7.3 62.4 -4.8 67.1 2013 274 1546 11.69 6.53 6.9 64.3 -4.4 68.9 2013 274 1547 11.98 6.20 7.3 67.4 -1.4 68.7 2013 274 1548 12.37 6.05 6.3 71.2 6.0 65.1 2013 274 1549 12.10 6.15 6.1 67.7 -1.8 69.4 2013 274 1550 12.63 5.76 6.3 66.5 -5.3 72.1 2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1553 11.09 6.88	CO (ppm) 0.6 0.5 0.5 0.6 0.6 0.8 0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4 0.4 0.5
Day (min) (%) (%) (ppm) (ppm) (ppm) (ppm) 2013 274 1545 12.07 6.19 7.3 62.4 -4.8 67.1 2013 274 1546 11.69 6.53 6.9 64.3 -4.4 68.9 2013 274 1547 11.98 6.20 7.3 67.4 -1.4 68.7 2013 274 1548 12.37 6.05 6.3 71.2 6.0 65.1 2013 274 1549 12.10 6.15 6.1 67.7 -1.8 69.4 2013 274 1550 12.63 5.76 6.3 66.5 -5.3 72.1 2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88	(ppm) 0.6 0.5 0.5 0.6 0.6 0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4 0.4
2013 274 1545 12.07 6.19 7.3 62.4 -4.8 67.1 2013 274 1546 11.69 6.53 6.9 64.3 -4.4 68.9 2013 274 1547 11.98 6.20 7.3 67.4 -1.4 68.7 2013 274 1548 12.37 6.05 6.3 71.2 6.0 65.1 2013 274 1549 12.10 6.15 6.1 67.7 -1.8 69.4 2013 274 1550 12.63 5.76 6.3 66.5 -5.3 72.1 2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33	0.6 0.5 0.6 0.6 0.8 0.8 0.8 0.7 0.9 0.3 0.3 0.3 0.4 0.4
2013 274 1546 11.69 6.53 6.9 64.3 -4.4 68.9 2013 274 1547 11.98 6.20 7.3 67.4 -1.4 68.7 2013 274 1548 12.37 6.05 6.3 71.2 6.0 65.1 2013 274 1549 12.10 6.15 6.1 67.7 -1.8 69.4 2013 274 1550 12.63 5.76 6.3 66.5 -5.3 72.1 2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274	0.5 0.6 0.6 0.6 0.8 0.8 0.7 0.9 0.3 0.3 0.3 0.4 0.4
2013 274 1548 12.37 6.05 6.3 71.2 6.0 65.1 2013 274 1549 12.10 6.15 6.1 67.7 -1.8 69.4 2013 274 1550 12.63 5.76 6.3 66.5 -5.3 72.1 2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70	0.5 0.6 0.6 0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4 0.4
2013 274 1549 12.10 6.15 6.1 67.7 -1.8 69.4 2013 274 1550 12.63 5.76 6.3 66.5 -5.3 72.1 2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.6 0.6 0.8 0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4 0.4
2013 274 1550 12.63 5.76 6.3 66.5 -5.3 72.1 2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.6 0.8 0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4
2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.6 0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4
2013 274 1551 11.55 6.65 7.2 59.3 2.8 56.3 2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4
2013 274 1552 10.33 7.30 9.1 45.6 0.7 44.7 2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.8 0.8 0.7 0.9 0.9 0.3 0.3 0.4
2013 274 1553 11.09 6.88 9.2 44.6 0.6 43.9 2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.8 0.7 0.9 0.9 0.3 0.3 0.4 0.4
2013 274 1554 10.33 7.32 9.1 44.7 -2.0 46.6 2013 274 1555 12.54 5.91 7.6 55.5 -0.7 56.3 2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.7 0.9 0.9 0.3 0.3 0.4 0.4
2013 274 1556 9.45 8.42 12.2 67.4 -4.1 71.5 2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.9 0.9 0.3 0.3 0.3 0.4 0.4
2013 274 1557 9.70 8.18 18.8 71.6 1.4 69.9	0.9 0.3 0.3 0.3 0.4 0.4
,	0.3 0.3 0.3 0.4 0.4
	0.3 0.3 0.4 0.4
2013 274 1558 9.58 8.25 15.1 46.2 -0.8 46.8	0.3 0.4 0.4
2013 274 1559 10.79 7.29 13.0 44.9 -1.9 46.8	0.4 0.4
2013 274 1600 10.72 7.38 10.9 46.3 -3.2 49.4	0.4
2013 274 1601 11.52 6.68 10.2 52.6 -3.1 55.6	
2013 274 1602 11.54 6.75 8.6 57.5 0.0 57.4	
2013 274 1603 11.84 6.40 8.3 61.3 -0.6 61.8	0.4
2013 274 1604 11.84 6.51 7.5 62.8 1.6 61.1	0.5
2013 274 1605 12.04 6.24 7.5 64.4 0.9 63.5	0.5
2013 274 1606 12.14 6.28 6.8 64.5 2.9 61.6	0.5
2013 274 1607 12.09 6.17 6.7 65.7 2.2 63.4	0.5
2013 274 1608 12.40 6.08 6.3 67.5 5.2 62.1	0.5
2013 274 1609 12.01 6.21 6.5 65.7 1.0 64.7	0.5
2013 274 1610 12.85 5.71 6.2 63.1 -2.2 65.4	0.5
2013 274 1611 12.26 6.15 6.1 62.2 -6.2 68.9	0.7
2013 274 1612 10.15 7.99 13.7 63.3 -3.7 66.8	1.0
2013 274 1613 9.06 8.73 19.9 51.6 -1.1 52.8	0.6
2013 274 1614 10.27 7.82 19.4 48.6 -0.8 49.7	0.1
2013 274 1615 9.81 8.01 18.7 50.6 -1.3 51.8	0.0
2013 274 1616 10.87 7.34 17.2 48.6 -0.3 48.8	0.0
2013 274 1617 10.34 7.56 18.0 48.6 -1.5 49.9	0.1
2013 274 1618 11.17 7.08 15.9 50.7 1.2 49.4	0.1
2013 274 1619 10.86 7.14 16.4 52.8 0.2 52.7	0.1
2013 274 1620 11.27 6.98 15.6 54.4 2.1 52.2	0.1
2013 274 1621 11.24 6.84 15.8 56.4 0.5 55.8	0.1
2013 274 1622 11.45 6,82 15.3 57.6 3.5 54.3	0.2
2013 274 1623 11.56 6.59 16.3 58.1 -0.2 58.2	0.1
2013 274 1624 11.52 6.74 13.9 59.0 2.3 56.3	0.1
2013 274 1625 11.76 6.44 14.9 58.5 -1.1 59.5	0.1
2013 274 1626 11.58 6.68 12.7 58.4 0.6 57.7	0.2
2013 274 1627 11.86 6.35 13.0 60.3 0.2 60.0	0.1
2013 274 1628 12.29 9.06 14.1 51.9 1.4 51.2	2.7
2013 274 1629 19.97 19.55 1.4 0.3 -0.7 1.5	0.9
2013 274 1630 19.99 19.63 0.6 0.0 -0.1 0.0	-1.5
2013 274 1631 17.70 16.73 0.7 0.0 -2.2 2.3	-1.4
2013 274 1632 10.06 9.80 0.5 0.0 -0.3 0.3	-0.7
2013 274 1633 4.45 4.11 40.8 43.1 11.6 31.3	29.0
2013 274 1634 0.09 0.11 86.8 88.9 -0.1 88.9	88.6
2013 274 1635 0.12 0.12 89.5 88.5 0.2 88.5	88.9
2013 274 1636 0.11 0.09 77.7 80.6 6.9 73.9	81.7
2013 274 1637 0.11 0.08 46.8 44.1 0.0 44.1	46.4
2013 274 1638 0.12 0.09 46.3 44.0 -0.1 44.0	45.0
2013 274 1639 4.97 0.05 38.3 37.3 -2.8 40.6	41.7
2013 274 1640 20.23 10.30 1.5 1.4 0.1 1.3	4.8
2013 274 1641 20.15 19.90 0.2 0.0 -0.1 0.0	-1.4

- 0,0-,-0	•								
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	CO
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	274	1642	20.16	19.92	0.0	0.0	-0.1	0.0	-1.4
2013	274	1643	20.16	19.95	0.0	0.0	-0.1	0.0	-1.1
2013	274	1644	19.14	18.62	-0.1	0.0	-0.1	0.0	-0.9
2013	274	1645	10.11	9.89	-0.2	0.0	-0.1	0.0	-0.1
2013	274	1646	4.79	4.42	56.2	105.7	25.1	82.8	44.6
2013	274	1647	-0.01	0.01	100.6	236.5	0.3	236.0	100.3
2013	274	1648	-0.02	0.00	100.5	207.5	24.7	182.9	100.3
2013	274	1649	-0.03	-0.01	94.2	91.4	0.4	91.0	94.4
2013	274	1650	-0.04	-0.01	93.5	91.4	0.4	90.9	92.6
2013	274	1651	-0.05	-0.01	93.5	91.4	0.4	91.0	92.9
2013	274	1652	-0.05	-0.02	59.1	62.1	3.5	58.7	67.7
2013	274	1653	-0.06	-0.02	47.0	44.9	0.4	44.8	48.6
2013	274	1654	1.38	-0.02	44.5	44.9	2.9	42.1	48.0
2013	274	1655	19.94	0.01	3.3	6.3	4.8	1.5	13.0

Table 10 Continuous Emissions Measurements Results Run 129-4 10/02/13

Time	NOx	NOx		со	co)	SO2	\$02		O2	02	CO2	CO2
(1-min)	(ppm)	(ppm Cor.)	(lb/hr)	(ppm)	(ppm Cor.)	(lb/hr)	(ppm)	(ppm Cor.)	(lb/hr)	(%)	(% Cor.)	(%)	(% Cor
846	48.0	48.9	0.30	1.3	1.3	0.00	8.8	8.6	0.07	12.87	12.70	5.45	5.59
847	43.8	44.6	0.27	9,2	9.0	0.03	7.5	7.3	0.06	14.36	14.18	4.53	4.63
848	46.1	47.0	0.29	12.7	12.5	0.05	7.6	7.4	0.06	13.40	13.23	5.41	5.54
849	43.2	43.9	0.27	1.0	1.0	0.00	13.7	13.3	0.11	10.22	10.08	7.67	7.88
850	35.8	36.4	0.22	1.5	1.5	0.01	18.1	17.6	0.15	9.11	8.98	8.41	8.64
851	34.0	34.6	0.21	0.8	0.8	0.00	15.3	14.8	0.13	8.63	8.51	8.73	8.97
852	38.1	38.8	0.24	0.6	0.6	0.00	21.4	20.7	0.18	7.60	7.49	9.36	9.62
853 854	34.4 30.4	34.9 30.9	0.21	1.8	1.8	0.01	22.7	22.0	0.19	9.91	9.77	7.84	8.05
855	40.0	40.7	0.19 0.25	3.2 1.5	3.1 1.5	0.01 0.01	16.2	15.7	0.13	9.56	9.43	8.03	8.25
856	45.6	46.4	0.28	2.6	2.5	0.01	10.5	10.2	0.09 0.06	10.97	10.82	6.93	7.11
857	48.3	49.3	0.30	3.1	3.0	0.01	7.5 6.8	7.2 6.6	0.06	11.65 12.29	11.50	6.48	6.64
858	49.1	50.1	0.31	1.5	1.5	0.01	6.0	5.8	0.05	12.29	12.13 12.07	6.03 6.04	6.18
859	48.5	49.5	0.30	3.8	3.7	0.01	5.1	4.9	0.04	12.60	12.44	5.81	6.19 5.95
900	50.1	51.1	0.31	2.3	2.2	0.01	4.8	4.7	0.04	12.68	12.51	5.74	5.88
901	50.0	50.9	0.31	2.6	2.6	0.01	4.3	4.1	0.04	12.48	12.32	5.85	6.00
902	49.4	50.4	0.31	2.6	2.6	0.01	4.4	4.2	0.04	12.89	12.72	5.59	5.72
903	56.9	58.1	0.35	3.5	3.4	0.01	3.9	3.8	0.03	13.44	13.27	5.24	5.36
904	61.1	62.4	0.38	1.8	1.8	0.01	10,5	10.2	0.09	9.52	9.39	8.90	9.15
905	67.5	69.0	0.42	1.3	1.3	0.00	18.9	18.4	0.16	8.69	8.56	9.22	9.48
906	53.0	54.1	0.33	2.5	2.5	0.01	18.4	17.9	0.15	9.45	9.32	8.57	8.81
907	48.5	49.4	0.30	2.9	2.8	0.01	16.5	16.0	0.14	9.68	9.54	8.27	8.50
908	47.2	48.1	0.29	2.1	2.1	0.01	13.6	13.2	0.11	10.41	10.27	7.70	7.91
909	49.7	50.7	0.31	1.9	1.9	0.01	12.4	12.0	0.10	10.98	10.83	7.21	7.40
910	50.9	51.9	0.32	1.7	1.6	0.01	13.6	13.2	0.11	11.17	11.02	7.04	7.23
911	53.9	55.0	0.34	1.3	1.2	0.00	12.4	12.0	0.10	11.02	10.87	7.08	7.27
912	55.6	56.8	0.35	2.2	2.2	0.01	10.0	9.7	0.08	11.62	11.47	6.65	6.82
913	57.4	58.5	0.36	1.9	1.9	0.01	8.5	8.3	0.07	11.74	11.58	6.54	6.71
914 915	58.6 58.2	59.8	0.36	1.2	1.2	0.00	8.5	8.3	0.07	11.80	11.64	6.46	6.62
916	58.8	59.4 60.0	0.36	1.9	1.9	0.01	7.7	7.5	0.06	11.78	11.62	6.49	6.66
917	58.3	59.5	0.37 0.36	2.3 1.8	2.3	0.01	7.3	7.1	0.06	12.10	11.94	6.25	6.40
918	59.2	60.4	0.36	1.6	1.7 1.6	0.01 0.01	7.0 6.1	6.8	0.06	12.19	12.03	6.18	6.33
919	59.7	61.0	0.37	2.3	2.3	0.01	5.5	5.9 5.4	0.05 0.05	12.15 12.82	11.99	6.15	6.31
920	68.2	69.7	0.43	1.7	1.6	0.01	6.2	6.0	0.05	12.02	12.65 11.85	5.79	5.93
921	63.9	65.3	0.40	1.3	1.3	0.00	10.6	10.3	0.09	10.17	10.03	6.70 7.84	6.88 8.05
922	55.0	56.2	0.34	1.8	1.8	0.01	11.4	11.1	0.09	11.17	11.02	7.05	7.24
923	52.1	53.1	0.32	1.7	1.7	0.01	10.2	9.9	0.08	11.41	11.26	6.81	6.99
924	52.1	53.1	0.32	1.0	1.0	0.00	9.3	9.0	0.08	11.41	11.26	6.72	6.90
925	51.6	52.6	0.32	2.1	2.1	0.01	8.6	8.3	0.07	11.81	11.65	6.49	6.65
926	53.6	54.7	0.33	1.6	1.6	0.01	8.3	8.0	0.07	12.00	11.84	6.31	6.47
927	55.3	56.4	0.34	1.5	1.5	0.01	7.0	6.8	0.06	11.77	11.61	6.43	6.60
928	55.2	56.3	0.34	2.2	2.1	0.01	5.8	5.6	0.05	12.15	11.99	6.18	6.33
929	54.8	55.9	0.34	2.3	2.3	0.01	5.2	5.0	0.04	12.22	12.06	6.12	6.27
930	55.0	56.1	0.34	1.6	1.6	0.01	4.8	4.7	0.04	12.27	12.11	6.08	6.23
931	54.7	55.8	0.34	2.0	2.0	0.01	4.2	4.1	0.03	12.05	11.89	6.20	6.36
932	54.1	55.2	0.34	2.5	2.5	0.01	4.3	4.1	0.04	12.38	12.22	5.98	6.13
933	53.4	54.5	0.33	1.9	1.8	0.01	4.7	4.6	0.04	12.44	12.28	5.93	6.07
934	54.4	55.5	0.34	1.7	1.7	0.01	4.4	4.3	0.04	12.22	12.06	6.05	6.20
935	62.5	63.9	0.39	2.8	2.7	0.01	4.5	4.3	0.04	13.12	12.95	5.44	5.57
936 937	83.1 125.3	85.0	0.52	2.9	2.9	0.01	5.9	5.7	0.05	10.59	10.45	7.96	8.18
937	65.3	128.4 66.7	0.78 0.41	2.7 2.1	2.7 2.1	0.01 0.01	19.1 24.0	18.5 23.3	0.16	9.46 10.49	9.33	8.45	8.68
									0.20	10.49	10.35	7.52	7.72
Ave	53.9	55.0	0.34	2.3	2.3	0.01	9.8	9.5	0.08	11.42	11.27	6.79	6.97

10/02/13									
Year	Julian	Time	02	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	275	759	20.32	0.04	-0.3	0.1	0.0	0.0	5.9
2013	275	800	20.32	0.05	-0.3	0.1	0.0	0.1	6.0
2013	275	801	20.32	0.05	-0.3	0.1	0.0	0.1	6.1
2013	275	802	20.32	0.04	-0.3	0.0	-0.1	0.0	6.0
2013	275	803	20.32	0.04	-0.4	0.0	-0.1	0.0	5.8
2013	275	804	20.33	0.04	-0.3	0.0	-0.1	0.0	6.0
2013	275	805	20.33	0.04	-0.3	0.0	0.0	0.0	6.3
2013	275	806	20.33	0.04	-0.4	0.0	-0.1	0.0	5.8
2013	275	807	20.38	8.19	-0.1	0.0	-0.4	0.3	5.1
2013	275	808	20.32	19.84	-0.4	-0.1	-0.1	0.0	2.7
2013	275	809	20.32	19.67	-0.3	0.0	-0.1	0.0	1.5
2013	275	810	20.33	19.57	0.0	0.0	-0.1	0.0	0.1
2013	275	811	8.38	7.42	63.5	98.5	2.8	111.4	52.9
2013	275	812	0.04	0.04	100.6	237.6	0.3	237.3	100.3
2013	275	813	0.09	0.02	100.3	192.4	-2.7	213.2	100.3
2013	275	814	0.01	0.01	96.5	91.7	0.6	91.0	94.2
2013	275	815	4.67	5.09	75.3	84.2	6.9	77.3	85.0
2013	275	816	20.34	19.57	1.5	3.9	3.8	0.0	9.8
2013	275	817	20.36	19.60	0.2	0.0	-0.1	0.0	0.1
2013	275	818	8.39	7.48	65.3	104.3	3.7	113.6	51.8
2013	275	819	0.02	0.04	100.6	236.5	1.2	235.5	100.3
2013	275	820	0.01	0.02	96.4	142.5	12.8	131.2	98.9
2013	275	821	0.00	0.01	90.2	91.4	0.4	90.8	92.5
2013	275	822	0.02	0.01	68.9	76.7	3.0	73.5	82.4
2013	275	823	-0.02	0.00	44.6	44.9	0.4	44.9	48.2
2013	275	824	-0.02	0.00	45.1	44.9	0.4	45.0	47.6
2013	275	825	6.21	6.19	20.5	24.4	1.3	23.2	30.5
2013	275	826	10.16	9.78	0.2	-0.1	-0.1	0.0	1.5
2013	275	827	10.14	9.83	0.0	0.0	-0.1	0.0	1.1
2013	275	828	16.90	3.14	1.5	9.1	2.5	6.7	3.0
2013	275	829	13.49	5.00	1.7	43.1	-1.2	44.3	2.8
2013	275	830	13.42	5.07	2.0	44.2	-1.0	45.1	2.3
2013	275	831	15.81	3.48	1.7	35.1	1.8	33.2	2.8
2013	275	832	20.91	0.16	1.0	5.1	1.7	3.2	3.0
2013	275	833	19.29	1.43	0.9	3.9	-2.4	7.6	3.1
2013	275	834	13.08	5.30	1.9	45.2	-1.5	47.2	2.2
2013	275	835 836	12.95	5.39	2.5	47.6	-0.8	48.5	
2013	275	836	11.11	5.24	5.6	42.0	-0.6	42.4	5.6
2013	275	837	10.15	9.75	1.5	2.8	-0.1	2.7	4.8
2013	275	838	10.16	9.84	0.4	0.3	-0.1	0.3	0.3
2013	275	839	8.96	8.45	7.8	3.6	-2.4	8.0	2.5
2013	275	840	0.10	0.12	82.6	85.1	2.7	82.4	76.5
2013	275	841	0.06	0.05	88.0	89.9	0.4	89.5	90.4
2013	275	842	0.05	0.03	75.8	75.2	-3.4	81.3	82.5
2013	275	843	0.04	0.02	46.3	44.7	0.3	44.5	47.0
2013	275	844	0.91	0.51	45.0	44.7	-0.9	45.9	45.7
2013	275	845	13.11	5.22	14.7	48.4	3.5	44.9	14.5
2013	275	846	12.87	5.45	8.8	48.0	-1.1	48.9	1.3
2013	275	847	14.36	4.53	7.5	43.8	-9.3	54.7	9.2
2013	275	848	13.40	5.41	7.6	46.1	-2.4	48.6	12.7
2013	275	849	10.22	7.67	13.7	43.2	-0.5	43.6	1.0
2013	275	850	9.11	8.41	18.1	35.8	1.2	34.7	1.5
2013	275	851	8.63	8.73	15.3	34.0	0.3	33.7	
2013	275	852	7.60	9.36	21.4	38.1	0.3	37.8	
2013	275	853	9.91	7.84	22.7	34.4	2.0	32.3	1.8
2013	275	854	9.56	8.03	16.2	30.4	-1.1	31.5	3.2
2013	275	855	10.97	6.93	10.5	40.0	0.6	39.4	1.5

SMMI - Pogo Mine 10/02/13

10/02/13	i								
Year	Julian	Time	O2	CO2	SO2	NOx	NO2	NO	co
	Day	(min)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2013	275	856	11.65	6.48	7.5	45.6	-0.3	45.9	2.6
2013	275	857	12.29	6.03	6.8	48.3	1.9	46.6	3.1
2013	275	858	12.23	6.04	6.0	49.1	-1.2	50.2	1.5
2013	275	859	12.60	5.81	5.1	48.5	-1.2	49.7	3.8
2013	275	900	12.68	5.74	4.8	50.1	1.0	49.2	2.3
2013	275	901	12.48	5.85	4.3	50.0	0.6	49.3	2.6
2013	275	902	12.89	5.59	4.4	49.4	0.4	49.1	2.6
2013	275	903	13.44	5.24	3.9	56.9	3.9	52.9	3.5
2013	275	904	9.52	8.90	10.5	61.1	2.6	58.4	1.8
2013	275	905	8.69	9.22	18.9	67.5	1.0	66.1	1.3
2013	275	906	9.45	8.57	18.4	53.0	0.4	52.7	2.5
2013	275	907	9.68	8.27	16.5	48.5	-1.4	49.9	2.9
2013	275	908	10.41	7.70	13.6	47.2	-1.6	48.8	2.1
2013	275	909	10.98	7.21	12.4	49.7	-0.9	50.5	1.9
2013	275	910	11.17	7.04	13.6	50.9	-2.1	52.9	1.7
2013	275	911	11.02	7.08	12.4	53.9	-0.8	54.7	1.3
2013	275	912	11.62	6.65	10.0	55.6	0.8	54.7	2.2
2013	275	913	11.74	6.54	8.5	57.4	1.1	56.1	1.9
2013	275	914	11.80	6.46	8.5	58.6	-0.8	59.3	1.2
2013	275	915	11.78	6.49	7.7	58.2	-1.5	59.6	1.9
2013	275	916	12.10	6.25	7.3	58.8	-1.0	59.8	2.3
2013	275	917	12.19	6.18	7.0	58.3	-2.2	60.6	1.8
2013	275	918	12.15	6.15	6.1	59.2	-1.1	60.3	1.6
2013	275	919	12.82	5.79	5.5	59.7	-3.8	63.5	2.3
2013	275	920	12.01	6.70	6.2	68.2	-0.1	68.1	1.7
2013	275	921	10.17	7.84	10.6	63.9	0.2	63.6	1.3
2013	275	922	11.17	7.05	11.4	55.0	-0.4	55.4	1.8
2013	275	923	11.41	6.81	10.2	52.1	0.1	52.0	1.7
2013	275	924	11.41	6.72	9.3	52.1	-0.4	52.5	1.0
2013	275	925	11.81	6.49	8.6	51.6	-1.5	53.1	2.1
2013	275	926	12.00	6.31	8.3	53.6	-0.5	54.2	1.6
2013	275	927	11.77	6.43	7.0	55.3	-0.1	55.5	1.5
2013	275	928	12.15	6.18	5.8	55.2	1.9	53.3	2.2
2013	275	929	12.22	6:12	5.2	54.8	1.7	53.1	2.3
2013	275	930	12.27	6.08	4.8	55.0	0.9	54.0	1.6
2013	275	931	12.05	6.20	4.2	54.7	0.3	54.6	2.0
2013	275	932	12.38	5.98	4.3	54.1	0.5	53.7	2.5
2013	275	933	12.44	5.93	4.7	53.4	-1.4	54.8	1.9
2013	275	934	12.22	6.05	4.4	54.4	-0.4	54.5	1.7
2013	275	935	13.12	5.44	4.5	62.5	0.2	62.6	2.8
2013	275	936	10.59	7.96	5.9	83.1	0.8	82.5	2.9
2013	275	937	9.46	8.45	19.1	125.3	2.3	122.9	2.7
2013	275	938	10.49	7.52	24.0	65.3	1.3	63.9	2,1

RM 3 MOLECULAR WEIGHT DETERMINATION

Client: Pogo Mine		<u> </u>	Operator: J	Rosburg	
Plant Location: Delta Junction, AK		Ambient	Temperature:	65	
Test Location: Incinerator			_		
Sample Type (circle one):	Bag	Integrated	Continuous	Other	
Has Orsat or Fyrite unit been successfully	leak che	cked?	YES/NO		

			% O ₂			% CO ₂	
Date	Bag ID/Run Number	Actual Re	eadings	Average	Actual Rea	dings	Average
		10.45	10.49		7.91	7.96	
10/02/13	l29-4			10.47			7.94
40/00/400		10.83	10.92		7.47	7.41	
10/02/130	123-4			10.88			7.44
10/02/130	15-4	10.72	10.79	40.70	7.62	7.77	
10/02/130	15-4	 		10.76			7.70
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	AIICOM	Moietura	Final	799.9	621.3	720.5	848.3				in. H ₂ 0/15 sec.	nr. H ₂ 0/15 sec.	Vacuum	(in. Hg)	7	5	7	20	7,	4	و)	2	tr-	4	**	Ĕ	+ 12	7	7	7-	14	1	4	4	7		Max Vac	
	~ ~		Initial		2 589.3			Net Gain		Static	0		DCM Transport	emp. (<i>F</i> .)	2.5	51	17	5(52	2.5	5.3	54	75	35	5+	57	23	7	2.5	5.9	308	5,5	59	09	13	7,9		3M Temp.	4
	165, to 153.4	_	_	. 6	F 77.	F.75.	2 . 62			Impact	o		1 200	ד ואיסרו	53	5.3	77	56 50	60	79	64	6.5	67	89	607	6.3	65	6 C	68	69	10	72	72	72	×,	74		Average DC	59,4
7! (20)!		7071		 -						Pitot:	Pre: Post	1001	Imp. Outlet Temp	(f)	9	38	000	35	39	35	37	2 5	1/5	41	45	//5	37,	17,	25	42	275	43	2.5	43	4,5	77			
in the second decrease of the second decrease	77	1306	\$2.	, , ,	1556	51.51	22.5	היינסיל	10t1 T		in. Hg Vac.		Filter Temp.	(F)	252	457	754	1.52	182	25,	3,7,5	248	250	250	727	254	252	252	251	251	250	250	250	245	2,70	640			
165.5 162.9 160.4 158.0	OKINETIC SAMPLE DATA FORM							911	4/4		01		Probe Temp.	(P)	235	257	747	251	257	760	22.5	255	242	241	246	25.2	7,79	254	346	253	251	245	241	745	0 7 7	7			
5721 0021 0511 0511	CSAMPLEI	24	56	28,00	2000		30	710 0 570	2		acf		Stack Temp. (F)	,	27.	12761	10.11	1178	1134	1771	20.7	1156	1)41	25 25	1123	1130	1121	2711	143	4.55	1130	21.43	1164	1167	377	42.11		Avg. ts	1151
Control of the contro	ISOKINETI		Ę.	Hg):	15U):			1 0 75 V		1	2000		HV	(m. ft ₂ 0)	7.65	75.7	1.66	(,60	1,66	G	29	1.63	1.63	1.63	1.66	1.66	2	1,63	1.63	1,63	90.7	1.6.7	1.63	1.6.3	^ ^			Avg. AH	,
or the first control of the fi		Filter ID:	Ambient Temp. (P.)	Saro. Fress. (in. Hg):	O ₂ (%);	CO, (%):	Duct Dia. (in):	Nozzle Dia (in)	K Factor:	Leak Check:	Pre: ○. ○. Post: ★ 10226		ΔP 9.	(ML. FI ₂ O.)	6.03	0.000	0.01	0.0	15,0	10.07	1000	0.01	0,01	12.6	0,01	0.0	10 0	10.0	100	5.6	1 1	0.01	12.2	0.0	60			Avg. VAP	10/07
			ME						1				DGM Reading	(DACE)	152113	144, 02	146.65	148,08	(5(.09	155.24	15,751	159.83	167.12	164.64	168.56	170.76	01.31	177,43	79.57	20 7 0	186.32		196.85	195.06	Ι.			Vol. (DACF)	50,400
			المرابع المرابع	19 13	- 4		D.S. AW	503	1.733		12M5		Sample Time	(, ~	e	b	21	<u>C</u>	22 - 7	74	2.1	30	3 5	34	27	2,5	15	24	1				75	70,	13	+	\vdash	9
The state of the s	,	2040	De146 1	120,26/27		H	\$G	151		r outlet I.D.	e: H		Port/Point I.D.	-		167	2	5	۶ و	v	,,,	0	5 5	2 1		M:	2 ~	į	50	200	10		12						
		Plant	Source I D.	Date:	Flow Traverse Time:	Run No.:	Operators:	Meter Y:	Meter Delta H@:	Probe I.D./ Impinger outlet I.D.:	Pitot Coeff. (Cp):		DGM Clock	7007										1112 11157	,						a					1242			

			2	~	₹*		7		[_
		Change	87.2						Meter Pres.	(in Hg)	28.12	28.23	28.17	28.12	00 13
	IIe	Final	799.9	621.3	720.5	699.3	898.3	3739.3	Stack Pres	(in Hg)	28.00	28.00	28.00	28.00	00 00
	Moisture	Initial	712.7	589.3	714.1	9.269	9.988	3600.3	velocity	(ft/s)	10.2	14.8	12.8	10.3	10.3
								Sum	DGM Ave	(F)	52.5	52.0	52.5	53.5	. 0 25
									DGM Outlet	(F)	52.0	51.0	51.0	51.0	52.0
	ю	28	0.04	0.8747	1.7732	1.0034	139		DGM Inlet	(F)	53.0	53.0	54.0	56.0	58.0
	= (1		11	=					Stack T	(F)	1148	1243	1224	1174	1178
	Point Duration (min) =	Bar. Pres. (in Hg) =	Static Pres. (in WC) =	Nozzle Dia (in WC) =	Meter dH @=	Meter Yd =	H2O Mass (ml/g) =		dH1/2	(in WC)1/2	1.28	1.75	1.53	1.26	1 26
									HP	(in WC)	1.63	3.07	2.33	1.60	1.60
	fine	AK							dP1/2	(in WC)1/2	0.10	0.14	0.12	0.10	0.10
	SMMI - Pogo Mine	Delta Junction, AK	Incinerator	15-1	09/29/13	1106-1242	81		ď₽	(in WC)	0.01	0.02	0.02	0.01	0.01
•							in) =		Sample Volume	(acf)	2.162	2.740	2.630	2.230	2,200
	Plant =	Plant Location =	Source ID =	Run No =	Date =	Run Time =	Sample Duration (min) =		DGM Reading Sample Volume	(acf)	139.118	141.280	144.020	146.650	148.880
	I	I	V 1	-	П		V 1		oint No.		1	2	m	4	5

Meter Pres.	(in Hg)	28.12	28.23	28.17	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12		28.13
Stack Pres	(in Hg)	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00		28.00
velocity	(ft/s)	10.2	14.8	12.8	10.3	10.3	10.2	10.2	10.3	10.3	10.2	10.2	10.2	10.1	10.1	10.1	10.1	10.1	10.2	10.2	10.2	10.1	10.1	10.2	10.3	10.2	10.2	10.2		10.46
DGM Ave	(F)	52.5	52.0	52.5	53.5	55.0	26.0	57.5	58.5	59.5	0.09	60.5	61.5	59.0	59.5	0.09	61.0	61.5	62.0	62.5	63.5	63.5	65.0	65.5	65.5	66.5	.0.79	67.5		60.31
DGM Outlet	(F)	52.0	51.0	51.0	51.0	52.0	52.0	53.0	53.0	54.0	54.0	54.0	55.0	57.0	57.0	57.0	57.0	57.0	57.0	57.0	58.0	58.0	59.0	59.0	59.0	60.0	61.0	61.0		55.78
DGM Inlet	(F)	53.0	53.0	54.0	56.0	58.0	0.09	62.0	64.0	65.0	0.99	67.0	0.89	61.0	62.0	63.0	65.0	0.99	67.0	0.89	0.69	0.69	71.0	72.0	72.0	73.0	73.0	74.0		64.85
Stack T	(F)	1148	1243	1224	1174	1178	1134	1141	1163	1170	1156	1141	1146	1128	1123	1130	1121	1122	1145	1143	1135	1124	1130	1143	1164	.1162	1152	1140		1151.1
dH1/2	(in WC)1/2	1.28	1.75	1.53	1.26	1.26	1.29	1.28	1.26	1.26	1.28	1.28	1.28	1.29	1.29	1.29	1.29	1.29	1.28	1.27	1.28	1.29	1.29	1.28	1.28	1.28	1.28	1.28		1.31
Ħ	(in WC)	1.63	3.07	2.33	1.60	1.60	1.66	1.63	1.60	1.60	1.63	1.63	1.63	1.66	1.66	1.66	1.66	1.66	1.63	1.63	1.63	1.66	1.66	1.63	1.63	1.63	1.63	1.63		1.71
dP1/2	(in WC)1/2	0.10	0.14	0.12	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10		0.10
₽	(in WC)	0.01	0.02	0.02	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.01
Sample Volume	(acf)	2.162	2.740	2.630	2.230	2.200	2.190	2.310	2.130	2.120	2.290	2.120	2.176	2.144	2.200	2.220	2.220	2.230	2.140	2.310	2.220	2.220	2.190	2.340	2.210	2.200	2.150	2.115		
DGM Reading	(acf)	139.118	141.280	144.020	146.650	148.880	151.080	153.270	155.580	157.710	159.830	162.120	164.240	166.416	168.560	170.760	172.980	175.200	177.430	179.570	181.880	184.100	186.320	188.510	190.850	193.060	195.260	197.410	199.525	60.407
Point No.			7	m	4	5	9	7	∞	6	10	Ε	12	-	7	es.	4	5	9	7	∞	σ.	10	11	12					

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		ISOKINETIC SAMPLE DATA FORM	T (6,2)	×	A COM
Plant	Page Mile	Filter ID: ρL	5211	(65.8-	
Location:	Deita Sunction MK	Ambient Tenn (PF):	<i>3</i> .5℃		Moisture
Source I.D.:	incinoration	Baro. Press. (in. Hg): 25. 26			minal C
Date:	9-30-13	8	5/12	_	1 4/3.8 806.7
Flow Traverse Time:	۳. ۸		(20)	(5.0	15/9 0.00.2
Run No.:	1.51	CO ₂ (%):	1	o o	3 7/40 4/7.8
Operators:	DB, AW	Duct Dia. (in): 30 ".	12221 -	- (15.5. 6	4 400.7
Meter Box I.D.:	Blacik	B _{we} (assumed): /2		- .	J 270, 3 707. +
Meter Y:	1,00739	Nozzle Dia. (in): O. 8747	ſ		Ivet Gain
Meter Delta H@:	1.7732	K Factor:	•		
Probe I.D./ Impinger outlet I.D.:	r outlet I.D.: 403	Leak Check:	ا چۇن		
Probe Length/Type:	41 pms	7 6	in Ho Vac Pre-		mipaci Static
Pitot Coeff. (Cp):	2.84	Post: 0.201 acf 2	in. Hg Vac. Post:		in ti 0/15 acc.
					III. TAZOL I J SEC.

Vacuum	(in. Hg)	•	V	1	V	v	1	7		1	a co	ì	ال و	9	2	3 ~	2	٥	Ó	اد	7	7	ا	2	_	-	\ \ \	,	ļ			Max. Vac.	
OGM Temn (P)	(1) ·dim	ડેવ	\$	25	56	, cc		100	30) 3	3	(C. 2)	7.5	7 2 3		2 2 3	100	70	62	2/2	اور	67	んつ	67	67	60	300	37	8	0 67		iM Temp.	
DGM Te	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	59	- 7	(6.7	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	33	50%	3,7	2/2	200	73	26	76	7-	31	100	77	20	03,0	٦٥	×	12	တ	79	79	<i>S</i>	79	74	78			Average DGM Temp.	
Imp. Outlet Temp.	(P)	<u>\\Z</u>	lμ	7.5	7	- 7	7	1.77	42	22	24	42	24.	47	2.5	25	77	27.7	27		4,5	<u>, , , , , , , , , , , , , , , , , , , </u>	45	43	43	43	£.h	43	itu				
Filter Temp.	(F)	247	C+2	2\$2	£52	252	286	253	252	522	442	246	252	452	25.7) 52	24.0	250	7770	12.0		250	2 57	0.57	281	252	251	152	152				
Probe Temp.	£	251	255	152	248	LHZ	552	282	250	372	248	249	251	254	745	253	248	250	249	200	120	25.2	7 5 7	249	251	752	254	152	250				
Stack Temp. (F)		100	(126	1150	ાહ	hhi	1101	9511	1153	1111	(175	1145	11,67	1411	45)1	501)	1166	1125	1771	1/517	1/3/1	161	37)	(77)	8911	22))	1132	(133	1130			Avg. t _s	
HV HV	(117-1170)	1.66	1.66	ر ر	1.63	ر <i>د</i> خ	1,63	1,63	1.63	1,60	1,60	1,63	1,60	1.63	1,63	23')	(.63	77')	1,50	2/1	1,7,7		987	< a).	29,7	1.60	٠. ردو	1,66	(,66			Avg. AH	
dV (O'H (ii)	(Mt. 1120)	10.5	0.0(0.01	0.0(0,01	0.01	0.6;	0.01	0.01	0-01	0.0(0.01	0.01	100	0.01	0.01	10.0	0.03	0	100	100	0.0	0.0	0	0.0)	,	10.0	0.01			Avg. VAP	-
DGM Reading	(YOUG)				J		438.28	440.43	442,61	רה,ויייי	446.94	449.17	451,25	453,39	455.55	457 61	459,49		464, 42	29 711		12 11-17	1,1,1,1	J,	415,40	471.60	١١	482.00	484, 19	484.918		Vol. (DACF)	
Sample Time (min.)) 2 1	1	- 1	15 5	21 02	25 15	30 18	12 56	75 27	1225	20 30		36	39	24	45	84	15	7.5	57	T	23			Ì		13	တ	79		Total Time	
Port/Point I.D.			3,	×	2	~	۰)	œ	3	3	=	1,7		2	~	3	>	9	-	Ċ	2		2)		7)							_
DGM Clock Time	1200	- 62																												(A/I)			ş

Change 91.1 23.1	2.9	9.4	Meter Pres.	(in Hg)	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37
Final 806.9 613.1	719.9	907.7 3748.0	Stack Pres	(in Hg)	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25
Moisture Initial 715.8 590.0	717.0	898.3	velocity	(ft/s)	10.0	10.1	10.2	10.2	10.1	10.2	10.2	10.2	10.2	10.3	10.1	10.2	10.1	10.2	10.0	10.1	10.2	10.2	10.1	10.1	10.1	10.2	10.2	5.4	10.2	5.4	5.4	9.64
		Sum	DGM Ave	(F)	59.0	0.09	61.0	62.0	63.5	64.0	65.0	65.0	0.79	0.79	68.5	69.5	70.0	70.0	. 70.5	70.5	71.5	72.0	72.0	73.0	73.5	73.0	73.0	74.0	73.5	73.5	73.5	68.70
			DGM Outlet	(F)	59.0	59.0	59.0	59.0	59.0	59.0	0.09	0.09	0.19	61.0	62.0	63.0	63.0	64.0	64.0	64.0	65.0	0.99	0.99	67.0	67.0	67.0	67.0	68.0	68.0	68.0	68.0	63.44
3 28.25 0.04 0.8747	1.7732	126.8	DGM Inlet	(F)	59.0	61.0	63.0	65.0	68.0	0.69	70.0	70.0	73.0	73.0	75.0	76.0	77.0	76.0	77.0	77.0	78.0	78.0	78.0	79.0	80.0	79.0	79.0	80.0	79.0	79.0	79.0	73.96
n) = = = () = () =		n.	Stack T	(F)	1109.0	1126.0	1150.0	1168.0	1144.0	1161.0	1150.0	1153.0	1171.0	1179.0	1145.0	1167.0	1141.0	1157.0	1109.0	1166.0	1125.0	1177.0	1156.0	1134.0	1138.0	1145.0	1168.0	1172.0	1132.0	1133.0	1130.0	1148.37
Point Duration (min) = Bar. Pres. (in Hg) = Static Pres. (in WC) = Nozzle Dia (in WC) =	Meter dH @ = Meter Yd =	H2O Mass (ml/g) =	dH1/2	(in WC)1/2	1.29	1.29	1.28	1.28	1.28	1.28	1.28	1.28	1.26	1.26	1.28	1.26	1.28	1.28	1.29	1.28	1.29	1.26	1.28	1.29	1.29	1.28	1.26	1.26	1.29	1.29	1.29	1.28
			Η̈́	(in WC)	1.66	1.66	1.63	1.63	1.63	1.63	1.63	1.63	1.60	1.60	1.63	1.60	1.63	1.63	1.66	1.63	1.66	1.60	1.63	1.66	1.66	1.63	1.60	1.60	1.66	1.66	1.66	1.63
dine AK			₽1/2	(in WC)1/2	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
SMMI - Pogo Mine Delta Junction, AK Incinerator 15-2	09/30/13 1251-1410	6/	ф	(in WC)	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
		= (un	Sample Volume	(acf)	2.197	2.160	2.160	2.180	2.150	2.150	2.180	2.160	2.170	2.230	2.080	2.140	2.160	2.060	2.380	2.230	2.200	2.200	2.260	2.230	2.090	2.200	2.200	2.180	2.220	2.190	0.728	
Plant = Plant Location = Source ID = Run No =	Date = Run Time = Some le Direction (**)	Sample Duranon (min) =	DGM Reading	(acf)	427.433	429.630	431.790	433.950	436.130	438.280	440.430	442.610	444.770	446.940	449.170	451.250	453.390	455.550	457.610	459.990	462.220	464.420	466.620	468.880	471.110	473.200	475.400	477.600	479.780	482.000	484.190	57.485
			Point No.			7	ĸ	4	۰ ۲۷	9	7	∞ .	σ ;	10		12	-	2	m	4 '	5	9	7	∞ -	6	10	11	12				

AFCOM	Noithean Walter	Imp. Initial Final	1715.8 807.8	2 591.1 618.2	375,8 749,3	4 659 4 700.7	2,707.5	Net Gain
1(0F) K	2.52/1/5211	1150 1529	1176	1,00	(200 / 150.0		-	
ISOKINETIC SAMPLE DATA FORM	ne Filter ID: PG	Schow, AK	ルクエアもつ Dato, rtess, (m. rtg): ており しんし (ロー / 3 Statio Press (in H.O): カンパ	0,(%):		Duct Dia, (in): 30	المجاري عند المجاري المجاري المجاري المجاري المجاري المجاري المجاري المجاري المجاري المجاري المجاري المجاري الم	1. 0 と フラ 4 Nozzle Dia. (in): ひ S 7 サ フ
	Plant: Poso Mine	Source I D		Flow Traverse Time:	Run No.: I S - 3	Operators:	Meter Box I.D.:	Meter Y:

in. H₂0/15 sec. in. H₂0/15 sec.

Static ٥

Impact 0

Pitot: Pre: Post:

in. Hg Vac. in. Hg Vac.

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acf acf

3.000

10.8747

Bws (assumed):
Nozzle Dia. (in):
K Factor:
Leak Check:
Pre:

Paris

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Meter Delta H@: Probe I.D./ Impinger outlet I.D.:

Probe Length/Type: Pitot Coeff. (Cp):

0.84

5/4,16 1.00334 1.7732

Vacuum	(m. Hg)	*		, v		1	1	1	4	٧,	^	5	ç	نہ	9		ه اد	2 1	3	٠ ن	s	o	O	,		7	7		8,	4		May Vac	IVIAN. Vac.
DGM Temp. (PF)		65	â	25	200	0,0	27	7,		\ ^	28	23	5.9	58	5.9	59	00	200	3	<u>ر</u>	2.2	63	63	64	59	59	27	2,2		12.5		M Temp	ATA A CAMP.
DGM Te		58	20	60	6.7	1,2	1		35			60	70	70	1/2	72	73	2	27.5	1,0		3)	76	76	76	26	16	77	12			Average DGM Temp	> ~ AGmun
Imp. Outlet Temp.	(F)	40	36	75	70	1,1	27	(2)	2077		9	1),	1/4	111	117	7,7	7/2	17		,,,,	t	1//	<i>}</i>	///	4/	42	42	6.2				
Filter Temp.	(1)	251	253	256	152	120	200	12.4	27.0	15,5		12	3	250	250	250	250	25.6	24%	200	365,6	200	250	250	251	253	222	250	251				
Probe Temp.	(F)	264	762	262	552	252	242	246	25.5	25.72	25.0	637	2.50	146	247	256	1-57	249	247	246	1	2 2 2	3 5 5	650	254	549	249	280	25.6				
Stack Temp. (F)		2511	1(8)	1167	1121	1125	1/56	27/1	1127	hhli	277	2,7,7	11 40	11.47	1157	1126	071)	1136	2411	1169	1,43		2 7	12/1	(130	11.42	1154	1165	このグ			Avg. ts	
ΔH (in. H_20)		\ \(\frac{1}{2}\)	1,58	1,60	163	1.66	1,63	271	(20)	79.1	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1		500	103	1165	1,66	1,63	1,63	(.63	93,1	5	1,2		((6)	, , ,	1,66	1:63	1,63	1.63			Avg. AH	
ΔP (in. H ₂ O)	\(\frac{1}{2}\)	75	0.01	10.01	0.01	0.01	0.01	100	0.01	0.01	20.0		3 6	12.5	100	0,0	50.0	0.01	0.0	100	10.0	3	, , ,		100	3	0.61	2070	0.01			Avg. VAP	
DGM Reading (DACF)	340 200	2001001	166.35	16-1, 51	766.57	765.71	770.87	773.02	02 1522		47 977	191 70	h-	76/163		Ч	240 00	197. 64	194, 51	797,08	ીવલ	77. 108	119 200	20,000	23, 62	2000	000	0/6:18	814,61	8.8,318		Vol. (DACF)	
Sample Time (min.)	()	1	e	2	7.7	15	18	21	h2	27	30	22	100	~ c		2,7	34	3,7	5,1	5.5	S		2 2 2		3 (c)] e	7,	715	\$0		Total Time	
Port/Point I.D.	,.	4	,	1	3	ځ/	c	,	مان	9	97);	12	3,	,	26		-	٨	9	Ĺ	仌	6				1						
DGM Clock Time	1501																													9291			

	Change	807.8 92			00.7 3.5	915.6 1.3	61.6
Moisture	Initial Final					907.5	
			•				Sum
S	28.4	0.04	0.8747	1.7732	1.0034	132	
Point Duration (min) =	Bar. Pres. $(in Hg) =$	Static Pres. (in WC) $=$	Nozzle Dia (in WC) =	Meter dH @ =	Meter Yd =	H2O Mass $(ml/g) =$	
SMMI - Pogo Mine	Delta Junction, AK	Incinerator	I5-3	10/01/13	1506-1626	80	
Plant =	Plant Location =	Source ID =	Run No =	Date =:	Run Time =	Sample Duration (min) =	

Point No.	DGM Reading	ading Sample Volume dP	Ð	dP1/2	Ħ	dH1/2	Stack T	DGM Inlet	DGM Outlet	DGM Ave	velocity	Stack Pres	Meter Pres
	(acf)	(acf)	(in WC)	(in WC)1/2	(in WC)	(in WC)1/2	(F)	(F)	(F)	(F)	(£/s)	(in Hg)	(in Hg)
													Ô
-	760.208	2.182	0.01	0.10	1.63	1.28	1142.0	58.0	59.0	58.5	10.1	28.40	28.52
2	762.390	2.120	0.01	0.10	1.58	1.26	1187.0	58.0	59.0	58.5	10.3	28.40	28.52
m	764.510	2.060	0.01	0.10	1.60	1.26	1167.0	0.09	58.0	59.0	10.2	28.40	28.52
4	766.570	2.140	0.01	0.10	1.63	1.28	1151.0	62.0	58.0	0.09	10.1	28.40	28.52
۶	768.710	2.160	0.01	0.10	1.66	1.29	1125.0	63.0	58.0	60.5	10.1	28.40	28.52
9	770.870	2.150	0.01	0.10	1.63	1.28	1150.0	65.0	57.0	61.0	10.1	28.40	28.52
7	773.020	2.180	0.01	0.10	1.63	1.28	1163.0	0.99	57.0	61.5	10.2	28.40	28.52
∞	775.200	2.180	0.01	0.10	1.66	1.29	1127.0	67.0	57.0	62.0	10.1	28.40	28.52
6	777.380	2.160	0.01	0.10	1.63	1.28	1144.0	0.89	58.0	63.0	10.1	28.40	28.52
10	779.540	2.160	0.01	0.10	1.66	1.29	1112.0	0.69	58.0	63.5	10.0	28.40	28.52
11	781.700	2.150	0.01	0.10	1.66	1.29	1120.0	70.0	58.0	64.0	10.0	28.40	28.52
12	783.850	2,160	0.01	0.10	1.63	1.28	1143.0	70.0	58.0	64.0	10.1	28.40	28.52
	786.010	2.190	0.01	0.10	1.63	1.28	1152.0	71.0	59.0	65.0	10.1	28.40	28.52
7	788.200	1.800	0.01	0.10	1.66	1.29	1126.0	72.0	59.0	65.5	10.1	.28.40	28.52
ю	790.000	2.420	0.01	0.10	1.63	1.28	1140.0	73.0	0.09	66.5	10.1	28.40	28.52
4	792.420	2.450	0.01	0.10	1.63	1.28	1136.0	73.0	61.0	67.0	10.1	28.40	28.52
ۍ	794.870	2.210	0.01	0.10	1.63	1.28	1142.0	74.0	61.0	67.5	10.1	28.40	28.52
•	797.080	2.180	0.01	0.10	1.60	1.26	1169.0	75.0	62.0	68.5	10.2	28.40	28.52
7	799.260	2.180	0.01	0.10	1.63	1.28	1153.0	76.0	63.0	69.5	10.1	28.40	28.52
∞	801.440	2.200	0.01	0.10	1.63	1.28	1140.0	76.0	63.0	69.5	10.1	28.40	28.52
6	803.640	2.200	0.01	0.10	1.63	1.28	1147.0	76.0	64.0	70.0	10.1	28.40	28.52
10	805.840	2.200	0.01	0.10	1.66	1.29	1130.0	76.0	64.0	70.0	10.1	28.40	28.52
11	808.040	2.190	0.01	0.10	1.60	1.26	1172.0	76.0	65.0	70.5	10.2	28.40	28.52
12	810.230	2.150	0.01	0.10	1.63	1.28	1154.0	76.0	64.0	70.0	10.1	28.40	28.52
	812.380	2.230	0.01	0.10	1.63	1.28	1165.0	77.0	65.0	71.0	10.2	28.40	28.52
	814.610	3.708	0.01	0.10	1.63	1.28	1155.0	77.0	65.0	71.0	10.2	28.40	28.52
	818.318									٠			
	58.110		0.01	0.10	1.63	1.28	1146.62	70.15	60.38	65.27	10.13	28.40	28.52

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ATCOM	Mointen	Jacuic Final	371.6	013.5	1	700.2	226				in 11 0/16	in. H ₂ 0/15 sec.		Vacuum (in. Hg)	ľ	1	70	16	Ş	\$	5	~	SI		ک و	3	9	9	9.	9	ل و	ال	9	0	6	9	9	9			Max. Vac.
# n		Initial	1	2587.7	3716.0	4 699.6	5918,6	Net Gain		Ctotic	Static			DGM Temp. (°F)	23	200	200	58	\$3	78	284	28	1 N	C (3)	الما الما	78	85	98	500	7,8	350	28	84	84.	2.00	30,7	SS	1,52			Average DGM Temp.
·		Imp						<u>د</u>		Tmnoct	o o			DGM	28	à	300	90	So	g	25	2 20	20	200	43	gu	۲,	٦ (ر ن	×1.	97	92	92	92	93	26	200	45	22			Average D
	7 (cas) (C	1	25 165.5	1150 162.5	(7)		1200 1240	225/185.8		Pitot-	Pre:	Post	Ľ	Temp.		52	45	777	47	47	47	χ 1	877	87.	4.9	55	717	7 6	577	077	77	49	hd	63	4%	20	20	7,			
¥	10		z 1 1	ž	1	;			ı	ı	in. Hg Vac.	in. Hg Vac.	Filter Temn	₽,	544	2h2	243	151	25.6	2.5	132	7537	772	252	251	25.2	250	252	25.0	248	152	283	251	25.1	152	052	250	0.52			
DATA FORN											0~	_	L	Temp.	243	9.52	258	257	552	52	252	120	250	152	256	252	252	43	200	75.7	25H	252	250) 52	157	777	14	2023			
KINETIC SAMPLE DATA FORM	P &	45	8.45	70				7			acf	acf		Stack Temp. (F)	5211	(187	1201	1197	9811	2	1261	277	120	(22!	1200	123/	128	767	1202	2121	4121	1225	1021	1021	1225	1521	707.	ב		Α χια. φ	Avg. k
ISOKINET			2	0	1	4.5		7780			00000	0000	ΗV	(in. H ₂ 0)	1,66	1,58	३८१	35h	1,557	SC: 1	775 7	100	(. ٢٤	1.56	1.58	1,56	1,58	351	1.58	35')	1.58	1,5%	1.58	1.58	1.56	2000	33.	27.		A vice ALI	Avg. dai
	Filter ID:	Ambient Temp. (P:	Baro. Press. (in. Hg):	Static Press. (in H,O):	0,(%):	CO ₂ (%):	B (assumed):	Nozzle Dia. (in):	K Factor:	Leak Check:	Pre:	Post:	ď∇	(in. H ₂ O)	Ø, O.(100	10,0	100	960	10.0	0.0	20,0	9,00	Ġ.0i	10,0	0.0	0000	10.0	10.0	0.01	0.01	0.00	2.0	0,0	0.0	3 0	300			DAL ALLA	AVB- VAI
		17 AC	•								15.	4	DGM Reading	(DACF)	851,856	1000.37	1002.41	1004.63	6.28	12.0	10.24 15 17	20 77	16,70	18.80	20,02	29,65	25,16	20.47	31,57	33,68	35.77	37,92	40.04	42.45	74,4	25.001	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	53.755		Vol (DACE)	
	Mire	1th Sunction	3	51-2-01	£ 2.7	411	15 Co. 17	1,00339	1.7732	463	41 ,2m5	P. S. C	Sample Time	(min.)	ଚ	3	٩	5	7.1	0/	, ,	24	7.2	30	33	35	۲,	34	87	5,	Şçj	S:1	000	3	39	- 27	75	٦٥		Total Time	
;	Pago M	200	(NC.		(-	1				ger outlet I.D.:	ne:		014	FOLUT OILL L.D.	_	2	_	7	1	٦	ck	T	3)	jį	72	-	7,0	1	٧	ف	-	ماد	3-12	3)	- 2	2					
	Plant:	Location:	Source I.D.:	Date:	Rim No.	Operators:	Meter Box I.D.:	Meter Y:	Meter Delta H@	Probe I.D./ Impinger outlet I.D.	Probe Length/Type:	Pitot Coeff. (Cp):	DGM Clock	Time	1510																							16291	•		

_		_	_			_	_		_		_		_		-											_				
Meter Pres.	(in Hg)		28.57	28.57	28.57	28.57	28.57	28.57	28.56	28.56	28.56	28.56	28.56	28.57	28.56	28.57	28.57	28.57	28.57	28.57	28.57	28.56	28.57	28.57	28.56	28.56	28.57	28.57		28.57
Stack Pres	(in Hg)		28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45		28.45
velocity	(ft/s)		10.0	10.2	10.3	10.3	10.2	10.3	10.4	10.4	10.2	10.3	10.4	10.3	10.4	10.3	10.3	10.3	10.3	10.3	10.3	10.4	10.3	10.3	10.4	10.4	10.3	10.3		10.30
DGM Ave	(F)		83.0	85.0	85.5	86.5	86.5	87.5	88.0	89.0	89.0	89.0	0.06	89.0	90.0	89.5	90.0	0.68	88.0	88.0	88.0	88.0	88.0	88.5	88.0	88.5	89.0	89.5		88.08
DGM Outlet	(F)		83.0	84.0	83.0	83.0	83.0	84.0	84.0	85.0	85.0	85.0	86.0	85.0	86.0	85.0	86.0	85.0	84.0	84.0	84.0	84.0	84.0	84.0	84.0	84.0	85.0	85.0		84.38
DGM Inlet	(F)		83.0	86.0	88.0	0.06	90.0	91.0	92.0	93.0	93.0	93.0	94.0	93.0	94.0	94.0	94.0	93.0	92.0	92.0	92.0	92.0	92.0	93.0	92.0	93.0	93.0	94.0		91.77
Stack T	(F)		1125.0	1187.0	1201.0	1197.0	1186.0	1199.0	1248.0	1236.0	1189.0	1206.0	1227.0	1200.0	1231.0	1209.0	1205.0	1195.0	1202.0	1212.0	1214.0	1225.0	1201.0	1207.0	1225.0	1241.0	1204.0	1190.0		1206.23
dH1/2	(in WC)1/2		1.26	1.26	1.26	1.26	1.26	1.26	1.24	1.24	1.24	1.24	1.25	1.26	1.25	1.26	1.26	1.26	1.26	1.26	1.26	1.25	1.26	1.26	1.25	1.24	1.26	1.26		1.25
HP	(in WC)		1.60	1.58	1.58	1.58	1.58	1.58	1.54	1.54	1.54	1.54	1.56	1.58	1.56	1.58	1.58	1.58	1.58	1.58	1.58	1.56	1.58	1.58	1.56	1.54	1.58	1.58		1.57
dP1/2	(in WC)1/2		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10		0.10
Q	(in WC)		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.01
Sample Volume	(acf)		2.172	2.040	2.220	1.650	2.010	2.080	2.080	2.130	2.120	2.100	2.120	2.130	2.110	2.110	2.150	2.150	2.110	2.090	2.150	2.150	2.180	2.180	2.160	2.150	2.150	2.865		
DGM Reading	(acf)		998.198	1000.370	1002.410	1004.630	1006.280	1008.290	1010.370	1012.450	1014.580	1016.700	1018.800	1020.920	1023.050	1025.160	1027.270	1029.420	1031.570	1033.680	1035.770	1037.920	1040.070	1042.250	1044.430	1046.590	1048.740	1050.890	001.0001	55.557
Point No.			-	7	es.	4	'n	9	7	∞	6	10	11	12	Ĥ	7	m	4	S	9	7	∞	δ	10	11	12				

FORM
APLE DATA
ETIC SAN
ISOKINE

					ISOKINET	KINETIC SAMPLE DATA FORM	DATA FORM			•	•	AIICOM
Plant	000			Filter ID:		44 DK-		# cert	1/856-003		blacil box	erikiya d
Location: Source I D	Velta Yun	action AK		Ambient Temp. (P): Baro Press (in Hg).				: .		Imp.	Initial	Mosture Final
Date:	10000000000000000000000000000000000000	0-75-12		Static Press (in H.O):		20.05		1		(8.162
Flow Traverse Time:		4. 4.		O ₂ (%):		20.7		ı		7 6	351.2	542,0
Run No.:	1 23	7		CO, (%):						9.4		207.0
Operators:	<i>৯</i> ০	34		Duct Dia. (in):	(7)	3011				5	.l	624.5
Meter Box I.D.:		36216		Bws (assumed):	7 60	7		i I		973.0		930.5
Meter Delta H@.		757 (20.1		Nozzle Dia. (m):	0.8/8.0	818	874 : 0.3	5/47				
Probe I D / Impinger outlet I D :	ger outlet I D .	11.15		I eat Check-				ı	i			
Probe Length/Type:	De: 4.D	103			7000	ju	5.07	in He Vec	Pitot:	Impact	Static	
Pitot Coeff. (Cp):		0.84			0.003	act	3 5	in. Hg Vac.	Post:	9	0	in. H ₂ 0/15 sec. in. H ₂ 0/15 sec.
							Probe	- 1	Imn Outlet			
DGM Clock Time	Port/Point I.D.	Sample Time (min.)	DGM Reading (DACF)	ΔP (in. H ₂ O)	ΔΗ (in. H ₂ 0)	Stack Temp. (F)	-	Filter Temp.		DGM Te	DGM Temp. (F)	Vacuum (in, Hg)
271		0	243, 443	0.01	1,66	5211	246	852	7 F	Ø	0.3	, n
	7	5	247, 11	10.0	1.6.6	0211	552	255	37	300	5.5	7
	3	01	'	0.01	1.66	1124	255	255	3.7	ě	2.2	1
	2	4	254.13	0.01	1.06	103	7.51		88	62	\$5	<u>ئ</u>
	7	200	251.20	3 6	1.66	1,777	157	252	39	53	55	Į,
	٥	25	760 25	2 3	3-1-1	5011	25.1	1221	XZ.	77	26	ا
	3	200	7 6 6 7	12.0	X (1)	1,7	152	7.50	07	59	5,6	\ <u>\</u>
	,5	7/0	272.7		777	1211	200	700	2,7,7	59	3/0	<u>ر</u>
	01	5/2	275.89	0	29 1	073	1,12	252	7.7	ا ئ ر) c	-0
	-1	50	279.78	! ດ : ລ	(۶۹۰	1139	257	250	77	90	ار ال	00
	12	\$\$	283 24	o.o.	1.63	1139	249	250	42	1.9	<\$	° Съ
		700	286,98	0.0	1.63	1147	232	152	1h	1.9	23	5 5
	36	100	2942	14.0	1.6.5	15.77	25%	137	27	950	58	Œ
	7 7	27	29.7.62	13.0	27 1	2011	1130	25.5	7.5	20	200	70/
	5	80	301,42	0.01	1,66	1130	249	202	43	6.5	24	NO CO
	7	85	305.11	0.01	1.63	5411	752	256	43	70	60	300
	-	90	308.00	0. 0(1.63	1156	rigg	252	43	70	60	ò
	× 0	95	316.58	10.0	1.63	1155	342	244	43	72	Ìψ	ઈઉ
	-	201	£1, \$1, \$1, \$1, \$1, \$1, \$1, \$1, \$1, \$1, \$	0.0	1165	¢ \$1.1	250	250	43	43	62	6
	10	105	317161	200	1,4,5	75.1	757	257	43	73	63	3-10
	- 1	0/1	326.95	13.0	\ عار ا	٠ <u>٠</u> ٠ ٠ ٠ ٠	25.50	25.0	ر ۲	7.5	5 %	٠
	3,	120	2.00.1.1	300	\$ 0 12 6 7 7		25.0	157	25	27.5	6.3	5
		120	של הרג	0.0	291	477	27.7	200	~\2 7 7	7,5	7.0	ù-0
1979		161	7 35 72 6				25.2			1,0	6.4	
-												
		Total Time	Vol (DACE)	Avie alAD	Πγ ~γ	+ 200 V					4,5	;
		ama timot		74VB- V24	AV8. OII	\$1 -5447,				Average DOM 1emp.	JIM Temp.	Max. Vac.

	Final Change	291.8 13.6	542.0 190.8		207 9 0.5	624.5 2.2
	5	28.05	0.04	0.8747	1.7732	1.0034
5 28.05 0.04 0.8747 1.7732	nin) =	= (/C)=	/C)=		
	Point Duration (1	Bar. Pres. (in Hg.	Static Pres. (in W	Nozzle Dia (in W	Meter dH @=	Meter Yd =
(min) = (g) = WC) = WC) =						
(min) = (g) = WC) = WC) =	Viine	AK				
Point Duration (min) = Bar. Pres. (in Hg) = Static Pres. (in WC) = Nozzle Dia (in WC) = Meter dH @ =	SMMI - Pogo l	Delta Junction,	Incinerator	123-1	09/29/13	1722-1929
Point Duration (min) = ction, AK Bar. Pres. (in Hg) = Static Pres. (in WC) = Nozzle Dia (in WC) = Meter dH @ =						
Point Duration (min) = ction, AK Bar. Pres. (in Hg) = Static Pres. (in WC) = Nozzle Dia (in WC) = Meter dH @ =	Plant =	Plant Location =	Source ID =	Run No =	Date =	Run Time =
SMMI - Pogo Mine Point Duration (min) = Delta Junction, AK Bar. Pres. (in Hg) = Incinerator Static Pres. (in WC) = 123-1 Nozzle Dia (in WC) = 09/29/13 Meter dH @ =						

DGM Reading Samp (acf)	Sample Volume (acf)	dP (in WC)	dP1/2 (in WC)1/2	dH (in WC)	dH1/2	Stack T	DGM Inlet	DGM Outlet	DGM Ave	velocity	Stack Pres	Meter Pres.
	11				217(2) 1117		الله		(+)	(601)	(gr m)	(gram)
3.637		0.01	0.10	1.66	1.29	1125	56.0	54.0	55.0	10.1	28.05	28.17
3.620		0.01	0.10	1.66	1.29	1120	58.0	55.0	56.5	10.1	28.05	28.17
3.400		0.01	0.10	1.66	1.29	1124	61.0	55.0	58.0	10.1	28.05	28.17
3.570		0.01	0.10	1.66	1.29	1104	62.0	55.0	58.5	10.1	28.05	28.17
3.650		0.01	0.10	1.66	1.29	1115	63.0	55.0	59.0	10.1	28.05	28.17
3.640		0.01	0.10	1.66	1.29	1109	64.0	56.0	0.09	10.1	28.05	28.17
3.610		0.01	0.10	1.63	1.28	1147	65.0	26.0	60.5	10.2	28.05	28.17
3.610		0.01	0.10	1.63	1.28	1142	65.0	56.0	60.5	10.2	28.05	28.17
3.680		0.01	0.10	1.66	1.29	1131	0.99	56.0	61.0	10.2	28.05	28.17
3.890		0.01	0.10	1.63	1.28	1140	0.99	57.0	61.5	10.2	28.05	28.17
3.460		0.01	0.10	1.63	1.28	1139	0.99	57.0	61.5	10.2	28.05	28.17
3.640		0.01	0.10	1.63	1.28	1139	67.0	57.0	62.0	10.2	28.05	28.17
3.630		0.01	0.10	1.63	1.28	1147	67.0	57.0	62.0	10.2	28.05	28.17
3.630		0.01	0.10	1.63	1.28	1131	0.89	58.0	63.0	10.2	28.05	28.17
3.660		0.01	0.10	1.63	1.28	1140	68.0	58.0	63.0	10.2	28.05	28.17
3.670		0.01	0.10	1.60	1.26	1125	0.69	59.0	64.0	10.1	28.05	28.17
3.640		0.01	0.10	1.66	1.29	1130	0.69	59.0	64.0	10.1	28.05	28.17
3.630		0.01	0.10	1.63	1.28	1145	70.07	0.09	65.0	10.2	28.05	28.17
3.640		0.01	0.10	1.63	1.27	1156	70.0	0.09	65.0	10.2	28.05	28.17
3.610		0.01	0.10	1.63	1.28	1155	72.0	61.0	66.5	10.2	28.05	28.17
3.620		0.01	0.10	1.63	1.28	1157	73.0	62.0	67.5	10.2	28.05	28.17
3.660		0.01	0.10	1.63	1.28	1141	73.0	63.0	0.89	10.2	28.05	28.17
3.680		0.01	0.10	1.63	1.28	1143	73.0	63.0	0.89	10.2	28.05	28.17
3.660		0.01	0.10	1.63	1.28	1146	73.0	63.0	0.89	10.2	28.05	28.17
3.650		0.01	0.10	1.63	1.28	1161	72.0	64.0	0.89	10.2	28.05	28.17
1.465		0.01	0.10	1.63	1.28	1147	72.0	64.0	0.89	10.2	28.05	28.17
		0.01	0.10	1.64	1.28	1136.9	67.23	58.46	62.85	10.17	28.05	28.17

					ISOKINE	ISOKINETIC SAMPLE DATA RORM	DATA FOR	•		7/2		
Dient	c							<u>.</u>		, o , o	black	
rianc.	7 260	30 WINE		Filter ID:		2/6.2			1120 10	じいづ		Moietura
Course I D .	128174	المناحل المناز		Ambient Tenn. (Pr.		26 St.		ļ	11 50	60.4 Inn.	Initial	Lino
Dole:	35	INCINAVA Par		Baro. Press. (in. Hg):	12	8.20		ı		. c	\$ 20	CA 20 CA
Flow Traverse Time		7 - 30 - (3		Static Press. (in H,O):	0);2		1 !)) ()	3<2 <	525
Run No.		T 23 - 2		0,(%):					1225 1	55.6	3700.9	255
Operators:	4	P 2		Duct Dia (fn):	6			1	_	•	1	705.7
Meter Box I.D.:		Sixil		B (assumed):				i			5620.1	
Meter Y:		1.00339	7	Nozzle Dia. (in):	6	11 L		1			92. SNet Gain	1 943.5
Meter Delta H@		1,773	7	K Factor:				<i>;</i>				
Probe 1.D./ Impinger outlet 1.D.	r outlet I.D.	н		Leak Check:				1.	Pitot.	Import	0.000	
Probe Length/Type:		イ・ でかく		Pre:	00.00	acf	jo	in. Hg Vac.	Pre:	mpact	Static	
Filot Coeff. (Cp.):		0.54	-	Post:	0.00	acf	0/	in. Hg Vac.	Post:	9	0	in. H ₂ 0/15 sec.
DGM Clock	Port/Point I.D.	Sample Time	DGM Reading		НΩ	£ 1000		Filter Temp.	H			1
Lime		ر آ	(DACF)	(in. H ₂ O)	(in. H ₂ 0)	stack temp. (F)	Lemp.	E E	Temp.	DGMT	DGM Temp. (F)	vacuum (in. Hg)
7.2.3	-	చ	336.315	0,01	1.66	1100	251	25.1	42	3	711	
	7		339.67	0.0	1,66	(1.05	255	255	1-6	1.77	577	٥,
	\		343.37	0.0	1.66	11.11	250	252	38	2.3	r c	3
	7		346 94	000	1.66	1416	253	252	38	5.2	42	3
	4.	07	1505	7000	99	123	252	275	7,	25	7.7	3 0
		12	207 60		7.67	130	244	252	Ĭ,	95	ħħ	0
	ţ)n	35	2,1,09	700	20,7	1168	750	222	75	28	55	2
	8	250	3.4.67		2, 1, 1,	27.5	2.50	650	24	\$9	240	7
	11	75	368,25	0 0	163	2611	246	200	\$ h	00,	47	1
	ij	30	1371. 85	0.01	1.63	(138	122	244	120	6/	48	+
	7	35	. 1	0.01	1.66	1131	250	25/	5,7	100	7.60	+
		23	379,10	10.0	1, 46	1122	152	250	34	7.7	5	1
	2 ~	(a)	386, 71	0 0	1.63	3411	142	250	47.	63	13	7
	,	27	350 41	100	757	11.84	244	248	45	(, y	1.5	
	2	5.5	39201	3,0	2,7	1611	21.70	057	27	7.7	52	u
	9	58	397.12	9.Ci	1.66	(120	251	75,		65	53	00
	۲	90	מכני זמ	001	1,63	1146	249	2.57	777	2 .	74	200
	√····	75		0.01	1,63	1144	245	252	27	67	1	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
	5-	29)	71	00:	1,63	1165	250	25.2	46	000	77	O C
	٥		25 11	001	1.63	1164	251	052	9%	600	57	00
	-	017	1,2,7,7	0.01	1.63	25//	249	251	45	00	57	e 2x
	1		\$ 200 C	9	ر. وع	1/54	250	249	Ch	89	58	200
		T	1.20.11	0.01	39.7	11.357	250	250	40	66	5.5	0.
1135		127	452, 2007	2	١ , 66	((23	257	250	46	69	ટર	00
		Total Time	Vol (CA)	4,1								
		TOTAL THREE	voi: (Dater)	Avg. VAF	Avg. AH	Avg. t _s				Average DGM Temp.	iM Temp.	Max. Vac.
	1								_			

	Change	10.9	182.6	0		6.7	13	Meter Pres.	(in Hg)	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32	28.32		0000	28.32
ච	Final	339,4	535.1	700.9	705.7	626.8	943.5	Stack Pres		28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20	28.20		00 00	28.20
Moisture	Initial	328.5	352.5	700.9	704.7	620.1	930.5	velocity	ı	10.0	10.0	10.1	10.1	10.1	10.2	10.1	10.2	10.1	10.2	10.1	10.1	10.1	10.2	10.2	10.2	10.1	10.2	10.2	10.2	10.2	10.2	10.2	10.1	10.1	5.4		000	9.96
								DGM Ave	(F)	41.5	43.5	46.5	48.5	49.5	50.0	51.5	52.5	53.5	54.5	55.5	55.5	56.5	57.0	57.5	58.0	59.0	0.09	60.5	61.0	62.0	62.5	62.5	63.0	63.0	64.0		25 70	55.73
								DGM Outlet	(F)	43.0	40.0	41.0	42.0	43.0	0.44	45.0	46.0	47.0	48.0	49.0	49.0	50.0	51.0	51.0	52.0	53.0	54.0	55.0	55.0	56.0	57.0	57.0	58.0	58.0	59.0		50.40	20.1Z
ν.	28.2	0.04	0.875	1.7732	1.0034	214.2		DGM Inlet	(F)	40.0	47.0	52.0	55.0	26.0	56.0	58.0	59.0	0.09	61.0	62.0	62.0	63.0	63.0	64.0	64.0	65.0	0.99	0.99	67.0	0.89	0.89	0.89	0.89	68.0	0.69		64.05	01.00
=(•	l1	lł.					Stack T	(F)	1100.0	1105.0	1111.0	1110.0	1127.0	1145.0	1128.0	1146.0	1137.0	1142.0	1138.0	1131.0	1122.0	1146.0	1139.0	1141.0	1154.0	1120.0	1149.0	1144.0	1165.0	1164.0	1152.0	1159.0	1134.0	1123.0		112E BE	1133.03
Point Duration (min)	Bar. Pres. (in Hg) =	Static Pres. (in WC)	Nozzle Dia (in WC) =	Meter dH @=	Meter Yd =	H2O Mass (ml/g) =		dH1/2	(in WC)1/2	1.29	1.29	1.29	1.29	1.29	1.28	1.29	1.28	1.28	1.28	1.28	1.29	1.29	1.28	1.28	1.28	1.28	1.29	1.28	1.28	1.28	1.28	1.28	1.28	1.29	1.29		1 28	07.1
Poi	Ba	Sta	Š.	Me	Me	H		Η̈́P	(in WC)	1.66	1.66	1.66	1.66	1.66	1.63	1.66	1.63	1.63	1.63	1.63	1.66	1.66	1.63	1.63	1.63	1.63	1.66	1.63	1.63	1.63	1.63	1.63	1.63	1.66	1.66		1 64	c .
ne	¥							₽1/2	(in WC)1/2	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.100	0.100		040	2
SMMI - Pogo Mine	Delta Junction, AK	Incinerator	123-2	09/30/13	0923-1130	127		Ð	(in WC)	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010		0.04	- 2
<i>δ</i> 3	ı	Я	1	0		in) =		Sample Volume	(acf)	3.555	3.500	3.570	3.570	3.530	3.510	3.540	3.580	3.580	3.600	3.670	3.580	3.610	13.570	-6.370	3.600	3.610	3.620	3.590	3.590	3.590	3.600	3.560	3.550	3.550	1.434			
Plant =	Plant Location =	Source ID =	Kun No =	Date =:	Run Time =	Sample Duration (min) =		DGM Reading	(acf)	336.315	339.870	343.370	346.940	350.510	354.040	357.550	361.090	364.670	368.250	371.850	375.520	379.100	382.710	396.280	389.910	393.510	397.120	400.740	404.330	407.920	411.510	415.110	418.670	422.220	425.770	427.204	688 06	700,00
P	Į,	Ĭ.	⊻ 1	a 1	Α.	ĸ		Point No.			2	٣	4	٧.	9	7	∞.	6	10	11	12		7	m	4	۰	9	7	∞	6	10	11	12					

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AECOM	Moisture	Final	342,5	535,+	7,101	626.5	972.5				in. H ₂ 0/15 sec. in. H ₂ 0/15 sec.	1,000,000	(in. Hg)	9	9	8	ڻ	3	او	9				7	7		1	7	7	7	, + '		Ţ	-	1				Max. Vac.	
sjack .		Initial	529	2 254.5	4 700.6	5 626,0	10			Static	0		DGM Temp. (°F)	58	58	2.5	87	57	ا ا ا), 0° ∧ ∨	5-5	55	00)	60	67	6.0	27	2.0	63	6.3	63	< 9 9	70,	79	250				GM Temp.	
<u> </u>	5:59)	ĮĮ.		3		•			,	Impact	0		DGMI	57	- 59	29	759	65	1-3	50	10	70	J_{ℓ}	31	7.2	(4)	72	12	72	72	77.7	77.6	11,	77.	カレ				Average DGM Temp.	
1(3.5)	1/252/1	155	1 2211						, i	Pitot:	Post:	F	Temp.	43	39	3,5	3.5	38	2,2	272	38	33	35	40	7	47	77	. 76 (15	1,1	70	77	25:	ch	27,					-
ī	ı		1	ı	ı	1 1	ı	ı		in Ha Vac	in. Hg Vac.	Filter Temp.	£.	235	238	752	258	255	252	157	250	250	252	222	152 /	250	249	251	250	247	3000	200	250	0\$2	252					
ISOKINETIC SAMPLE DATA FORM										Ş	90		1emp.	L52	259	251	252	756	244	542	157	245	248	257	25.5	250	255	247	248	25.5	9(3)	247	261	157	247					
C SAMPLE	3	77.0	2							acf	acf	E -	Stack 1emp. (F)	6111	1185	1143	1159	25/1	2511	(173	1135	S A 13	1173	11.5%	17.03	59))	1185-	1911	1186	1173		1172	1149	1195	1193				Avg. t _s	
ISOKINETI	2/6	1				30 "	İ	0.8747			6.00	HV	(in. H ₂ 0)	1.66	1.60	1,63	(60)	1.65	1.63	4,66	1.6.6	1.63	1,40	(1,6,7	3 2	(63)	1,63	(.63	(,60	(1,63		(S) i	1,63	1,58	1.53	,			Avg. AH	
	Filter ID:	Ambient Temp. (*F): Raro Press (in Hg):	Static Press (in H.O)	O ₂ (%):	CO, (%):	Duct Dia. (in):	Bwe (assumed):	Nozzle Dia. (in):	I eak Check			ď∇	(in. H ₂ O)	0.0	0.01) () () ()	3	0.0 1	0.0	10.0	10.0	0.01		10:0) (c	0.0 (0.01	0,0	ร์ง	5.65	12:0	\$ 0.0	0,01	5.01	0 01				Avg. VAP	
	111	M K								\ \		DGM Reading	(DACF)	914679	675.67	6/6, (7	10000	F 7 289	6,99, 69	693 22	69 6 8	100.51	207, 60	30,00	27:50	718,34		125. 20	752.45	12/ 72	7 36 74	744 00	トレルカト	151.40	71.55.	758,9,2			Vol. (DACF)	
	2 -	7020102	(0-1-6)	lí		00 m	15/4cK	1,000,597	7677	41 Pens	0.84	Sample Time	(min.)	S		200	\$ 6	25	30	35	20	33	05	55	34	70	75	200	X G	30		1			c				Total Time	1
,	9200	14) SV			' 1	9			ver ouflet I D :	ie:		Port/Point I D	t Other Cant a.D.	7	1	^		(,	7	c)so	5	9/)	17	2	3	'n	γ.	9 [4	01	1)	ځ)				1		1
	Plant: Location:	Source I.D.:	Date:	Flow Traverse Time:	Run No.:	Operators:	Meter Box 1.D.:	Meter 1:	Probe I.D./ Imnin	Probe Length/Type:	Pitot Coeff. (Cp):	DGM Clock	Time	1159																						140 °C				

			13.4	180.8	-0.4	-0.4	-0.3	0.5	×			-										-									_	_				ī	
		Change		18	7	Т	٦	- ;	Meter Pres	(in Hg)		78.52	26.02	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52		28.52
	sture	Final	342.5	535.7	701.2	705.4	626.5	933.5	Stack Pres	(in Hg)		28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40		28.40
	Moisture	Initial	329.1	354.9	701.6	705.7	626	915.4	velocity	(ft/s)		10.0	10.1	10.2	10.2	10.1	10.2	10.2	10.1	10.1	10.2	10.1	10.1	10.3	10.2	10.3	10.2	10.3	10.2	10.2	10.2	10.2	10.1	10.3	10.3		10.19
									DGM Ave	(F)	3 63	5.70 5.85	59.5	60.5	61.0	62.5	62.5	63.5	64.5	64.5	65.5	65.5	67.0	67.0	67.0	67.0	67.0	67.5	67.5	0.89	0.89	0.69	69.5	69.5	69.5		65.16
									DGM Outlet	(F)	0	28.0	57.0	57.0	57.0	58.0	58.0	58.0	59.0	59.0	0.09	0.09	62.0	62.0	62.0	62.0	62.0	63.0	63.0	63.0	63.0	64.0	65.0	65.0	65.0		60.80
	8	28.4	0.04	0.875	1.7732	1.0034	212.1		DGM Inlet	(F)	0.42	50.0	62.0	64.0	65.0	67.0	67.0	0.69	70.0	70.0	71.0	71.0	72.0	72.0	72.0	72.0	72.0	72.0	72.0	73.0	73.0	74.0	74.0	74.0	74.0		69.52
·	nin) ==	=	(C) =	(C) =			11		Stack T	(F)	11140	1185.0	1143.0	1159.0	1160.0	1137.0	1157.0	1173.0	1135.0	1140.0	1173.0	1141.0	1140.0	1183.0	1164.0	1185.0	1161.0	1186.0	1173.0	1171.0	1177.0	1173.0	1149.0	1195.0	1193.0		1162.68
	Point Duration (min) =	Bar. Pres. (in Hg) =	Static Pres. (in WC)	Nozzle Dia (in WC) =	Meter dH @ =	Meter Yd =	H2O Mass (ml/g) =		dH1/2	(in WC)1/2	1 20	1.26	1.28	1.28	1.28	1.28	1.28	1.26	1.29	1.28	1.26	1.28	1.28	1.26	1.28	1.26	1.28	1.20	1.28	1.28	1.26	1.26	1.28	1.26	1.26		1.27
									Ħ	(in WC)	1 66	1.60	1.63	1.63	1.63	1.63	1.63	1.60	1.66	1.63	1.60	1.63	1.63	1.60	1.63	1.60	1.63	1.60	1.63	1.63	1.60	1.60	1.63	1.58	1.58		1.62
·	Mine	AK							dP1/2	(in WC)1/2	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10		0.10
	SMMI - Pogo Mine	Delta Junction, AK	Incinerator	123-3	10/01/13	1159-1406	127		ф	(in WC)	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010		0.010
							nin) =		Sample Volume	(acf)	3.554	3.450	3.280	3.240	3.230	3.220	3.530	3.630	3.660	3.650	3.700	3.500	3.620	3.360	3.810	3.650	3.030	2.710	5.380	3.670	3.700	3.680	3.630	3.720	4.792		
	Plant =	Plant Location =	Source IID =	Kun No =	Date =	Run Time =	Sample Duration (min) =		DGM Reading	(acf)	669.716	673.270	676.720	000'089	683.240	686.470	069.689	693.220	696.850	700.510	704.160	707.860	711.360	714.980	718.340	725.150	729.430	722 140	727.140	746.720	740.390	744.090	747.770	751.400	755.120 759.912	70100	90.196
									Point No.		Н	2	en .	4	٠,	٥	7	∞	o :	10	11	17	- '	7 7	n -	1 4	י ר	> 1	\ c	۰ ۵	ν ;	O ;	Ι :	12			

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AICOM	Moisture	Final	347.2	561.8	2	100	200				n. H ₂ 0/15 sec. in. H ₂ 0/15 sec.	;	(in. Hg)	7	ر	9	9	6	2	ی	Ç	9	,9	7		8		-		1	7	7	F	ŗ				Max. Vac.	
, 5 Jacie		Initial	33541	2 353. 1	201 6	5 /27/ 8	22.00	mo 1017 0:201		Static			DGM Temp. (°F)	58	55	\$5	5.6	57	7,7	630	©S.	67	53	02	100	12.2	75	25	ا آ	265	0X)	77	LL	50¢	75			Average DGM Temp.	
	أد	Imp	7.5	5.2	۲۰۰	رى ئى ئ	Ů.	?		Impact	٥		DGMT	5,5	5.8	9	64		20	10	પ્ર	2	Ω,	783	700	T t	% T	, <u>1</u> , <u>1</u> , <u>1</u> , <u>1</u> , <u>1</u> , <u>1</u> , <u>1</u> , <u>1</u>	\Q \Q \Q	550	0	85	58	J (98			Average D	
,	T(c;)		1125 16	1180 116	1175 16	1200 1.5	7	,	i	Pitot: Pee:	Post:		Temp.	43	40	40	77	7.5	727	hh	5 <i>h</i>	9)	46	9),	77	48	ત્લ	So	100	5,1	52	53	54	56	3 \$				
									•	in Ua Voo	in. Hg Vac.	Filter Temn	£	272	カカマ	255	75.2	156	254	152	1.52	152	752	250	226	251	052	357	7.52	249	252	282	22.5	25.1	5,42				•
OATA FORM											2 80	Probe	Temp.	5.52	264	25°	227	255	252	253	252	157	747	567.	252	248	546	252	7 50	952	354	252	247	h \$ 7	7 57				
KINETIC SAMPLE DATA FORM	DEU		. 5.							عرو	act		Stack Temp. (F)	5511	12.15	8221	777)	1216	1521	1238	2/2!	75 21	242	16.55	84.	1245	(229	7171	17.10	1216	1249	<u>L) 21</u>	1506	1218	7 7 7 7			Avg. ts	
ISOKINETI			`	15U. C. C.		30	ic	6.8747		1.80	0000	ΥV	(in. H_20)	1.63	i, SS	1.5%	1200	5 U	1.56	1 ,56	(.58	1.56	1,56	\$ C >	200	1.54	1.58	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	200	1.58	15,7299	1,58	1,58	1.36	9 6 1			Avg. AH	
	Filter ID:	Ambient Temp. (PF):	Baro. Press. (in. Hg):	O. (%):	CO, (%):	Duct Dia. (in):	B _{ws} (assumed):	Nozzle Dia. (in):	K Factor:	Pre:	••	ΔP	(in. H ₂ O)	0.01	0.01	0.01	0.0	10.0	0.0	0.01	0.01	0.01	0000	3 3	0.0	0.01	10.0	0.0	6.01	0.01		0.0	0.01	00	0,0			Avg. VAP	
		AK										DGM Reading	(DACF)		95,36	25,315	31,710	926.25	429.77	433.26			445.92	456.00	954.60	11	ч	0000000			979.41	982 al	956, 35	260 36	29× 602	2000		Vol. (DACF)	
	Mine	wachin.	Incirco co to		23-4	OB, 2W	819016	3.36	25.5	200	5.34	Sample Time	(min.)	0	٧,			25.5			40		20			30	Ï					ilk	(10		120			Total Time	
	3		<u>z</u>		44			1.00336	C Language	e: 4/			rorvroint L.D.	_/	7	7	b	ق و	٦.	Š	5	શ		2	. 7	3	7	Y	3	מני	Ь	02	= 2	7					. l
	Plant:	Location:	Source 1.D.:	Flow Traverse Time:	Run No.:	Operators:	Meter Box I.D.:	Meter Y:	Probe I D / Impinger curlet I D :	Probe Length/Type:	Pitot Coeff. (Cp):	DGM Clock	Time	1157																					1001				

	ge	12.1	208.7	-0.5	-0.5	0.2	0.8	22.9	Meter Pres.	(in Hg)	,	28.57	28.57	28.56	28.56	28.56	28.56	28.56	28.56	28.57	28.56	28.56	28.56	28.56	28.56	28.56	28.57	28.57	28.56	28.57	28.57	28.56	28.57	28.57	28.56	28.56	11	28.57
	Change	347.2	561.8	702.1	6.707	627.7	951.7																															
Moisture	Final	æ	5	7	7	9	6		Stack Pres	(in Hg)		28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	00	28.45
Moi	Initial	335.1	353.1	702.6	7.707	626.9	928.8		velocity	(ft/s)		10.2	10.3	10.4	10.4	10.4	10.4	10.4	10.4	10.3	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.3	10.4	10.3	10.3	10.4	10.3	10.3	10.4	10.4	40.04	10.37
									DGM Ave	(F)	1	0.00	56.5	58.0	0.09	62.0	65.0	66.5	69.5	71.5	73.5	75.0	75.5	76.5	78.0	79.0	79.5	79.5	80.5	80.5	82.0	82.0	81.0	81.0	82.0	82.5	72 20	/3.28
									DGM Outlet	(F)	1	25.0	55.0	55.0	26.0	57.0	59.0	0.09	63.0	65.0	67.0	0.69	70.0	71.0	73.0	74.0	75.0	75.0	76.0	76.0	78.0	78.0	77.0	77.0	78.0	79.0	68 70	58.72
5	28.45	0.04	0.875	1.7732	1.0034	244.2			DGM Inlet	(F)	c u	55.0	58.0	61.0	64.0	0.79	71.0	73.0	76.0	78.0	0.08	81.0	81.0	82.0	83.0	84.0	84.0	84.0	85.0	85.0	86.0	86.0	85.0	85.0	86.0	86.0	77 94	77.84
in) =	II	=()=	= ()			II			Stack T	(F)	0.3211	1133.0	1215.0	1228.0	1224.0	1223.0	1218.0	1231.0	1238.0	1212.0	1236.0	1242.0	1235.0	1225.0	1248.0	1245.0	1229.0	1214.0	1239.0	1210.0	1216.0	1249.0	1217.0	1206.0	1218.0	1222.0	1000 80	1223.80
Point Duration (min) =	Bar. Pres. (in Hg) =	Static Pres. (in WC) =	Nozzle Dia (in WC) =	Meter dH @ =	Meter Yd =	H2O Mass (ml/g) =			dH1/2	(in WC)1/2	. 0	1.28	1.26	1.25	1.25	1.25	1.25	1.25	1.25	1.26	1.25	1.25	1.25	1.25	1.24	1.24	1.26	1.26	1.25	1.26	1.26	1.25	1.26	1.26	1.25	1.25	1 25	67.1
									书	(in WC)	. 631	1.03	1.58	1.56	1.56	1.56	. 1.56	1.56	1.56	1.58	1.56	1.56	1.56	1.56	1.54	1.54	1.58	1.58	1.56	1.58	1.58	1.56	1.58	1.58	1.56	1.56	1.57	1.57
Aine	AK								dP1/2	(in WC)1/2	0	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	07.0	00
SMMI - Pogo Mine	Delta Junction, AK	Incinerator	123-4	10/02/13	1157-1404	127			Ф	(in WC)	0100	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	2.0.0
						nin) =			Sample Volume	(acf)	3 550	0,00	3.360	3.460	3.540	3.530	3.520	3.490	3.510	3.590	3.560	3.560	3.600	3.580	3.510	3.600	3.590	3.520	3.520	3.550	3.460	3.500	3.470	3.450	3.430	4.827		
Plant =	Plant Location =	Source ID =	Run No =	Date =	Run Time =	Sample Duration (min) =			DGM Reading	(acf)	008 800	200.002	912.360	915.720	919.180	922.720	926.250	929.770	933.260	936.770	940.360	943.920	947.480	951.080	954.660	958.170	961.770	965.360	968.880	972.400	975.950	979.410	982.910	986.380	989.830	993.260	89 285	07.70
	. •		. •		. •	-			Point No.		•	٠ ،	7 (w .	4	٠	9	7	«	6	10	11	12	1	2	ĸ	4	5	9	7	∞	6	10	11	12			

	1(05) (ļ	
	1125 168	65.5	
ISOKINETIC SAMPLE DATA FORM	.71 0511	5.2	AIICOM
	1175 166	60.4	_ _ 中
Filter ID: P.3		- n	Moisture
Ambient Temp. (PF):	(700)	Imi	o. Initial Hinal
Baro. Press. (in. Hg): 2 \$ 00	5. 720.	ð. č	19757 6616
Static Press. (in H,O):	17.53		100000000000000000000000000000000000000
0,(%):			2 19:00 13:03
		-	2011:0-01:0

Moisture	796.1	731.3		723.8		_			in. H ₂ 0/15 sec.	in. H ₂ 0/15 sec.		Vacuum (in. Hg)	2	1	77	7	7,	7	₩.	Š	<i>ا</i>	5	.\ <u>\</u>	5														
	1	7		721.3	1			Static	0			DGM Temp. (°F)	\$5	29	19	63	59	99	ره	89	ダラ	59	89	69														
	Tru Tru	7	w.z	4 v	2000			Impact	۵,			DGM Te	61	1.7	73	hL	77	79	79.	90	9 <i>8</i>	ۍ ن	ပ ခ	79														
158.0	3.55.6							Pitot:	Pre:	Post:	Imp. Outlet	Temp.	775	35	40	hh	hh	45	っか	46	76	<i>th</i>	47	ઝ)-														
2.7	200.	, , ,				0.8743						riller Lemp. (F)	255	255	452	252	252	152	250	25.0	253	250	249	250														
						= 268.			iO	٠	Probe	Temp.	238	1/2	246	872	252	542	248	249	248	ل <i>اب</i> ر	245	244														
23	28.00	0,04	į	5	2.	0.874.0	ı		acf	act		Stack Temp. (F)	1211	1110	1109	1103	1,13	1211	1128	1158	\ 1 12 1	1190	1203	1199														
ė		H ₂ O):		30		1 4680			0.00.0			ΔH (in. H_20)	1911	1,66	1,66	00.1	1,66	1,66	1,66	(.63	60	1-,58	1.58	1.56														
Filter ID:		Static Press. (in	CO.(%):	Duct Dia. (in):	Bws (assumed):	Nozzle Dia. (in):	K Factor:	Leak Check:	Pre:	Post:	4	(in. H ₂ O)	10.0	6.01	0.01	0.01	6.01	0.01	0.01	0.01	0.01	0.01	8.01	0.0;														
74	ŤΙ										: 43.60	DACF)	199,662	203.34	206,90	210, ५०			221,54	225 16	228.85	232,51	236,11	2	243.287													
June 1.	チャンシャントラン	2113	, 2	AW	Binett	<i>O</i>	1,7732	403	41 RMS	6.84	į.	Sample 1 me (min.)	0	- 5	01	51	20	25	30	35	43	\Box		35	60	CS.	70	75	3	85	90	95	09/	100/	011	الكر	120	
8060	Ancin	4	T 29-	0,3	Bi			ger outlet I.D.:	ë:			Port/Point I.D.	1	2	^	,	5	و	7	Ú.	6	10	11	12	j	2	3	4	5	s	.1.	35	6	0	11	u		
Plant: Location:	Source I.D.:	Date:	Run No.:	Operators:	Meter Box I.D.:	Meter Y:	Meter Delta H@:	Probe I.D./ Impinger outlet I.D	Probe Length/Type:	Pitot Coeff. (Cp):		Time	1408											<	1506/													

Мах. Vac.

Average DGM Temp.

Avg. t_s

Avg. AH

Avg. VAP

Total Time Vol. (DACF)

		Change	83.9	27.6	3.9	17.0	-14.5	8.2	Meter Pres.	(in Hg)	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12	28.12		28.120
	ture	Final	796.1	731.3	625.7	723.8	707.4	668	Stack Pres	(in Hg)	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00	28.00		28.003
	Moisture	Initial	712.2	703.7	621.8	706.8	721.9	830.8	Velocity	(ft/s)	10.2	10.1	10.1	10.1	10.1	10.2	10.2	10.3	10.3	10.4	10.4	10.4		10.234
									DGM Ave	(F)	0.09	61.5	65.5	68.5	71.0	72.5	73.0	74.0	74.0	74.5	74.0	74.0		70.208
						•			DGM Outlet	(F)	59.0	59.0	61.0	63.0	65.0	0.99	67.0	68.0	68.0	0.69	0.89	0.69		65.167
	5	28	0.04	0.8743	1.7732	1.0034	126.1		DGM Inlet	(F)	61.0	64.0	70.0	74.0	77.0	79.0	79.0	80.0	80.0	80.0	80.0	79.0		75.250
	=(u	11	=(;	=(;					Stack T	(F)	1121.0	1110.0	1109.0	1103.0	1113.0	1121.0	1128.0	1158.0	1180.0	1190.0	1203.0	1199.0		1144.583
	Point Duration (min) =	Bar. Pres. (in Hg) =	Static Pres. (in WC) =	Nozzle Dia (in WC) =	Meter dH @ =	Meter Yd =	H2O Mass (ml/g) =		dH1/2	(in WC)1/2	1.288	1.288	1.288	1.288	1.288	1.288	1.288	1.277	1.265	1.257	1.257	1.257		1.278
									ΗP	(in WC)	1.66	1.66	1.66	1.66	1.66	1.66	1.66	1.63	1.60	1.58	1.58	1.58		1.633
	Mine	AK							₫₽1/2	(in WC)1/2	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100		0.100
	SMMI - Pogo Mine	Delta Junction, AK	Incinerator	129-1	09/29/13	1406-1506	09		Ð	(in WC)	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.010
•			1	1	_		nin) =		Sample Volume	(acf)	3.678	3.560	3.500	3.650	3.840	3.650	3.620	3.690	3.660	3.600	3.580	3.597		
	Plant =	Plant Location =	Source ID =	Run No =	Date =	Run Time =	Sample Duration (min) =		DGM Reading	(acf)	199.662	203.340	206.900	210.400	214.050	217.890	221.540	225.160	228.850	232.510	236.110	239.690	243.287	43.625
									Point No.	e de la companya de l		7	m	4	5	9	7	8	6	10	11	12		

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					ISOKINET	KINETIC SAMPLE DATA FORM	ATA FORM		7	‡		ATCOM
Plant:	7000	Mine		Filter ID:	id			7613] :=	- (;	
Location:	1 Deita	fa June him	MIC	Ambient Temp. (PF):				1	<u>-</u> 	· Imu	Initial	Moisture
Source I.D.:	inc	2000		Baro. Press. (in. Hg):	"	25		1150	0 162.9		r	Fullall Sec. 5
Date:		9-30-13		Static Press. (in H,O):		6.04		1175	7.07.		7567	75/36
Run No.:	7	75-2		02(%):				- - !		4	13	632.1
Operators:	1	06.AW		Duct Dia. (in):	369			0021 -				725.2
Meter Box I.D.:				B _{ws} (assumed):	21		1	17.7.5	i 55.6	0	М	125
Meter Y:		~ (Nozzle Dia. (in):	0.8747	7		, , ,			j	7,5,7
Drobe I D / Imain	::::::::::::::::::::::::::::::::::::::			K Factor:								io.
Probe Length/Tyne:	r100e 1.D./ Impinger outlet 1.D.: Prohe I enoth/Tyne:	7/2		Leak Check:	(9	Ć		Pitot:	Impact	Static	
Pitot Coeff. (Cp):);	0.54		Post:	0 .000	act	24	in. Hg Vac.	Pre: Post:	อ	O	in. H ₂ 0/15 sec. in. H ₂ 0/15 sec.
DGM Clock		Sample Time	DGM Peoding	ΔV	VIIV		Probe	E	Imp. Outlet			
Time	Port/Point I.D.		(DACF)	(in. H ₂ O)	(in. H ₂ 0)	Stack Temp. (F)	Temp.	ruce remp.	Temp.	DGMI	DGM Temp. (°F)	Vacuum (in. Hg)
1505	•	0	501:584	0.00	1.66	(120	h57.	142	173	20)	60	V
	2	5		0,0	1.66	(10)	292	254	do	ee	2.7	S
	`\	١٥		0.0(1,66	1,07	255	752	40	69		\v
	2	20	449 68	0.0	1, 1, 1,	8,401	25.5	256	707	17,	29	5
	9	52		10.0	7071	361	2.50	200	76		21	5
	7	30	506.99	0,01	(, 66.	8111	250	25.	2/7	75	60	~ V
	دار	35	7	0.01	2211	1159	249	251	43	1	77	\v
	7	0)	27.77.50	0.01	1.63	ろアニ	251	250	43	רר	65	2
	0 :	S S	57 + 74	0.0 0.0	3 (3)	1131	25.5	157	पंत	77	65	e
	2/	25	520 25	0 0	1.53	1139	200	152	775	X.	9,9	6
	,	09	528 27	0.0	1,0,1	7	282	2,46	21/2	300	و ف ا	9,
	2	ĠΣ	532, 51	0.01	1,60	1165	246	052	25	79	200	
	<u> </u>	70	536.14	5.01	1.60	6213	250	052	47	79	6.7	9.4
	4	\$ (\$	25.05	(a)	1,58	1700	246	241.	1.17	して	67	7
	^2	200	247.55		0/1	11 (2	20/9	250	210	17	67	7
	10	900	550.47	10.0	1,63	2 20	247	157	2/2	16	000	7
	g	95	Ι.	10.0	1.63	2/17	100	757	9/1	١١٥	, 0	1
	6	00)	155-76	0:01	1,63	1 56	244	0.52	7/7	1/0	5 7	
	0)	(0)	561, 43	0.0	1.60	1172	7\$2	25.0	52	7)[00	1
	3	110	565 10	6.01	1, 60	99))	247	252	45	75	200	T
	1/2	211	568, 72	0.01	1.66	9811	13Z	152	47	76	25.79	1
L. L.		02)		0,0	ر شع	140	251	252	L#1	76	66	-
7: 1		77	2 (-1,5)									•
		Total Time	Vol (DACE)	AVE JAP	Ava AH	A vyer +						
					1115. CHI	\$.9.11				Average DGM Temp.	GM Lemp.	Max. Vac.

		134.7	45.2	8.9	8.8	6.0	14.4	0.0	Jes.	(g)		_	_	7	_		_	7		_	_		_				_	_	_		_	7	_		_			
	Change								Meter Pres.	(in Hg)	, c	76.57	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37	28.37		28.37
ture	Final	850.2	751.9	632.7	725.2	709	913.4		Stack Pres	(in Hg)	i c	67.97	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25	28.25		28.25
Moisture	Initial	715.5	706.7	625.9	720.4	708.1	668		Velocity	(ft/s)	,	10.1	10.0	10.0	10.0	10.1	10.1	10.1	10.2	10.1	10.1	10.1	10.1	10.0	10.2	10.2	10.3	10.2	10.2	10.2	10.2	10.2	10.2	10.2	10.1	10.1		10.1 28.25
									DGM Ave	(F)	3 07	67.7	64.0	65.5	66.5	0.89	68.5	0.69	70.0	71.0	71.0	72.0	72.0	72.0	73.0	73.0	72.0	72.0	71.0	71.5	71.0	71.0	71.0	70.0	70.5	71.0		6.69
									DGM Outlet	(F)	0.00	0.70	62.0	62.0	62.0	63.0	63.0	63.0	64.0	65.0	65.0	0.99	0.99	0.99	67.0	67.0	67.0	0.79	0.99	67.0	0.99	0.99	0.99	65.0	65.0	0.99		65.0
ν.	28.25	0.04	0.8747	1.7732	1.0034	206.8			DGM Inlet	(F)	0 63	0.50	0.99	0.69	71.0	73.0	74.0	75.0	76.0	77.0	77.0	78.0	78.0	78.0	79.0	79.0	77.0	77.0	76.0	76.0	76.0	76.0	76.0	75.0	76.0	76.0		75.0
= (u		=(=(Stack T	(F)	1120.0	1120.0	1101.0	1107.0	1098.0	1118.0	1128.0	1118.0	1159.0	1144.0	1131.0	1141.0	1139.0	1113.0	1165.0	1179.0	1200.0	1172.0	1172.0	1150.0	1164.0	1159.0	1172.0	1166.0	1136.0	1140.0		1143.7
Point Duration (min)	Bar. Pres. (in Hg)=	Static Pres. (in WC) =	Nozzle Dia (in WC) =	Meter dH @ =	Meter Yd =	H2O Mass (ml/g) =			dH1/2	(in WC)1/2	1 200	1.200	1.288	1.288	1.288	1.288	1.288	1.288	1.277	1.277	1.265	1.277	1.277	1.288	1.265	1.265	1.257	1.265	1.265	1.277	1.277	1.277	1.265	1.265	1.288	1.277		1.277
н	щ		4	A	4	I			HP	(in WC)	1 66	3	1.66	1.66	1.66	1.66	1.66	1.66	1.63	1.63	1.60	1.63	1.63	1.66	1.60	1.60	1.58	1.60	1.60	1.63	1.63	1.63	1.60	1.60	1.66	1.63		1.630
fine	AK								dP1/2	(in WC)1/2	0 100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100		0.100
SMMI - Pogo Mine	Delta Junction, AK	Incinerator	129-2	09/30/13	1505-1712	127			ď₽	(in WC)	100	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		0.010
						nin) =			Sample Volume	(acf)	2 646	6	303.640	-296.340	3.630	3.680	3.630	3.650	3.620	3.680	3.690	3.620	3.620	3.640	3.630	3.600	3.610	3.620	3.460	3.700	3.630	3.670	3.670	4.620	2.670	5.127		
Plant =	Plant Location =	Source ID =	Run No =	Date =	Run Time =	Sample Duration (min) =			DGM Reading	(acf)	105 105	701.00	488.750	792.390	496.050	499.680	503.360	506.990	510.640	514.260	517.940	521.630	525.250	528.870	532.510	536.140	539.740	543.350	546.970	550.430	554,130	557.760	561.430	565.100	569.720	572.390	577.517	92.412
,		J	pand .		#	V 1			Point No.			٠ .	2	m	4	S	9	7	∞	σ	10	111	12	-	2-	ю	4	'n	9	7	∞	σ,	10	11	12			

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AICOM	Moisture	7(5.3 854 6	148 G	626.3 630.7	7.807	413 H Net Gain 924 /			Static	in H-0/15 cor	in. H ₂ 0/15 sec.
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	اردی کر ۱	ر 62.5 1	160.7	(SS.C) 3	155.6 5	•			Impact	j O	
(°E)	\$211	3 6	175	0021	52		•		Pitot		/ac. Post:
DATA FORM										/ O in. Hg Vac.	jin. Hg Vac.
KINETIC SAMPLE DATA FORM	75	28.40	0.04		.,≎∑	21	£448			OOO acf	cot acf
ISOKI	Filter ID:	Baro. Press. (in. Hg):	Static Press. (in H,O):	U ₂ (%): CO ₂ (%):	Duct Dia. (in):	B _{ws} (assumed):	Nozzle Dia. (in): c .	K Factor:	Leak Check:	Pre: 0.0	
	Paso Mine	Lacinerates	10-1-13	T 29-3	DB, AV	Bleck	1.00334	1.7732	tlet I.D.: 403	4' 2ms	h8 '0
	Plant: Location:	Source I.D.:	Date:	Run No.:	Operators:	Meter Box I.D.:	Meter Y:	Meter Delta H@:	Probe I.D./ Impinger outlet I.D.:	Probe Length/Type:	Pitot Coeff. (Cp):

Vacuum (in. Hg)	ن	, , ,	1	\ \ \	4	2	\ \ \	\$	\ \ \	5	6	1		5	1	`	V	*	2	<u> </u>	۲.	٧	٧.	5	~				Max. Vac.	
DGM Temp. (F)	47	77	77.	7	Øħ	ş	1	25	25	75	56	ر د ک	ر ا ا	5.7	00	61	20)	63	6.3	63	カツ	6.5	59	65					ЭМ Тетр.	
DGM Te	レン	SN	5.3	57	58	63	ho	7.3	1.9	63	70	17	26	77	73	74	7 5	7.5	16	72	76	96	26	76	76				Average DGM Temp.	
Imp. Outlet Temp. (PF)	33	38	35	39	32	.34	39	40	34	38	40	40	40	5	42	42	É	11/	27	42	44	77	hh	55	hh					
Filter Temp. (°F)	248	250	253	252	<i>C</i> \$2	052	251	152	250	502	5772	250	052	252	272	252	252	251	1.52	256	252	252	27.7	200	152					
Probe Temp.	252	255	250	25(25 (251	7.52	1.52	377	249	25.0	550	152	2016	122	7.56	282	252	250	254	248	50	251	248	0.27					
Stack Temp. (F)	0111	1011	2711	1123	りわけ	! (אמ	113d	-560	((50	1138	1192	1176	1147	1911	(133	1143	1156	1141	115Y	11531	1140	1157	1154	1149	128				Avg. t _s	
ΔH (in. $H_2 0$)	9971	991	1,66	1.66	1,63	1,63	1,66	1.60	6, أ. ا	(,63	1.58	1,60	1,63	(,63	1,66	1.63	1.1.7	1167	1,63	1.63	1,63	1.63	1,63	1.67	1.66				Avg. AH	
ΔP (in. H_2O)	0.0(10:0	0.01	10,0	0.01	0.0	0.01	0.01	0.0	0.01	0,0	0.0	0	0.01	10.0	0.01	10.0	10.0	0.01	ئي. ت	10,0	0.01	10.0	10.0	0.01				Avg. VAP	
DGM Reading (DACF)	577,663	581.25	584.85	588.42	St. 0.	595.67	599,26	1,02 . 200	600,42	610.03	613,64	617, 16	620,70		627.90	636,54	635.27	678. 93	642.60		38,843	653.50	657.13	260 75	664.38	669.510			Vol. (DACF)	
Sample Time (min.)	0		0/			2.5	3°c	35	40	۲۶	So	5٤	09	99	70	75	30	85	90		/00	105	011	11.5	120	127	•		Total Time	
Port/Point I.D.)	2	2	7	5	Ġ	-	⊗	9	0/	11	2/		7	3	7	٧	و	7	વડ	G	(0)	ij	12						1
DGM Clock Time	HS4																									9011				

٠	Change	139.3	40.8	4.4	3.1	0.4	10.7	0	Meter Pres.	(in Hg)		28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52	28.52		28.52
ture	Final	854.6	748.6	630.7	724.7	708.6	924.1		Stack Pres	(in Hg)	:	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40	28.40		28.40
Moisture	Initial	715.3	707.8	626.3	721.6	708.2	913.4		Velocity	(£/s)		10.0	10.0	10.0	10.0	10.1	10.1	10.1	10.2	10.1	10.1	10.3	10.2	10.1	10.2	10.1	10.1	10.1	10.1	10.2	10.1	10.1	10.1	10.1	10.1	10.1		10.1
									DGM Ave	(F)		47.0	47.5	49.5	52.0	53.5	56.0	57.5	59.0	0.09	61.0	63.0	64.0	65.0	0.99	66.5	67.5	68.5	0.69	69.5	69.5	70.0	70.5	70.5	70.5	70.5		62.5
									DGM Outlet	(F)		47.0	45.0	46.0	47.0	48.0	49.0	51.0	52.0	53.0	54.0	56.0	57.0	58.0	59.0	0.09	61.0	62.0	63.0	63.0	63.0	64.0	65.0	65.0	65.0	65.0		56.7
5	28.4	0.04	0.8747	1.7732	1.0034	198.7			DGM Inlet	(F)	ć,	0./4	50.0	53.0	57.0	59.0	63.0	64.0	0.99	67.0	0.89	70.0	71.0	72.0	73.0	73.0	74.0	75.0	75.0	76.0	76.0	76.0	76.0	76.0	76.0	76.0		68.4
1)=		= (=						Stack T	(F)	·	1110.0	1101.0	1122.0	1123.0	1144.0	1144.0	1134.0	1175.0	1150.0	1138.0	1192.0	1176.0	1147.0	1164.0	1133.0	1143.0	1156.0	1141.0	1158.0	1153.0	1140.0	1153.0	1154.0	1149.0	1128.0	1	1145.1
Point Duration (min) =	Bar. Pres. (in Hg) =	Static Pres. (in WC)	Nozzle Dia (in WC) =	Meter dH @ =	Meter Yd =	H2O Mass (ml/g) =			dH1/2	(in WC)1/2	900	1.288	1.288	1.288	1.277	1.277	1.288	1.265	1.277	1.277	1.257	1.265	1.277	1.277	1.288	1.277	1.277	1.277	1.277	1.277	1.277	1.277	1.277	1.277	1.277	1.288		1.278
									书	(in WC)	77	1.00	1.66	1.66	1.63	1.63	1.66	1.60	1.63	1.63	1.58	1.60	1.63	1.63	1.66	1.63	1.63	1.63	1.63	1.63	1.63	1.63	1.63	1.63	1.63	1.66		1.633
fine	AK								₽1/2	(in WC)1/2	6	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100		0.100
SMMI - Pogo Mine	Delta Junction, AK	Incinerator	I29-3	10/01/13	0859-1106	127			Ð	(in WC)	010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0,00	0.010
						nin) =			Sample Volume	(acf)	2 607	1.301	3.600	3.570	3.590	3.660	3.590	3.620	3,540	3.610	3.610	3.520	3.540	3.590	3.610	2.640	4.730	3.660	3.670	3.640	3.640	3.620	3.630	3.620	3.630	5.130		
Plant =	Plant Location =	Source ID =	Kun No =	Date =	Run Time =	Sample Duration (min) =			DGM Reading	(acf)	277 663	500.770	581.250	584.850	588.420	592.010	595.670	599.260	602.880	606.420	610.030	613.640	617.160	620.700	624.290	627.900	630.540	635.270	638.930	642.600	646.240	649.880	653.500	657.130	660.750	664.380	010:000	91.847
•				•					Point No.		-	٠ ,	7	m	4	'n	9	7	8	6	10	Π	12	-	7	٣	4	5	9	7	8	6	10	11	12			

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		ISOKI	ISOKINETIC SAMPLE DATA FORM	A FORM		·	# 410	Z
Plant	Dog Mint	Filter ID:	せん	<u></u>	>) (点)		;	
Location:	Delta Sunchion, AK	Ambient Tenn. (P):	34		+	1	Moisture	
Source I.D.:	indingatar	Baro. Press. (in. Hg):	75.27		5.591 5211	im S	- mutal Final	
Date:	10-2-13	Static Press (in H.O):	700			U	1 107.5) <u>\$</u> 3h
Flow Traverse Time:	6,4	0,(%):	ý		1.20 - 001	•	7708.8 754.4	
Run No.:	7-8-1	CO, (%):			11/2/11/2	(3 625.5 630.7	
Operators:	NR 260	Duct Dia. (in):	1102		7 : oo : - c :)	4 722.1 711.0	
Meter Box I.D.:	8 16 616	B (assumed):	2		7 3>) (302)	(8	
Meter Y:	1,00335	Nozzle Dia. (in):	<u> </u>			2	424, 1 Net Gain 933, 2	
Meter Delta H@:	17732	K Factor:						
Probe I.D./ Impinger outlet I.D.:	outlet I.D.: 4_D 3	Leak Check:			Ditot:	1	÷	
Probe Length/Type:	41 RMS	Pre: 0.00	acf	in Ho Vac	Dra.	unpact	Static	
Pitot Coeff. (Cp):	h8.0	Post: 0.00	3 acf	in Ho Vac	Doet.	٥	O in. H ₂ 0/15 sec.	ن ن
				m 415 mc	100		m. H ₂ 0/15 sec.	ປ

	Vacuum (in. Hg)		8	2	2	2.	Ş	Š	6	4	V	1	ı	1	1		1	7	2	ک	\$	5		م إ	,,,	Į.			2					Max. Vac.	
	DGM Temp. (°F)		34	7,7	2	35	30	37	00 00	35	ر بر	111	7	7.3	3	70/	277	١	47	4.1	41	27.3	46	1,125	50	123	43	225)					iM Temp.	
	DGM Te	96	25	22	75	45	77	49	21	5.3	.45	6,6	3	57	46	000	750			00	ÇC	9	6/	67.	(27	67	27	\ \ \	٦					Average DGM Temp.	
Imp. Outlet	_	25	2,5	26	3/5	300	27	2,5	ۍ. ۲	37	3.7	33	7.5	52	5.5	120	30	200	i i	75	36	35	46.	20	40	2.5	70	17							
Filter Temn	€	130	1,1,0	1,52	25.7	52 5		14.51	249	249	252	257	152	252	252	250	249	757	100	37,	257	157	25.5	252	557	248	3.52	757							
Probe	Temp.	20.6	757	777	136	25.7	2,70	1217	24%	277	152	253	251	252	0.52	200	2×7	10/		3	252	152	249	252	252	545	748	250							
	Stack Temp. (F)	1672	5117	7///	1001	7.617	13/11	- CT	1/3/	1140	1137	1100	116.7	1152	1122	1211	1/4/1	1157	7,5	1,35	\$677	1115	1125	ותת	inu	11.46	1166	2211						Avg. t _s	
H∇	(in. H_20)	77'	1.7.1	1,7,7	0,,,		7/1	277	1,66	1,63	95,11	1,65	1.63	1,63	1.66	1771	1,63	1.6.7		1000	3	1.66	1,16	1,63	1.6.3	1.63	160	1,66						Avg. ΔH	
₽	(in. H_2O)	13:0	10:0	0.0	0.00	3	0	3 6	130	0.00	13.73	001	0.01	0.61	0,5 f	0.0	3.03	10,0	100	100	3 ,	2.0	0.0	c, c,	~7	10,0	0,0	0.01						Avg. VAP	
DGM Reading	(DACF)	8:8.522	922.03	325.62	829.00	73 54		20.00	4	-	21 31.25	*1	- 4	137.65		C64.85	21.8 48	35:15	7		7 000	00 x x 200	486.28	3,3	٠,		5000, 30	26 5010	900 642	•			(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	VOI. (UACF)	
Sample Time	(min.)	0	V	0/	//	22	25	202	32		200	35	20	\$\$	00	65	20	75	08	23	2,2	2/2	1	1		0);		2	121				Total Time	Total Tillie	
Doct Moding 1 D	roturomi i.D.	-	7	3	I	ۍ,	0)	7	0	90	- C	2	=	7,1		7	3	1,1	200	27	35		عن	4	100	7	77								J
DGM Clock	Time	K + S																												250	,				

	Change	127.8	45.6	5.2	-11.1	14.2	8.9	0	Meter Pres.	(in Hg)		28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57	28.57		28.57
hre	Final (837.3	754.4	630.7	711.0	722.3	933		Stack Pres	(in Hg)		28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45	28.45		28.45
Moisture	Initial	709.5	708.8	625.5	722.1	708.1	924.1		Velocity	(ft/s)		7.6	10.0	10.0	6.6	10.0	10.0	10.1	10.1	10.1	10.0	10.2	10.1	10.0	10.0	10.1	10.1	10.0	10.1	10.0	10.0	10.1	10.1	10.1	10.2	10.0		10.0
									DGM Ave	(F)		34.5	36.0	38.0	40.0	41.5	43.0	44.5	46.0	47.0	48.0	48.5	50.0	51.0	51.5	52.5	53.0	53.5	53.5	54.0	55.0	56.0	56.0	56.0	58.5	59.0		49.1
									DGM Outlet	(F)	-	34.0	34.0	34.0	35.0	36.0	37.0	38.0	39.0	40.0	41.0	41.0	43.0	44.0	45.0	46.0	47.0	47.0	47.0	48.0	49.0	50.0	50.0	50.0	52.0	53.0		43.2
5	28:45	0.04	0.8747	1.7732	1.0034	190.6			DGM Inlet	(F)		35.0	38.0	42.0	45.0	47.0	49.0	51.0	53.0	54.0	55.0	56.0	57.0	58.0	58.0	59.0	59.0	0.09	0.09	0.09	61.0	62.0	62.0	62.0	65.0	65.0		54.9
n) =		= (;	= (:			11			Stack T	(F)		1023.0	1117.0	1112.0	1096.0	1124.0	1115.0	1131.0	1140.0	1137.0	1100.0	1167.0	1152.0	1122.0	1127.0	1141.0	1157.0	1117.0	1138.0	1115.0	1125.0	1144.0	1144.0	1146.0	1166.0	1122.0		1127.1
Point Duration (min) =	Bar. Pres. (in Hg) =	Static Pres. (in WC)	Nozzle Dia (in WC) =	Meter dH @=	Meter Yd =	H2O Mass (ml/g) =			dH1/2	(in WC)1/2		1.296	1.288	1.288	1.296	1.288	1.288	1.288	1.277	1.288	1.296	1.277	1.277	1.288	1.288	1.277	1.277	1.288	1.277	1.288	1.288	1.277	1.277	1.277	1.265	1.288		1.284
									HP	(in WC)		1.68	1.66	1.66	1.68	1.66	1.66	1.66	1.63	1.66	1.68	1.63	1.63	1.66	1.66	1.63	1.63	1.66	1.63	1.66	1.66	1.63	1.63	1.63	1.60	1.66		1.649
fine	AK								₫₽1/2	(in WC)1/2		0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	-0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100	0.100		0.100
SMMI - Pogo Mine	Delta Junction, AK	Incinerator	129-4	10/02/13	0845-1052	127			ď₽	(in WC)		0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010		0.010
						nin) =			Sample Volume	(acf)		3.508	3.490	3.480	3.540	3.520	3.580	3.590	3.550	3.630	3.630	3.610	3.600	3.600	3.630	3.500	3.590	3.560	9.550	-2.400	3.560	3.590	3.530	3.420	3.380	4.882		
Plant =	Plant Location =	Source ID =	Run No =	Date =	Run Time =	Sample Duration (min) =			DGM Reading	(acf)		818.522	822.030	825.520	829.000	832.540	836.060	839.640	843.230	846.780	850.410	854.040	857.650	861.250	864.850	868.480	871.980	875.570	879.130	888.680	886.280	889.840	893.430	896.960	900.380	903.760	908.642	90.120
[. 7		.=						Point No.			1	7	ю	4	5	9	7	«	6	10	11	12		7	٣	4	5	9	7	*	6	10	111	12			

Method 22

Oate: 09/30/13

Tech: John Rosburg

Source: Pogo Incinerator

Run ID: IS-2

Start Time: 1252

Stop Time: 1352

Elapsed Time: 60 min = 3600 sec

Time of Smoke: O sec

% smoke of Elopsed Time = 0.0%

Climate = overcas+

Bp = 28.30 " Hg

Temps 37 of

Wind Speed: 0-5 mph N, NW

position: south west of stack

Method 22

Date: 10/01/13

Tech: John Rosburg

Source: Pogo Incinerator

Run ID: I 29-3

Start time: 02910 -

Stop time: 1010

Elapsed Time: 60 nin = 3600 sec.

Time of Smoke: Osec 90 sacke of Elopsed Time: 0.0%

Climate:

sky: mostly cloudy

Bp: 28.45 "Ha

Temp: 29 °F

Wind Speed: 0-5 N, NW

Position: south west of stack

Method 22

Pate: 10/01/13

Tech! John Rosburg

Source'. Pogo Incinerator

Run ID: I23-3

Start Time: 1200

Stop Time: 1308

Elapsed Time: 60 min = 3600 sec

Time of Smoke: O sec. % Smoke of Elapsed Time = 00%

dimate

Sky: Mostly Cloudy

Bp: 28.45" Hg

Temp. : 34°F

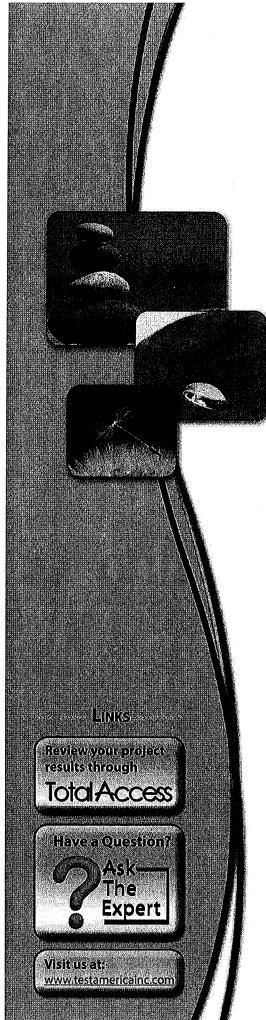
Wind Speed: 0-5 N, NW

Position: south west of stack

AECOM Environment

Appendix B

Laboratory Results



<u>TestAmerica</u>

THE LEADER IN ENVIRONMENTAL TESTING

ANALYTICAL REPORT

TestAmerica Laboratories, Inc. TestAmerica Sacramento 880 Riverside Parkway West Sacramento, CA 95605 Tel: (916)373-5600

TestAmerica Job ID: 320-4473-1

Client Project/Site: SMMI 60284905-2100

For: AECO

AECOM, Inc. 1601 Prospect Parkway Fort Collins, Colorado 80525

Attn: John Rosburg

Robert Wilfl

Authorized for release by: 10/31/2013 4:12:22 PM

Robert Weidenfeld, Project Manager II (916)374-4333 robert.weidenfeld@testamericainc.com

This report has been electronically signed and authorized by the signatory. Electronic signature is intended to be the legally binding equivalent of a traditionally handwritten signature.

Results relate only to the items tested and the sample(s) as received by the laboratory.

Table of Contents

Cover Page	1
Table of Contents	2
Definitions/Glossary	3
Case Narrative	4
Detection Summary	5
Client Sample Results	
QC Sample Results	
QC Association Summary	
Lab Chronicle	24
Certification Summary	29
Method Summary	30
Sample Summary	31
Chain of Custody	32
Receint Checklists	37

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Definitions/Glossary

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

2)	









Qualifiers

HPLC/IC

Qualifier **Qualifier Description**

Н Sample was prepped or analyzed beyond the specified holding time

Metals

Qualifier **Qualifier Description**

Quality Control

Relative error ratio

Toxicity Equivalent Factor (Dioxin)

Toxicity Equivalent Quotient (Dioxin)

Reporting Limit or Requested Limit (Radiochemistry)

Relative Percent Difference, a measure of the relative difference between two points

Result is less than the RL but greater than or equal to the MDL and the concentration is an approximate value. В

Compound was found in the blank and sample.

Glossary

QC

RER

RPD

TEF

TEQ

RL

Abbreviation	These commonly used abbreviations may or may not be present in this report.
¤	Listed under the "D" column to designate that the result is reported on a dry weight basis
%R	Percent Recovery
CNF	Contains no Free Liquid
DER	Duplicate error ratio (normalized absolute difference)
Dil Fac	Dilution Factor
DL, RA, RE, IN	Indicates a Dilution, Re-analysis, Re-extraction, or additional Initial metals/anion analysis of the sample
DLC	Decision level concentration
MDA	Minimum detectable activity
EDL	Estimated Detection Limit
MDC	Minimum detectable concentration
MDL	Method Detection Limit
ML	Minimum Level (Dioxin)
NC	Not Calculated
ND	Not detected at the reporting limit (or MDL or EDL if shown)
PQL	Practical Quantitation Limit

Case Narrative

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Job ID: 320-4473-1

Laboratory: TestAmerica Sacramento

Narrative

Job Narrative 320-4473-1

Comments

No additional comments.

Receipt

The samples in this report were received on 10/7/2013 9:00 AM; the samples arrived in good condition. The temperatures of the samples at receipt time were 14.6° C, 14.8° C and 15.1° C.

Metals

Method 29/6020:

The laboratory method blank associated with the audit (impinger) sample is positive for lead slightly above the 0.15 ug reporting limit (RL) at 0.164 ug. The audit sample is positive for this analyte at concentrations greater than 10X the value found in the method blank.

No other analytical or quality issues were noted.

General Chemistry-HCI

Method 0050/26A:

Due to a laboratory oversight, sample I5-1 (320-4473-6) and the associated matrix spike/matrix spike duplicate were analyzed one day outside of the 28 day hold time. The hold time expired on 10/27/13 and the sample was analyzed on 10/28/13.

No other analytical or quality issues were noted.

Detection Summary

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Analyte									D: 320-4473-
Allalyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Prep Type
Cadmium	9.0		0.35	0.026	ug/Sample	1	_	29/6020	Total/NA
Lead	97	В	0.35	0.023	ug/Sample	1		29/6020	Total/NA
Hg	0.65		0.030	0.0074	ug/Sample	1		29/7470A	Total/NA
Hg	0.59		0.10	0.025	ug/Sample	1		29/7470A	Total/NA
Hg 	0.87		0.80	0.20	ug/Sample	1		29/7470A	Total/NA
Client Sample ID: I29-2						L	.ab	Sample II	D: 320-4473-
- Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Ргер Туре
Cadmium	. 13		0.34	0.025	ug/Sample	1		29/6020	Total/NA
Lead	980	В	0.34	0.022	ug/Sample	1,		29/6020	Total/NA
Hg	0.077	J	0.21	0.052	ug/Sample	1		29/7470A	Total/NA
Hg	0.17		0.030	0.0074	ug/Sample	1		29/7470A	Total/NA
Hg	0.25		0.10	0.025	ug/Sample	1		29/7470A	Total/NA
Hg	1.2		0.95	0.23	ug/Sample	1		29/7470A	Total/NA
lient Sample ID: I29-3	At the street of	s			- delimination of a section of the s	L	.ab	Sample II	D: 320-4473
Analyte	Result	Qualifier	RL.	MDL	Unit	Dil Fac	D	Method	Prep Type
Cadmium	9.3		0.34	0.025	ug/Sample	1	_	29/6020	Total/NA
Lead	410	В	0.34		ug/Sample	1		29/6020	Total/NA
Hg	0.20		0.030	0.0074	ug/Sample	1		29/7470A	Total/NA
Hg	0.28		0.10	0.025	ug/Sample	1		29/7470A	Total/NA
Client Sample ID: I29-4				·		L	.ab	Sample II	D: 320-4473-
Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Prep Type
Cadmium	9.9		0.34	0.025	ug/Sample	1	_	29/6020	Total/NA
Lead	360	В	0.34	0.022	ug/Sample	1		29/6020	Total/NA
Hg	0.13		0.030	0.0074	ug/Sample	1		29/7470A	Total/NA
Hg	0.34		0.10	0.025	ug/Sample	1		29/7470A	Total/NA
lient Sample ID: BLANK						L	.ab	Sample II	D: 320-4473
Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Prep Type
Cadmium	0.060	J	0.38	0.028	ug/Sample	1	_	29/6020	Total/NA
Lead	8.5	В	0.38	0.025	ug/Sample	1		29/6020	Total/NA
Hg	0.051	J	0.10	0.025	ug/Sample	1		29/7470A	Total/NA
Client Sample ID: I5-1			,,			L	.ab	Sample II	D: 320-4473
Client Sample ID: I5-1	Result	Qualifier	RL	MDL	Unit	Dil Fac		Sample II	D: 320-4473 Prep Type

This Detection Summary does not include radiochemical test results.

Analyte

Particulate Matter

Particulate Matter

Client Sample ID: 15-2

TestAmerica Sacramento

Lab Sample ID: 320-4473-7

RL

0.0005

0.0005

Result Qualifier

0.0820

0.0235

RL Unit

0.0005 g

0.0005 g

Dil Fac D Method

5

Prep Type

Total/NA

Total/NA

Detection Summary

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

•									
Analyte		Qualifier	RL		Unit	Dil Fac	D	Method	Prep Type
Hydrochloric Acid	240		11	5.5	mg/sample	50		0050/26A	Total/NA
Analyte	Result	Qualifier	RL	RL	Unit	Dil Fac	D	Method	Prep Type
Particulate Matter	0.0532		0.0005	0.0005	g	1	_	5	Total/NA
Particulate Matter	0.0141		0.0005	0.0005	9	1		5	Total/NA
Client Sample ID: I5-3				TO THE RESERVE AND ADDRESS OF THE SECOND		L	.al	Sample I	D: 320-447
Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Prep Type
Hydrochloric Acid	230		11	5.4	mg/sample	50	_	0050/26A	Total/NA
Analyte	Result	Qualifier	RL	RL	Unit	Dil Fac	D	Method	Prep Type
Particulate Matter	0.0681		0.0005	0.0005	g	1	_	5	Total/NA
Particulate Matter	0.0165		0.0005	0.0005	g	1		5	Total/NA
Client Sample ID: I5-4						L	.al	Sample I	D: 320-447
- Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Prep Type
Hydrochloric Acid	530		41	21	mg/sample	200	_	0050/26A	Total/NA
Analyte	Result	Qualifier	RL	RL	Unit	Dil Fac	D	Method	Prep Type
Particulate Matter	0.0922		0.0005	0.0005		1	_	5	Total/NA
Particulate Matter	0.0399		0.0005	0.0005		1	4	5	Total/NA
lient Sample ID: I5-BLANK			the facility and the second of			La	ıb	Sample ID	: 320-4473
Analyte	Result	Qualifier	RL	RL	Unit	Dil Fac	D	Method	Prep Type
Particulate Matter	0.0014	-	0.0005	0.0005	g	1	_	5	Total/NA
Particulate Matter	0.0016		0.0005	0.0005	g	1		5	Total/NA
Client Sample ID: PEA1941						La	ıb	Sample ID	: 320-4473
Analyte	Result	Qualifier	RL ·	MDL	Unit	Dil Fac	D	Method	Prep Type
Hydrochloric Acid	38		2.6	1.3	mg/sample	5	-	0050/26A	Total/NA
lient Sample ID: PEA1945						La	ıb	Sample ID	: 320-4473
Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Prep Type
Cadmium	87		0.15	0.011	ug/Sample	1	_	29/6020	Total/NA
Lead	74	В	0.15	0.0099	ug/Sample	1		29/6020	Total/NA
lient Sample ID: PEA1947						La	b	Sample ID	: 320-4473
Analyte	Result	Qualifier	RL	MDL		Dil Fac	D	Method	Prep Type
Hg	6.0		0.24	0.059	ug/Sample	8	_	29/7470A	Total/NA
lient Sample ID: PEA1948						La	b	Sample ID	: 320-4473
Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Ргер Туре
Cadmium	27		0.15	0.011	ug/Sample	1	_	29/6020	Total/NA

This Detection Summary does not include radiochemical test results.

Detection Summary

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

Client Sample ID: PEA1950

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-15

	Analyte	Result	Qualifier	RL	MDL	Unit	Dil Fac	D	Method	Prep Type	•
İ	На	160		6.0	1.5	ug/Sample		_	29/7470A	Total/NA	



Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-1

Client Sample ID: I29-1 Date Collected: 09/29/13 00:00

Matrix: Air

Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

Analyte R	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fa
Cadmium	9.0		0.35	0.026	ug/Sample		10/11/13 10:05	10/24/13 11:45	-
Lead	97	В	0.35	0.023	ug/Sample		10/11/13 10:05	10/24/13 11:45	
Method: 29/7470A - Mercury - Empty									
Analyte R	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fa
Hg	ND		0.20	0.050	ug/Sample	_	10/10/13 10:31	10/10/13 14:34	
Method: 29/7470A - Mercury - Front Half									
	Result	Qualifier	. RL	MDL	Unit	D	Prepared	Analyzed	Dil Fa
Hg	0.65		0.030	0.0074	ug/Sample		10/16/13 09:19	10/16/13 11:29	
Method: 29/7470A - Mercury - HCI									
•	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fa
Hg	0.59	<u> </u>	0.10	0.025	ug/Sample		10/16/13 09:23	10/16/13 12:10	
Method: 29/7470A - Mercury - KMNO4				•					
•	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fa
Hg	ND		0.10	0.025	ug/Sample		10/10/13 10:29	10/10/13 13:35	
Method: 29/7470A - Mercury - Nitric/Peroxi	ide								
		Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fa
Hg	0.87		0.80	0.20	ug/Sample		10/10/13 10:24	10/10/13 13:59	

Client Sample ID: 129-2 Lab Sample ID: 320-4473-2

Date Collected: 09/30/13 00:00 Date Received: 10/07/13 09:00

Method: 29/6020 - Metals (ICPMS), Statio	onarv S	ource							
Analyte	-	Qualifier	RL	MDL	Unit	Đ	Prepared	Analyzed	Dil Fac
Cadmium	13		0.34	. 0.025	ug/Sample		10/11/13 10:05	10/24/13 11:41	1
Lead	980	В	0.34	0.022	ug/Sample		10/11/13 10:05	10/24/13 11:41	1
Method: 29/7470A - Mercury - Empty									
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hg	0.077	J	0.21	0.052	ug/Sample		10/10/13 10:31	10/10/13 14:39	1
Method: 29/7470A - Mercury - Front Half		•							
Analyte		Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hg	0.17		0.030	0.0074	ug/Sample		10/16/13 09:19	10/16/13 11:31	1
Method: 29/7470A - Mercury - HCI	•								
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hg	0.25		0.10	0.025	ug/Sample		10/16/13 09:23	10/16/13 12:11	1
Method: 29/7470A - Mercury - KMNO4									
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hg	ND		0.10	0.025	ug/Sample		10/10/13 10:29	10/10/13 13:37	

Matrix: Air

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

Client Sample ID: 129-2

Date Collected: 09/30/13 00:00

Date Received: 10/07/13 09:00

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-2

Matrix: Air

Method: 29/7470A - Mercury - Nitric/Peroxide

Sample Container: Amber Glass 500mL - unpreserved

Analyte RL Result Qualifier MDL Unit D Dil Fac Prepared Analyzed Hg 0.95 1.2 0.23 ug/Sample 10/10/13 10:24 10/10/13 14:01

Client Sample ID: 129-3 Lab Sample ID: 320-4473-3 Matrix: Air

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

Method: 29/6020 - Metals (ICPMS), Stationary Source Analyte Result Qualifier RL. MDL Unit Prepared Analyzed Dil Fac Cadmium 9.3 0.34 0.025 ug/Sample 10/11/13 10:05 10/24/13 11:37 Lead 410 B 0.34 0.022 ug/Sample 10/11/13 10:05 10/24/13 11:37

Method: 29/7470A - Mercury - Empty Analyte Result Qualifier RL MDL Unit Prepared Analyzed Dil Fac Hg ND 0.21 0.052 ug/Sample 10/10/13 10:31 10/10/13 14:42

Method: 29/7470A - Mercury - Front Half Analyte Result Qualifier RL MDL Unit Prepared Dil Fac Hg 0.20 0.030 0.0074 ug/Sample 10/16/13 09:19 10/16/13 11:38

Method: 29/7470A - Mercury - HCI Analyte Result Qualifier RL MDL Unit Analyzed Dil Fac Hg 0.10 0.025 ug/Sample 10/16/13 09:23 0.28 10/16/13 12:16

Method: 29/7470A - Mercury - KMNO4 Analyte Qualifier RL MDL Unit Result Prepared Analyzed Dil Fac Hg ND 0.10 0.025 ug/Sample 10/10/13 10:29 10/10/13 13:39

Method: 29/7470A - Mercury - Nitric/Peroxide Analyte Result Qualifier RL MDL Unit Prepared Analyzed Dil Fac Hg 0.95 ND 0.23 ug/Sample 10/10/13 10:25 10/10/13 14:10

Client Sample ID: 129-4 Lab Sample ID: 320-4473-4

Date Collected: 10/02/13 00:00 Matrix: Air Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

Method: 29/6020 - Metals (ICPMS), Stationary Source Analyte RL MDL Unit Result Qualifier Prepared Analyzed Dil Fac Cadmium 9.9 0.34 0.025 ug/Sample 10/11/13 10:05 10/24/13 11:34 Lead 360 B 0.34 0.022 ug/Sample 10/11/13 10:05 10/24/13 11:34

Method: 29/7470A - Mercury - Empty MDL Unit Analyte Result Qualifier RL Prepared Analyzed Dil Fac Hg ND 0.20 0.049 ug/Sample 10/10/13 10:31 10/10/13 14:43

Method: 29/7470A - Mercury - Front Half Analyte Result Qualifier RL MDL Unit Prepared Analyzed Dil Fac 0.030 Hg 0.13 0.0074 ug/Sample 10/16/13 09:19 10/16/13 11:39

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-5

10/16/13 12:20

Lab Sample ID: 320-4473-4

Matrix: Air

Matrix: Air

Client Sample ID: 129-4

Date Collected: 10/02/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

Method: 29/7470A - Mercury - HCI Analyte Result Qualifier RL MDL Unit D Dil Fac Prepared Analyzed Hg 0.10 0.025 ug/Sample 0.34 10/16/13 09:23 10/16/13 12:18 Method: 29/7470A - Mercury - KMNO4 Dil Fac Analyte Result Qualifier RI MDI Unit n Prepared Analyzed Hg ND 0.10 0.025 ug/Sample 10/10/13 10:29 10/10/13 13:41

Method: 29/7470A - Mercury - Nitric/Peroxide Result Qualifier Analyte RL MDL Unit Prepared Analyzed Dil Fac Hg ND 0.95 0.23 ug/Sample 10/10/13 10:25 10/10/13 14:12

Client Sample ID: BLANK Date Collected: 10/02/13 00:00

Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

Method: 29/6020 - Metals (ICPMS), Stationary Source Analyte Result Qualifier RL. MDL. Unit D Prepared Analyzed Dil Fac 0.38 Cadmium 0.060 J 0.028 ug/Sample 10/11/13 10:05 10/24/13 11:30 Lead 8.5 B 0.38 0.025 ug/Sample 10/11/13 10:05 10/24/13 11:30

Method: 29/7470A - Mercury - Empty Analyte Result Qualifier RL MDL Unit Prepared Dil Fac Hg ND 0.066 0.016 ug/Sample 10/10/13 10:31 10/10/13 14:45 Method: 29/7470A - Mercury - Front Half Analyte Result Qualifier RL MDL Unit Analyzed Dil Fac Hg ND 0.030 0.0074 ug/Sample 10/16/13 09:19 10/16/13 11:41 Method: 29/7470A - Mercury - HCI Analyte Result Qualifier RL MDL Prepared Analyzed Dil Fac

Method: 29/7470A - Mercury - KMNO4 Analyte Result Qualifier RL MDL Unit Prepared Dil Fac Analyzed Hg ND 0.10 0.025 ug/Sample 10/10/13 10:29 10/10/13 13:46

0.10

0.025

ug/Sample

10/16/13 09:23

Method: 29/7470A - Mercury - Nitric/Peroxide Analyte Resuit Qualifier RL. MDL Unit Prepared Analyzed Dil Fac Hg ND 0.20 0.049 ug/Sample 10/10/13 10:25 10/10/13 14:14

Client Sample ID: 15-1 Lab Sample ID: 320-4473-6

0.051

Date Collected: 09/29/13 00:00 Date Received: 10/07/13 09:00

Hg

Sample Container: Amber Glass 500mL - unpreserved

Method: 0050/26A - HCI Analyte Result Qualifier Prepared Analyzed Dil Fac 350 21 Hydrochloric Acid Н 11 mg/sample 10/28/13 21:05 100

Matrix: Air

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-6

Matrix: Air

Matrix: Air

Matrix: Air

Matrix: Air

Client Sample ID: 15-1 Date Collected: 09/29/13 00:00

Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

General Chemistry Analyte	Result	Qualifier	RL	RL	Unit	D	Prepared	Analyzed	Dil Fac
Particulate Matter	0.0820		0.0005	0.0005	g			10/16/13 18:07	1
Particulate Matter	0.0235		0.0005	0.0005	g			10/21/13 11:37	1

Client Sample ID: I5-2 Lab Sample ID: 320-4473-7

Date Collected: 09/30/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

Method: 0050/26A - HCI Analyte Result Qualifier RL MDL Unit D Prepared Dil Fac Analyzed 11 Hydrochloric Acid 240 5.5 mg/sample 10/28/13 22:47 **General Chemistry** Analyte Result Qualifier RL RL Unit D Prepared Dil Fac Analyzed Particulate Matter 0.0532 0.0005 0.0005 g 10/16/13 09:42 0.0005 0.0005 g **Particulate Matter** 0.0141 10/21/13 11:37

Client Sample ID: 15-3 Lab Sample ID: 320-4473-8

Date Collected: 10/01/13 00:00

Date Received: 10/07/13 09:00

Sample Container: Amber Glass 500mL - unpreserved

Method: 0050/26A - HCI Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hydrochloric Acid	230		11	5.4	mg/sample			10/28/13 23:16	50
General Chemistry Analyte	Result	Qualifier	RL	RL	Unit	.D	Prepared	Analyzed	Dil Fac
Particulate Matter	0.0681	-	0.0005	0.0005	g			10/16/13 09:43	1
Particulate Matter	0.0165		0.0005	0.0005	g			10/23/13 10:23	1

Client Sample ID: 15-4 Lab Sample ID: 320-4473-9

Date Collected: 10/02/13 00:00

Date Received: 10/07/13 09:00

Method: 0050/26A - HCI

Sample Container: Amber Glass 500mL - unpreserved

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hydrochloric Acid	530		41	21	mg/sample			10/28/13 23:45	200
Γ-									
General Chemistry									
Analyte	Result	Qualifier	RL	RL	Unit	D	Prepared	Analyzed	Dil Fac
Particulate Matter	0.0922		0.0005	0.0005	g			10/16/13 18:08	1
Particulate Matter	0.0399		0.0005	0.0005	g			10/21/13 11:39	1

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100 Client Sample ID: I5-BLANK

Date Collected: 10/02/13 00:00

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-10

Matrix: Air

Matrix: Air

Matrix: Air

Matrix: Air

Date Received: 10/07/13 09:00 Sample Container: Amber Glass 500mL - unpreserved

I	Method: 0050/26A - HCI									
	Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
-	Hydrochloric Acid	ND		0.43	0.22	mg/sample			10/29/13 02:24	4

	General Chemistry Analyte	Result	Qualifier	RL	RL	Unit	D	Prepared	Analyzed	Dil Fac
-	Particulate Matter	0.0014		0.0005	0.0005	g			10/16/13 18:09	1
Į	Particulate Matter	0.0016		0.0005	0.0005	g			10/21/13 11:39	1

Client Sample ID: PEA1941 Lab Sample ID: 320-4473-11

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Ampule (PT sample)

Method: 0050/26A - Hydrogen Halide and Halogen Emissions/Stationary Sources (Mod)									
Analyte	Result C	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hydrochloric Acid	38		2.6	1.3	mg/sample			10/29/13 00:14	- 5

Client Sample ID: PEA1945 Lab Sample ID: 320-4473-12 Matrix: Air

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Amber Glass 125mL - unpreserved

Method: 29/6020 - Metals ICPMS (F	ront Half)								
Analyte	Result	Qualifier	RL.	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Cadmium	87		0.15	0.011	ug/Sample		10/15/13 15:52	10/17/13 19:32	1.
Lead	74	В	0.15	0.0099	ug/Sample		10/15/13 15:52	10/17/13 19:32	1

Client Sample ID: PEA1947 Lab Sample ID: 320-4473-13

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Amber Glass 125mL - unpreserved

Method: 29/7470A - Mercury - Fron	t Half								
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hg	6.0		0.24	0.059	ug/Sample		10/16/13 09:45	10/16/13 11:21	8

Client Sample ID: PEA1948 Lab Sample ID: 320-4473-14

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Plastic 250ml - unpreserved

Method: 29/6020 - Metals ICPMS (Back Half)									
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Cadmium	27		0.15	0.011	ug/Sample		10/11/13 10:02	10/17/13 18:44	1
Lead	31	В	0.15	0.0099	ug/Sample		10/11/13 10:02	10/17/13 18:44	1





















Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-15

Matrix: Air

Client Sample ID: PEA1950

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

Sample Container: Ampule (PT sample)

Method: 29/7470A - Mercury - Nitrio	c/Peroxide								
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hg	160		6.0	1.5	ug/Sample		10/10/13 10:25	10/10/13 14:18	3

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lient: AECOM, Inc. roject/Site: SMMI 60284905-2100			
lethod: 0050/26A - HCI			
16thou. 0030/20A - 1101		•	
Lab Sample ID: MB 320-28698/10-A			
Matrix: Air			
Analysis Batch: 28872			
	MB	MB	
Analyte	Result	Qualifier	RL
Hydrochloric Acid	ND		0.51
Lab Sample ID: MB 320-28698/1-A			
Matrix: Air			
Analysis Batch: 28872			
•	MB	MB	
Analyte	Result	Qualifier	RL
Hydrochloric Acid	ND		0.51
_ab Sample ID: LCS 320-28698/11-A			
Matrix: Air			

TestAmerica Job ID: 320-4473-1

Client Sample ID: Method Blank

Analyzed

10/29/13 01:26

Client Sample ID: Method Blank

Analyzed

10/28/13 20:07

Client Sample ID: Lab Control Sample

%Rec.

Limits

90 - 110

Prep Type: Total/NA

Prep Type: Total/NA

Prep Type: Total/NA

Dil Fac

Dil Fac

Client Sample ID: Lab Control Sample Prep Type: Total/NA

Lab Sample ID: 320-4473-6 MS

Lab Sample ID: LCS 320-28698/2-A

Matrix: Air

Hydrochloric Acid

Hydrochloric Acid

Matrix: Air

Analyte

Analysis Batch: 28872

Analysis Batch: 28872

Analyte Hydrochloric Acid

Matrix: Air Analysis Batch: 28872

Sample Sample Result Qualifier

Analyte Hydrochloric Acid

Lab Sample ID: 320-4473-6 MSD

Lab Sample ID: MB 320-27318/1-A Matrix: Air

Analysis Batch: 27898

мв мв Analyte Result Qualifier ND

Method: 29/6020 - Metals ICPMS (Back Half)

Cadmium Lead 0.164

MDL Unit 0.26 mg/sample

10.3

Spike

Added

Sample Sample

350 H

350 H

Result Qualifier

10.3

Spike

Added

211

Spike

Added

211

MDL Unit 0.26 mg/sample

CS LCS Qualifier 10.6

LCS LCS

MS MS

MSD MSD

573

Result Qualifier

MDL Unit

0.011 ug/Sample

0.0099 ug/Sample

573

Result Qualifier

10.3

Unit mg/sample

Result Qualifier Unit

mg/sample

Unit

Unit

mg/sample

mg/sample

%Rec 101

%Rec

%Rec

104

104

Prepared

Prepared

%Rec

103

Limits 90 - 110

%Rec.

Limits

Limits

75 - 125

75 - 125

%Rec.

Client Sample ID: 15-1 Prep Type: Total/NA

Client Sample ID: 15-1 Prep Type: Total/NA

%Rec. RPD

RPD

Limit

20

Client Sample ID: Method Blank Prep Type: Total/NA

Prep Batch: 27318

Prepared Analyzed Dil Fac 10/11/13 10:02 10/17/13 18:53 10/11/13 10:02 10/17/13 18:53

RL

0.15

0.15

QC Sample Results

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Client Sample ID: Method Blank

Client Sample ID: Method Blank

Prep Type: Total/NA

Prep Type: Total/NA

Prep Type: Total/NA

Prep Batch: 27602

Method: 29/6020 - Metals ICPMS (Back Half) (Continued)

Lab Sample ID: LCS 320-27318/2-A Client Sample ID: Lab Control Sample Matrix: Air Analysis Batch: 27898 LCS LCS Spike

Prep Batch: 27318 %Rec Analyte Added Result Qualifier %Rec Limits Cadmium 30.0 27.4 ug/Sample 91 79 - 110 Lead 30.0 31.3 ug/Sample 86 - 110 104

Method: 29/6020 - Metals ICPMS (Front Half)

Lab Sample ID: MB 320-27602/1-A Matrix: Air

Analysis Batch: 27898

MR MR

Analyte Result Qualifier Dil Fac RL MDL Unit Prepared Analyzed 0.15 Cadmium ND 0.011 ug/Sample 10/15/13 15:52 10/17/13 19:54 0.0111 J 0.0099 ug/Sample 10/15/13 15:52 10/17/13 19:54 Lead 0.15

Lab Sample ID: LCS 320-27602/2-A Client Sample ID: Lab Control Sample Matrix: Air Prep Type: Total/NA Analysis Batch: 27898 Prep Batch: 27602 LCS LCS Spike %Rec. Added Analyte Result Qualifier Unit %Rec Limits 30.0 Cadmium 29.0 ug/Sample 97 79 - 110 30.0 29.8 Lead ug/Sample 99 86 - 110

Method: 29/6020 - Metals (ICPMS), Stationary Source

Lab Sample ID: MB 320-27320/1-A

Matrix: Air

Lead

Analysis Batch: 28474

Prep Batch: 27320 мв мв Result Qualifier MDL Unit Analyte RL Prepared Analyzed Dil Fac Cadmium ND 0.30 0.022 ug/Sample 10/11/13 10:05 10/24/13 10:05 Lead 0.178 J 0.30 0.020 ug/Sample 10/11/13 10:05 10/24/13 10:05

Lab Sample ID: LCS 320-27320/2-A Client Sample ID: Lab Control Sample Matrix: Air Prep Type: Total/NA Analysis Batch: 28474 Prep Batch: 27320 Spike LCS LCS Analyte Added Result Qualifier Unit %Rec Limits Cadmium 60.0 56.2 ug/Sample 94 79 - 110

61.0

ug/Sample

102

86 _ 110

60 O

Lab Sample ID: 320-4471-A-1-E DU Client Sample ID: Duplicate Matrix: Air Prep Type: Total/NA Analysis Batch: 28474 Prep Batch: 27320 DU DU Sample Sample RPD Analyte Result Qualifier Result Qualifier Unit ח RPD Limit Cadmium 0.18 J 0.186 ug/Sample 20 1.0 B 1.03 ug/Sample Lead 0.2 20

Client: AECOM, Inc. Project/Site: SMMI 60284905-2100		Q	C Sam	ple f	Resu	lts	•		Tes	stAme	erica Job II	D: 320-	4473-1
Method: 29/7470A - Mercury - HCI													
Lab Sample ID: MB 320-27212/1-C									Clie	nt Sa	mple ID: I	Method	l Blank
Matrix: Air											Prep Ty	ype: To	otal/NA
Analysis Batch: 27715											Prep	Batch:	27639
		MB											
Analyte		Qualifier		RL		MDL U		D	Prepa		Analyz		Dil Fac
Hg	ND			0.20	(0.049 ug	g/Sample	10	0/16/13	09:23	10/16/13 1	1:58	1
Lab Sample ID: LCS 320-27212/2-C Matrix: Air								Clie	nt Saı	nple I	D: Lab Co Prep Ty		_
Analysis Batch: 27715											Prep	Batch	27639
			Spike		LCS	LCS					%Rec.		
Analyte			Added		Result	Qualific	er Unit		D %F	lec	Limits		
Hg			1.00	-	0.946		ug/Sam	ple		95	85 - 115		
Lab Sample ID: LCSD 320-27212/3-C Matrix: Air Analysis Batch: 27715			Spike		LCSD	LCSD	CI	ient Sa	ample	ID: La	ab Contro Prep Ty Prep %Rec.	ype: To	_
Analyte			Added		Result	Qualifie	er Unit		D %F	Rec	Limits	RPD	Limi
Hg			1.00		0.930		ug/Sam	ple		93	85 - 115	2	20
Method: 29/7470A - Mercury - Emp	oty												
Lab Sample ID: MB 320-27211/1-B Matrix: Air									Clie	nt Sa	mple ID: I Prep Ty		
Analysis Batch: 27274											Prep	Batch:	27219
	МВ	MB											
Analyte	Result	Qualifier		RL		MDL U		D	Prepar		Analyz		Dil Fac
Hg	ND			0.20	().049 uç	g/Sample	10	0/10/13	10:31	10/10/13 1	14:24	1
Lab Sample ID: LCS 320-27211/2-B								Clie	nt Sar	nple l	D: Lab Co	ntrol S	Sample
Matrix: Air											Prep Ty	ype: To	tal/NA
Analysis Batch: 27274											Prep	Batch	27219
			Spike		LCS	LCS					%Rec.		
Analyte			Added		Result	Qualifie	er Unit	I) %F	tec	Limits		
Hg			1.00		0.968		ug/Sam	ple		97	85 - 115		
							CI	ient Sa	ample	ID: La	ab Contro Prep Ty	-	-
Lab Sample ID: LCSD 320-27211/3-B Matrix: Air												,	
Matrix: Air											Pren	Batch	27219
,			Spike		LCSD	LCSD					Prep %Rec.	Batch	27219 RPE
Matrix: Air			Spike Added			LCSD Qualifie	er Unit	ı	O %F	Rec	•	Batch:	

Method: 29/7470A - Mercury - KMNO4

Lab Sample ID: MB 320-27212/1-B Matrix: Air Analysis Batch: 27274							Client Sa	mple ID: Metho Prep Type: 1 Prep Batcl	「otal/NA
	MB	MB							
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Hg	ND		0.20	0.049	ug/Sample		10/10/13 10:29	10/10/13 13:25	1

QC Sample Results

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Method: 29/7470A - Mercury - KMNO4 (Continued)

Lab Sample ID: LCS 320-27212/2-B Matrix: Air

Client Sample ID: Lab Control Sample

Prep Type: Total/NA Prep Batch: 27218

LCS LCS Spike Added Result Qualifier Limits Hg 1.00 ug/Sample

1.00

0.999

85 - 115

Lab Sample ID: LCSD 320-27212/3-B

Matrix: Air

Client Sample ID: Lab Control Sample Dup

Prep Type: Total/NA

Analysis Batch: 27274

Analysis Batch: 27274

Prep Batch: 27218 Spike LCSD LCSD RPD Added Result Qualifier Unit %Rec

10/16/13 09:19

ug/Sample

0.049 ug/Sample

Limits **RPD** Limit 85 - 115

Method: 29/7470A - Mercury - Front Half

Lab Sample ID: MB 320-27208/1-B

Matrix: Air

Analyte

Hg

Analyte

Hg

Analysis Batch: 27715

Client Sample ID: Method Blank

Prep Type: Total/NA Prep Batch: 27637

Dil Fac Prepared Analyzed

10/16/13 11:12

Lab Sample ID: LCS 320-27208/2-B

Matrix: Air

Analysis Batch: 27715

Client Sample ID: Lab Control Sample

Prep Type: Total/NA Prep Batch: 27637

Spike LCS LCS Added Analyte Result Qualifier Unit %Rec Limits Hg 1.00 0.938 85 _ 115 ug/Sample

Lab Sample ID: LCSD 320-27208/3-B

Matrix: Air

Analysis Batch: 27715

Client Sample ID: Lab Control Sample Dup

Prep Type: Total/NA

Prep Batch: 27637

Spike LCSD LCSD %Rec. RPD Analyte Added Result Qualifier %Rec Limits Limit 1.00 Hg 0.970 ug/Sample 85 - 115 3

0.20

Method: 29/7470A - Mercury - Nitric/Peroxide

Lab Sample ID: MB 320-27210/1-B

Matrix: Air

Analysis Batch: 27274

Client Sample ID: Method Blank

Prep Type: Total/NA

Prep Batch: 27213

MB MB

MR MR

ND

Result Qualifier

Analyte Result Qualifier Prepared Analyzed Hg ND 2.0 0.49 ug/Sample 10/10/13 10:24 10/10/13 13:49

Lab Sample ID: LCS 320-27210/2-B

Matrix: Air

Analysis Batch: 27274

Client Sample ID: Lab Control Sample

Prep Type: Total/NA

Prep Batch: 27213

Spike LCS LCS Analyte Added %Rec Result Qualifier Unit D Limits 10.0 ug/Sample Hg 10.0 100 85 _ 115

QC Sample Results

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

2

Method: 29/7470A - Mercury -	 Nitric/Peroxide ((Continued)

Lab Sample ID: 320-4473-2 MS			•	Client Sample ID: 129-2
Matrix: Air				Prep Type: Total/NA
Analysis Batch: 27274				Prep Batch: 27213
	Sample Sample	Spike	MS MS	%Rec.

Analyte	Result	Qualifier	Added	Result	Qualifier	Unit	D	%Rec	Limits		
Hg	1.2		4.75	5.89		ug/Sample	_	98	85 - 115		
Lab Sample ID: 320-4473-2 MSI	n								Client Se	mnla IT	1. 120

Lab Sample ID: 320-4473-2 MSD Matrix: Air									Client Sa Prep T	mple ID vpe: To	
Analysis Batch: 27274									Prep	Batch:	27213
•	Sample	Sample	Spike	MSD	MSD				%Rec.		RPD
Analyte	Result	Qualifier	Added	Result	Qualifier	Unit	D	%Rec	Limits	RPD	Limit
Hg	1.2		4.75	5.80		ug/Sample		96	85 - 115	2	20

Method: 5 - Particulate - Acetone

Lab Sample ID: MB 320-28266/6 Matrix: Air Analysis Batch: 28266							Client S	ample ID: Metho Prep Type: T	
, many one	MB	МВ							
Analyte	Result	Qualifier	RL	RL	Unit	D	Prepared	Analyzed	Dil Fac
Particulate Matter	ND		0.0005	0.0005	a			10/21/13 11:40	

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

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HPLC/IC

Pre Prep Batch: 28698

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-6	15-1	Total/NA	Air	Air Train Vol.	
320-4473-6 MS	I5-1	Total/NA	Air	Air Train Vol.	•
320-4473-6 MSD	15-1	Total/NA	Air	Air Train Vol.	
320-4473-7	15-2	Total/NA	Air	Air Train Vol.	
320-4473-8	15-3	Total/NA	Air	Air Train Vol.	
320-4473-9	15-4	Total/NA	Air	Air Train Vol.	
320-4473-10	I5-BLANK	Total/NA	Air	Air Train Vol.	
320-4473-11	PEA1941	Total/NA	Air	Air Train Vol.	
LCS 320-28698/11-A	Lab Control Sample	Total/NA	Air	Air Train Vol.	
LCS 320-28698/2-A	Lab Control Sample	Total/NA	Air	Air Train Vol.	
MB 320-28698/10-A	Method Blank	Total/NA	Air	Air Train Vol.	
MB 320-28698/1-A	Method Blank	Total/NA	Air	Air Train Vol.	

Analysis Batch: 28872

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-6	15-1	Total/NA	Air	0050/26A	28698
320-4473-6 MS	I5-1	Total/NA	Air	0050/26A	28698
320-4473-6 MSD	I5-1	Total/NA	Air	0050/26A	28698
320-4473-7	15-2	Total/NA	Air	0050/26A	28698
320-4473-8	15-3	Total/NA	Air	0050/26A	28698
320-4473-9	15-4	Total/NA	Air	0050/26A	28698
320-4473-10	15-BLANK	Total/NA	Air	0050/26A	28698
320-4473-11	PEA1941	Total/NA	Air	0050/26A	28698
LCS 320-28698/11-A	Lab Control Sample	Total/NA	Air	0050/26A	28698
LCS 320-28698/2-A	Lab Control Sample	Total/NA	Air	0050/26A	28698
MB 320-28698/10-A	Method Blank	Total/NA	Air	0050/26A	28698
MB 320-28698/1-A	Method Blank	Total/NA	Air	0050/26A	28698

Metals

Pre Prep Batch: 27208

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	Air Train Vol.	
320-4473-2	129-2	Total/NA	Air	Air Train Vol.	
320-4473-3	129-3	Total/NA	Air	Air Train Vol.	
320-4473-4	129-4	Total/NA	Air	Air Train Vol.	
320-4473-5	BLANK	Total/NA	Air	Air Train Vol.	
320-4473-13	PEA1947	Total/NA	Air	Air Train Vol.	
LCS 320-27208/2-B	Lab Control Sample	Total/NA	Air	Air Train Vol.	
LCSD 320-27208/3-B	Lab Control Sample Dup	Total/NA	Air	Air Train Vol.	
MB 320-27208/1-B	Method Blank	Total/NA	Air	Air Train Vol.	

Pre Prep Batch: 27210

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	Air Train Vol.	
320-4473-2	129-2	Total/NA	Air	Air Train Vol.	
320-4473-2 MS	129-2	Total/NA	Air	Air Train Vol.	
320-4473-2 MSD	129-2	Total/NA	Air	Air Train Vol.	
320-4473-3	129-3	Total/NA	Air	Air Train Vol.	
320-4473-4	129-4	Total/NA	Air	Air Train Vol.	

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

2

Metals (Continued)

Pre Prep Batch: 27210 (Continued)

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-5	BLANK	Total/NA	Air	Air Train Vol.	
320-4473-15	PEA1950	Total/NA	Air	Air Train Vol.	
LCS 320-27210/2-B	Lab Control Sample	Total/NA	Air	Air Train Vol.	
MB 320-27210/1-B	Method Blank	Total/NA	Air	Air Train Vol.	

Pre Prep Batch: 27211

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	Air Train Vol.	
320-4473-2	129-2	Total/NA	Air	Air Train Vol.	
320-4473-3	129-3	Total/NA	Air	Air Train Vol.	
320-4473-4	129-4	Total/NA	Air	Air Train Vol.	
320-4473-5	BLANK	Total/NA	Air	Air Train Vol.	
LCS 320-27211/2-B	Lab Control Sample	Total/NA	Air	Air Train Vol.	
LCSD 320-27211/3-B	Lab Control Sample Dup	Total/NA	Air	Air Train Vol.	
MB 320-27211/1-B	Method Blank	Total/NA	Air	Air Train Vol.	

Pre Prep Batch: 27212

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	Air Train Vol.	
320-4473-2	129-2	Total/NA	Air	Air Train Vol.	
320-4473-3	129-3	Total/NA	Air-	Air Train Vol.	
320-4473-4	129-4	Total/NA	Air	Air Train Vol.	
320-4473-5	BLANK	Total/NA	Air	Air Train Vol.	
LCS 320-27212/2-B	Lab Control Sample	Total/NA	Air	Air Train Vol.	
LCS 320-27212/2-C	Lab Control Sample	Total/NA	Air	Air Train Vol.	
LCSD 320-27212/3-B	Lab Control Sample Dup	Total/NA	Air	Air Train Vol.	
LCSD 320-27212/3-C	Lab Control Sample Dup	Total/NA	Air	Air Train Vol.	
MB 320-27212/1-B	Method Blank	Total/NA	Air	Air Train Vol.	
MB 320-27212/1-C	Method Blank	Total/NA	Air	Air Train Vol.	

Prep Batch: 27213

Top Batom, 27210	F = ******* = 1 = 1 = 1 = 1 = 1 = 1 = 1 =							
Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch			
320-4473-1	129-1	Total/NA	Air	AT Prep (BH)	27210			
320-4473-2	129-2	Total/NA	Air	AT Prep (BH)	27210			
320-4473-2 MS	129-2	Total/NA	Air	AT Prep (BH)	27210			
320-4473-2 MSD	129-2	Total/NA	Air	AT Prep (BH)	27210			
320-4473-3	129-3	Total/NA	Air	AT Prep (BH)	27210			
320-4473-4	129-4	Total/NA	Air	AT Prep (BH)	27210			
320-4473-5	BLANK	Total/NA	Air	AT Prep (BH)	27210			
320-4473-15	PEA1950	Total/NA	Air	AT Prep (BH)	27210			
LCS 320-27210/2-B	Lab Control Sample	Total/NA	Air	AT Prep (BH)	27210			
MB 320-27210/1-B	Method Blank	Total/NA	Air	AT Prep (BH)	27210			
-								

Prep Batch: 27218

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	AT Prep (Per)	27212
320-4473-2	129-2	Total/NA	Air	AT Prep (Per)	27212
320-4473-3	129-3	Total/NA	Air	AT Prep (Per)	27212
320-4473-4	129-4	Total/NA	Air	AT Prep (Per)	27212
320-4473-5	BLANK	Total/NA	Air	AT Prep (Per)	27212
LCS 320-27212/2-B	Lab Control Sample	Total/NA	Air	AT Prep (Per)	27212

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1







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Metals (Continued)

Prep Batch: 27218 (Continued)

-	Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
-	LCSD 320-27212/3-B	Lab Control Sample Dup	Total/NA	Air	AT Prep (Per)	27212
-	MB 320-27212/1-B	Method Blank	Total/NA	Air	AT Prep (Per)	27212

Prep Batch: 27219

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	AT Prep (Empty)	27211
320-4473-2	129-2	Total/NA	Air	AT Prep (Empty)	27211
320-4473-3	129-3	Total/NA	Air	AT Prep (Empty)	27211
320-4473-4	129-4	Total/NA	Air	AT Prep (Empty)	27211
320-4473-5	BLANK	Total/NA	Air	AT Prep (Empty)	27211
LCS 320-27211/2-B	Lab Control Sample	Total/NA	Air	AT Prep (Empty)	27211
LCSD 320-27211/3-B	Lab Control Sample Dup	Total/NA	Air	AT Prep (Empty)	27211
MB 320-27211/1-B	Method Blank	Total/NA	Air	AT Prep (Empty)	27211

Analysis Batch: 27274

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batcl
320-4473-1	129-1	Total/NA	Air	29/7470A	27218
320-4473-1	129-1	Total/NA	Air	29/7470A	27213
320-4473-1	129-1	Total/NA	Air	29/7470A	27219
320-4473-2	129-2	Total/NA	Air	29/7470A	27218
320-4473-2	129-2	Total/NA	Air	29/7470A	27213
320-4473-2	129-2	Total/NA	Air	29/7470A	27219
320-4473-2 MS	129-2	Total/NA	Air	29/7470A	27213
320-4473-2 MSD	129-2	Total/NA	Air	29/7470A	27213
320-4473-3	129-3	Total/NA	Air	29/7470A	27218
320-4473-3	129-3	Total/NA	Air	29/7470A	27213
320-4473-3	129-3	Total/NA	Air	29/7470A	27219
320-4473-4	129-4	Total/NA	Air	29/7470A	27218
320-4473-4	129-4	Total/NA	Air	29/7470A	27213
320-4473-4	129-4	Total/NA	Air	29/7470A	27219
320-4473-5	BLANK	Total/NA	Air	29/7470A	27218
320-4473-5	BLANK	Tota!/NA	Air	29/7470A	27213
320-4473-5	BLANK	Total/NA	Air	29/7470A	27219
320-4473-15	PEA1950	Total/NA	Air	29/7470A	27213
LCS 320-27210/2-B	Lab Control Sample	Total/NA	Air	29/7470A	27213
LCS 320-27211/2-B	Lab Control Sample	Total/NA	Air	29/7470A	27219
LCS 320-27212/2-B	Lab Control Sample	Total/NA	Air	29/7470A	27218
LCSD 320-27211/3-B	Lab Control Sample Dup	Total/NA	Air	29/7470A	27219
LCSD 320-27212/3-B	Lab Control Sample Dup	Total/NA	Air	29/7470A	27218
MB 320-27210/1-B	Method Blank	Total/NA	Air	29/7470A	27213
MB 320-27211/1-B	Method Blank	Total/NA	Air	29/7470A	27219
MB 320-27212/1-B	Method Blank	Total/NA	Air	29/7470A	27218

Prep Batch: 27318

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method Prep Batch
320-4473-14	PEA1948	Total/NA	Air	Air Train Prep
LCS 320-27318/2-A	Lab Control Sample	Total/NA	Air	Air Train Prep
MB 320-27318/1-A	Method Blank	Total/NA	Air	Air Train Prep

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

9)

















Metals (Continued)

Prep Batch: 27320

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4471-A-1-E DU	Duplicate	Total/NA	Air	Air Train Prep	-
320-4473-1	129-1	Total/NA	Air	Air Train Prep	
320-4473-2	129-2	Total/NA	Air	Air Train Prep	
320-4473-3	129-3	Total/NA	Air	Air Train Prep	
320-4473-4	129-4	Total/NA	Air	Air Train Prep	
320-4473-5	BLANK	Total/NA	Air	Air Train Prep	
LCS 320-27320/2-A	Lab Control Sample	Total/NA	Air	Air Train Prep	
MB 320-27320/1-A	Method Blank	Total/NA	Air	Air Train Prep	

Prep Batch: 27602

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-12	PEA1945	Total/NA	Air	Air Tain Prep	
LCS 320-27602/2-A	Lab Control Sample	Total/NA	Air	Air Tain Prep	•
MB 320-27602/1-A	Method Blank	Total/NA	Air	Air Tain Prep	

Prep Batch: 27637

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	AT Hg Prep (FH)	27208
320-4473-2	129-2	Total/NA	Air	AT Hg Prep (FH)	27208
320-4473-3	129-3	Total/NA	Air	AT Hg Prep (FH)	27208
320-4473-4	129-4	Total/NA	Air	AT Hg Prep (FH)	27208
320-4473-5	BLANK	Total/NA	Air	AT Hg Prep (FH)	27208
320-4473-13	PEA1947	Total/NA	Air	AT Hg Prep (FH)	27208
LCS 320-27208/2-B	Lab Control Sample	Total/NA	Air	AT Hg Prep (FH)	27208
LCSD 320-27208/3-B	Lab Control Sample Dup	Total/NA	Air	AT Hg Prep (FH)	27208
MB 320-27208/1-B	Method Blank	Total/NA	Air	AT Hg Prep (FH)	27208

Prep Batch: 27639

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	AT (HCI)	27212
320-4473-2	129-2	Total/NA	Air	AT (HCI)	27212
320-4473-3	129-3	Total/NA	Air	AT (HCI)	27212
320-4473-4	129-4	Total/NA	Air	AT (HCI)	27212
320-4473-5	BLANK	Total/NA	Air	AT (HCI)	27212
LCS 320-27212/2-C	Lab Control Sample	Total/NA	Air	AT (HCI)	27212
LCSD 320-27212/3-C	Lab Control Sample Dup	Total/NA	Air	AT (HCI)	27212
MB 320-27212/1-C	Method Blank	Total/NA	Аiг	AT (HCI)	27212

Analysis Batch: 27715

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-1	129-1	Total/NA	Air	29/7470A	27637
320-4473-1	129-1	Total/NA	Air	29/7470A	27639
320-4473-2	129-2	Total/NA	Air	29/7470A	27637
320-4473-2	129-2	Total/NA	Air	29/7470A	27639
320-4473-3	129-3	Total/NA	Air	29/7470A	27637
320-4473-3	129-3	Total/NA	Air	29/7470A	27639
320-4473-4	129-4	Total/NA	Air	29/7470A	27637
320-4473-4	129-4	Total/NA	Air	29/7470A	27639
320-4473-5	BLANK	Total/NA	Air	29/7470A	27637
320-4473-5	BLANK	Total/NA	Air	29/7470A	27639
320-4473-13	PEA1947	Total/NA	Air	29/7470A	27637

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

22

Metals (Continued)

Analysis Batch: 27715 (Continued)

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch	
LCS 320-27208/2-B	Lab Control Sample	Total/NA	Air	29/7470A	27637	
LCS 320-27212/2-C	Lab Control Sample	Total/NA	Air	29/7470A	27639	
LCSD 320-27208/3-B	Lab Control Sample Dup	Total/NA	Air	29/7470A	27637	
LCSD 320-27212/3-C	Lab Control Sample Dup	Total/NA	Air	29/7470A	27639	
MB 320-27208/1-B	Method Blank	Total/NA	Air	29/7470A	27637	
MB 320-27212/1-C	Method Blank	Total/NA	Air	29/7470A	27639	

Analysis Batch: 27898

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-12	PEA1945	Total/NA	Air	29/6020	27602
320-4473-14	PEA1948	Total/NA	Air	29/6020	27318
LCS 320-27318/2-A	Lab Control Sample	Tota!/NA	Air	29/6020	27318
LCS 320-27602/2-A	Lab Control Sample	Total/NA	Air	29/6020	27602
MB 320-27318/1-A	Method Blank	Total/NA	Air	29/6020	27318
MB 320-27602/1-A	Method Blank	Total/NA	Air	29/6020	27602

Analysis Batch: 28474

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4471-A-1-E DU	Duplicate	Total/NA	Air	29/6020	27320
320-4473-1	129-1	Total/NA	Air	29/6020	27320
320-4473-2	129-2	Total/NA	Air	29/6020	27320
320-4473-3	129-3	Total/NA	Air	29/6020	27320
320-4473-4	129-4	Total/NA	Air	29/6020	27320
320-4473-5	BLANK	Total/NA	Air	29/6020	27320
LCS 320-27320/2-A	Lab Control Sample	Total/NA	Air	29/6020	27320
MB 320-27320/1-A	Method Blank	Total/NA	Air	29/6020	27320

General Chemistry

Analysis Batch: 28259

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-6	I5-1	Total/NA	Air	5	
320-4473-7	15-2	Total/NA	Air	5	
320-4473-8	15-3	Total/NA	Air	5	
320-4473-9	15-4	Total/NA	Air	5	
320-4473-10	I5-BLANK	Total/NA	Air	5	

Analysis Batch: 28266

Lab Sample ID	Client Sample ID	Prep Type	Matrix	Method	Prep Batch
320-4473-6	15-1	Total/NA	Air	5	
320-4473-7	15-2	Total/NA	Air	5	
320-4473-8	15-3	Total/NA	Air	5	
320-4473-9	15-4	Total/NA	Air	5	
320-4473-10	I5-BLANK	Total/NA	Air	5	
MB 320-28266/6	Method Blank	Total/NA	Air	5	

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

Client Sample ID: 129-1 Date Collected: 09/29/13 00:00 Date Received: 10/07/13 09:00 TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-1	
Madulus, Alia	MY INCH

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Pre Prep	Air Train Vol.			1.0 Sample	500 mL	27212	10/10/13 10:20	CV1	TAL SAC
Total/NA	Prep	AT Prep (Per)			30 mL	30 mL	27218	10/10/13 10:29	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27274	10/10/13 13:35	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	402 mL	27210	10/10/13 10:15	CV1	TAL SAC
Total/NA	Prep	AT Prep (BH)			3 mL	30 mL	27213	10/10/13 10:24	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 13:59	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	102 mL	27211	10/10/13 10:18	CV1	TAL SAC
Total/NA	Prep	AT Prep (Empty)			3 mL	30 mL	27219	10/10/13 10:31	CV1	TAL SAC
Total/NA	Analysis	29/7470A		. 1	3 mL	30 mL	27274	10/10/13 14:34	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	150 mL	27208	10/10/13 10:13	CV1	TAL SAC
Total/NA	Prep	AT Hg Prep (FH)			30 mL	30 mL	27637	10/16/13 09:19	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 11:29	CV1	TAL SAC
Total/NA	Prep	AT (HCI)			30 mL	30 mL	27639	10/16/13 09:23	CV1	TAL SAC
Total/NA	Analysis	29/7470A		. 1	30 mL	30 mL	27715	10/16/13 12:10	CV1	TAL SAC
Total/NA	Prep	Air Train Prep			1 Sample	349.6688741 72185 mL	27320	10/11/13 10:05	CV1	TAL SAC
Total/NA	Analysis	29/6020		1	1 Sample	349.6688741 72185 mL	28474	10/24/13 11:45	SAH	TAL SAC

Client Sample ID: 129-2

Date Collected: 09/30/13 00:00 Date Received: 10/07/13 09:00

Lab Sample ID: 320-4473-2

Matrix: Air

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Prep	AT Prep (Per)			30 mL	30 mL	27218	10/10/13 10:29	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27274	10/10/13 13:37	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	475 mL	27210	10/10/13 10:15	CV1	TAL SAC
Total/NA	Prep	AT Prep (BH)			3 mL	30 mL	27213	10/10/13 10:24	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 14:01	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	107 mL	27211	10/10/13 10:18	CV1	TAL SAG
Total/NA	Prep	AT Prep (Empty)			3 mL	30 mL	27219	10/10/13 10:31	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 14:39	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	150 mL	27208	10/10/13 10:13	CV1	TAL SAC
Total/NA	Prep	AT Hg Prep (FH)			30 mL	30 mL	27637	10/16/13 09:19	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 11:31	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1.0 Sample	500 mL	27212	10/10/13 10:20	CV1	TAL SAC
Total/NA	Prep	AT (HCI)			30 mL	30 mL	27639	10/16/13 09:23	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 12:11	CV1	TAL SAC
Total/NA	Prep	Air Train Prep			1 Sample	340 mL	27320	10/11/13 10:05	CV1	TAL SAG
Total/NA	Analysis	29/6020		1	1 Sample	340 mL	28474	10/24/13 11:41	SAH	TAL SA

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-3

Matrix: Air

Client Sample ID: I29-3

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Tota!/NA	Pre Prep	Air Train Vol.			1.0 Sample	500 mL	27212	10/10/13 10:20	CV1	TAL SAC
Total/NA	Prep	AT Prep (Per)			30 mL	30 mL	27218	10/10/13 10:29	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27274	10/10/13 13:39	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	475 mL.	27210	10/10/13 10:15	CV1	TAL SAC
Total/NA	Prep	AT Prep (BH)			3 mL	30 mL	27213	10/10/13 10:25	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 14:10	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	107 mL	27211	10/10/13 10:18	CV1	TAL SAC
Total/NA	Prep	AT Prep (Empty)			3 mL	30 mL	27219	10/10/13 10:31	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 14:42	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	150 mL	27208	10/10/13 10:13	CV1	TAL SAC
Total/NA	Prep	AT Hg Prep (FH)			30 mL	30 mL	27637	10/16/13 09:19	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 11:38	CV1	TAL SAC
Total/NA	Prep	AT (HCI)			30 mL	30 mL	27639	10/16/13 09:23	CV1	TAL SAC
Total/NA	Analysis	· 29/7470A		1	30 mL	30 mL	27715	10/16/13 12:16	CV1	TAL SAC
Total/NA	Prep	Air Train Prep			1 Sample	340 mL	27320	10/11/13 10:05	CV1	TAL SAC
Total/NA	Analysis	29/6020		1	1 Sample	340 mL	28474	10/24/13 11:37	SAH	TAL SAC

Client Sample ID: 129-4

Date Collected: 10/02/13 00:00 Date Received: 10/07/13 09:00 Lab Sample ID: 320-4473-4

Matrix: Air

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Туре	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Prep	AT Prep (Per)			30 mL	30 mL	27218	10/10/13 10:29	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27274	10/10/13 13:41	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.	•		1 Sample	475 mL	27210	10/10/13 10:15	CV1	TAL SAC
Total/NA	Prep ·	AT Prep (BH)			3 mL	30 mL	27213	10/10/13 10:25	CV1	TAL SAC
Total/NA	Analysis	29/7470A		. 1	3 mL	30 mL	27274	10/10/13 14:12	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	101 mL	27211	10/10/13 10:18	CV1	TAL SAC
Total/NA	Prep	AT Prep (Empty)			3 mL	30 mL	27219	10/10/13 10:31	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 14:43	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	150 mL	27208	10/10/13 10:13	CV1	TAL SAC
Total/NA	Prep	AT Hg Prep (FH)			30 mL	30 mL	27637	10/16/13 09:19	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 11:39	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1.0 Sample	500 mL	27212	10/10/13 10:20	CV1	TAL SAC
Total/NA	Prep	AT (HCI)			30 mL	30 mL	27639	10/16/13 09:23	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 12:18	CV1	TAL SAC
Total/NA	Prep	Air Train Prep			1 Sample	340 mL	27320	10/11/13 10:05	CV1	TAL SAC
Total/NA	Analysis	29/6020		1	1 Sample	340 mL	28474	10/24/13 11:34	SAH	TAL SAC

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-5

Matrix: Air

Client Sample ID: BLANK

Date Collected: 10/02/13 00:00 Date Received: 10/07/13 09:00

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Prep	AT Prep (Per)			30 mL	30 mL	27218	10/10/13 10:29	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27274	10/10/13 13:46	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	99 mL	27210	10/10/13 10:15	CV1	TAL SAC
Total/NA	Prep	AT Prep (BH)			3 mL	30 mL	27213	10/10/13 10:25	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 14:14	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	33 mL	27211	10/10/13 10:18	CV1	TAL SAC
Total/NA	Prep	AT Prep (Empty)			3 mL	30 mL	27219	10/10/13 10:31	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	3 mL	30 mL	27274	10/10/13 14:45	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	150 mL	27208	10/10/13 10:13	CV1	TAL SAC
Total/NA	Prep	AT Hg Prep (FH)			30 mL	30 mL	27637	10/16/13 09:19	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 11:41	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1.0 Sample	500 mL	27212	10/10/13 10:20	CV1	TAL SAC
Total/NA	Prep	AT (HCI)			30 mL	30 mL	27639	10/16/13 09:23	CV1	TAL SAC
Total/NA	Analysis	29/7470A		1	30 mL	30 mL	27715	10/16/13 12:20	CV1	TAL SAC
Total/NA	Prep	Air Train Prep			1 Sample	375 mL	27320	10/11/13 10:05	CV1	TAL SAC
Total/NA	Analysis	29/6020		1	1 Sample	375 mL	28474	10/24/13 11:30	SAH	TAL SAC

Client Sample ID: 15-1

Date Collected: 09/29/13 00:00 Date Received: 10/07/13 09:00 Lab Sample ID: 320-4473-6

Matrix: Air

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Pre Prep	Air Train Vol.			1 Sample	410 mL	28698	10/18/13 10:30	LW1	TAL SAC
Total/NA	Analysis	0050/26A		100			28872	10/28/13 21:05	JCB	TAL SAC
Total/NA	Analysis	5		1			28259	10/16/13 18:07	SKV	TAL SAC
Total/NA	Analysis	5		1			28266	10/21/13 11:37	SKV	TAL SAC

Client Sample ID: 15-2
Date Collected: 09/30/13 00:00

Date Received: 10/07/13 09:00

Lab Sample ID: 320-4473-7

Matrix: Air

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Туре	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Pre Prep	Air Train Vol.			1 Sample	430 mL	28698	10/18/13 10:30	LW1	TAL SAC
Total/NA	Analysis	0050/26A		50			28872	10/28/13 22:47	JCB	TAL SAC
Total/NA	Analysis	5		1			28259	10/16/13 09:42	SKV	TAL SAC
Total/NA	Analysis	5		1			28266	10/21/13 11:37	SKV	TAL SAC

Client Sample ID: 15-3

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00 Lab Sample ID: 320-4473-8

Matrix: Air

Dil Initial Final Batch Batch Batch Prepared Prep Type Type Method Run Factor Amount Amount Number or Analyzed Analyst Total/NA Pre Prep Air Train Vol. 1 Sample 420 mL 28698 10/18/13 10:30 LW1 TAL SAC

TestAmerica Sacramento

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Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-8

Matrix: Air

Matrix: Air

Client Sample ID: I5-3 Lab Sa
Date Collected: 10/01/13 00:00

Date Received: 10/07/13 09:00

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Туре	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Analysis	0050/26A		50			28872	10/28/13 23:16	JCB	TAL SAC
Total/NA	Analysis	5		· 1			28259	10/16/13 09:43	SKV	TAL SAC
Total/NA	Analysis	5		1			28266	10/23/13 10:23	SKV	TAL SAC

Client Sample ID: 15-4 Lab Sample ID: 320-4473-9

Date Collected: 10/02/13 00:00 Date Received: 10/07/13 09:00

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Pre Prep	Air Train Vol.			1 Sample	400 mL	28698	10/18/13 10:30	LW1	TAL SAC
Tota!/NA	Analysis	0050/26A		200			28872	10/28/13 23:45	JCB	TAL SAC
Total/NA	Analysis	5		1			28259	10/16/13 18:08	skv	TAL SAC
Total/NA	Analysis	5		· 1			28266	10/21/13 11:39	SKV	TAL SAC

Client Sample ID: I5-BLANK

Date Collected: 10/02/13 00:00

Lab Sample ID: 320-4473-10

Matrix: Air

Date Collected: 10/02/13 00:00 Date Received: 10/07/13 09:00

Prep Type	Batch Type	Batch Method	Run	Dil Factor	Initial Amount	Final Amount	Batch Number	Prepared or Analyzed	Analyst	l ab
l			i\uii	- racioi	Amount		- Hullibei	OI Allalyzeu	Analyst	_ Lab
Total/NA	Pre Prep	Air Train Vol.			1 Sample	210 mL	28698	10/18/13 10:30	LW1	TAL SAC
Total/NA	Analysis	0050/26A		4			28872	10/29/13 02:24	JCB	TAL SAC
Total/NA	Analysis	5		1			28259	10/16/13 18:09	SKV	TAL SAC
Total/NA	Analysis	5		1			28266	10/21/13 11:39	SKV	TAL SAC

Client Sample ID: PEA1941 Lab Sample ID: 320-4473-11
Date Collected: 10/01/13 00:00 Matrix: Air

Date Received: 10/07/13 09:00

·										
	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Туре	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Pre Prep	Air Train Vol.			1 Sample	1000 mL	28698	10/18/13 10:30	LW1	TAL SAC
Total/NA	Analysis	0050/26A		5			28872	10/29/13 00:14	JCB	TAL SAC

Client Sample ID: PEA1945

Date Collected: 10/01/13 00:00

Lab Sample ID: 320-4473-12

Matrix: Air

Date Received: 10/07/13 09:00

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Prep	Air Tain Prep			1 Sample	150 mL	27602	10/15/13 15:52	CV1	TAL SAC
Totai/NA	Analysis	29/6020		1	1 Sample	150 mL	27898	10/17/13 19:32	AMC	TAL SAC

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

Client Sample ID: PEA1947

TestAmerica Job ID: 320-4473-1

Lab Sample ID: 320-4473-13

Matrix: Air

Date Collected: 10/01/13 00:00 Date Received: 10/07/13 09:00

	Batch	Batch		Dil	Initial	Final	Batch	Prepared	,	
Prep Type	Type	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Pre Prep	Air Train Vol.			1 Sample	150 mL	27208	10/14/13 16:18	CV1	TAL SAC
Total/NA	Prep	AT Hg Prep (FH)			30 mL	30 mL	27637	10/16/13 09:45	CV1	TAL SAC
Total/NA	Analysis	29/7470A		8	30 mL	30 mL	27715	10/16/13 11:21	CV1	TAL SAC

Client Sample ID: PEA1948 Lab Sample ID: 320-4473-14 Date Collected: 10/01/13 00:00

Matrix: Air

Date Received: 10/07/13 09:00

•	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Туре	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Prep	Air Train Prep			1 L	150 mL	27318	10/11/13 10:02	CV1	TAL SAC
Total/NA	Analysis	29/6020		1	1 L	150 mL	27898	10/17/13 18:44	AMC	TAL SAC

Client Sample ID: PEA1950 Lab Sample ID: 320-4473-15

Date Collected: 10/01/13 00:00 Matrix: Air

Date Received: 10/07/13 09:00

	Batch	Batch		Dil	Initial	Final	Batch	Prepared		
Prep Type	Туре	Method	Run	Factor	Amount	Amount	Number	or Analyzed	Analyst	Lab
Total/NA	Prep	AT Prep (BH)			3 mL	30 mL	27213	10/10/13 10:25	CV1	TAL SAC
Total/NA	Pre Prep	Air Train Vol.			1 Sample	1000 mL	27210	10/10/13 13:18	CV1	TAL SAC
Total/NA	Analysis	29/7470A		3	3 mL	30 mL	27274	10/10/13 14:18	CV1	TAL SAC

Laboratory References:

TAL SAC = TestAmerica Sacramento, 880 Riverside Parkway, West Sacramento, CA 95605, TEL (916)373-5600

Certification Summary

Client: AECOM, Inc.

Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

Laboratory: TestAmerica Sacramento

All certifications held by this laboratory are listed. Not all certifications are applicable to this report.

Authority	Program	EPA Region	Certification ID	Expiration Date
A2LA	A2LA		NE-OS-22-13	01-31-14
A2LA	DoD ELAP		2928-01	01-31-14
Alaska (UST)	State Program	10	UST-055	12-18-13
Arizona	State Program	9	AZ0708	08-11-14
Arkansas DEQ	State Program	6	88-0691	06-17-14
California	NELAP	9	1119CA	01-31-14
Connecticut	State Program	1	PH-0691	06-30-15
Florida	NELAP	4	E87570	06-30-14
Guam	State Program	9	N/A	08-31-14
Hawaii	State Program	9	N/A	01-31-14
Illinois	NELAP	5	200060	03-17-14
Kansas	NELAP	7	E-10375	10-31-14
Louisiana	NELAP	6	30612	06-30-14
Michigan	State Program	5	9947	01-31-14
Nebraska	State Program	7	NE-OS-22-13	01-31-14
Nevada	State Program	9	CA44	07-31-14
New Jersey	NELAP	2	CA005	06-30-14
New York	NELAP	2 .	11666	04-01-14
Northern Mariana Islands	State Program	9	MP0007	02-01-14
Oregon	NELAP	10	CA200005	03-28-14
Pennsylvania	NELAP	3 .	68-01272	03-31-14
South Carolina	State Program	4	87014	06-30-14
Texas	NELAP	6	T104704399-08-TX	05-31-14
US Fish & Wildlife	Federal		LE148388-0	12-31-13
USDA	Federal		P330-11-00436	12-30-14
USEPA UCMR	Federal	1 '	CA00044	11-06-14
Utah	NELAP	8	QUAN1	01-31-14
Washington	State Program	10	C581	05-05-14
West Virginia	State Program	3	9930C	12-31-13
Wyoming	State Program	8	8TMS-Q	01-31-14























Method Summary

Client: AECOM, Inc.

Method

0050/26A

0050/26A

29/6020

29/6020

29/6020

29/7470A

29/7470A

29/7470A

29/7470A

29/7470A

Protocol References:

Laboratory References:

5

Project/Site: SMMI 60284905-2100

Method Description

Metals (ICPMS), Stationary Source

Metals ICPMS (Back Half)

Metals ICPMS (Front Half)

Mercury - Nitric/Peroxide

Mercury - KMNO4

Mercury - Empty

Mercury - HCI

EPA = US Environmental Protection Agency

Mercury - Front Half

Particulate - Filter

Particulate - Acetone

Hydrogen Halide and Halogen Emissions/Stationary Sources (Mod)

TAL SAC = TestAmerica Sacramento, 880 Riverside Parkway, West Sacramento, CA 95605, TEL (916)373-5600

TestAmerica Job ID: 320-4473-1

Laboratory

TAL SAC

TAL SAC

TAL SAC

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Sample Summary

Client: AECOM, Inc. Project/Site: SMMI 60284905-2100

TestAmerica Job ID: 320-4473-1

VALUE N.S.N.S.N.S.N.S.N.S.N.S.
-22

Lab Sample ID	Client Sample ID	Matrix	Collected	Received
320-4473-1	129-1	Air	09/29/13 00:00	10/07/13 09:00
320-4473-2	129-2	Air	09/30/13 00:00	10/07/13 09:00
320-4473-3	129-3	Air	10/01/13 00:00	10/07/13 09:00
320-4473-4	129-4	Air	10/02/13 00:00	10/07/13 09:00
320-4473-5	BLANK	Air	10/02/13 00:00	10/07/13 09:00
320-4473-6	l5-1	Air	09/29/13 00:00	10/07/13 09:00
320-4473-7	15-2	Air	09/30/13 00:00	10/07/13 09:00
320-4473-8	15-3	Air	10/01/13 00:00	10/07/13 09:00
320-4473-9	15-4	Air	10/02/13 00:00	10/07/13 09:00
320-4473-10	I5-BLANK	Air	10/02/13 00:00	10/07/13 09:00
320-4473-11	PEA1941	Air	10/01/13 00:00	10/07/13 09:00
320-4473-12	PEA1945	Air	10/01/13 00:00	10/07/13 09:00
320-4473-13	PEA1947	Air	10/01/13 00:00	10/07/13 09:00
320-4473-14	PEA1948	Air	10/01/13 00:00	10/07/13 09:00
320-4473-15	PEA1950	Air	10/01/13 00:00	10/07/13 09:00

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1601 Prospect Parkway, Fort Collins, CO 80525 AECOM Environment 05-2100

<u>www.аесот.сот</u>

970) 493-8878 Phone * (970) 493-0213 Fax

Project Name: SMMI	Project Number:		60284905-2100			Analysis Required	ired		
Send Report To: John Rosburg	Sampler (Print Name):		John Rosburg					G. G.	, T
Address: 20325 Moss Bend Ct	Sampler (Print Name):		Doug Bopray)))	5
Lutz, FL 33558	Shipment Method:		FED EX						
	Airbill Number								
Phone: (970) 219-4904	Laboratory Receiving:		TestAmerica					Purchase Order No.	der No 49212
Fax: (813) 948-7333									
Field Sample ID	Sample Date	Sample Time	Sample Matrix	Number of Containers	Mercu	рвет		Comments, Special	Lab Sample ID (to
129-1, Container 1	09/29/13		Filter	-	×				combicted by idb/
129-1, Container 3	09/29/13		0.1 N HNO ₃	-	×				
129-1, Container 4	09/29/13		H ₂ O ₂ /HNO ₃	2	×		-		
I29-1, Container 5	09/29/13		0.1 N HNO ₃	-	×				
129-1, Container 6	09/29/13	,	Acidified KMnO ₄	-	×				
129-2, Container 1	09/30/13	_	Filter	-	×				
129-2, Container 3	09/30/13)	0.1 N HNO ₃	-	×				
129-2, Container 4	09/30/13		H ₂ O ₂ /HNO ₃	2	×				
129-2, Container 5	09/30/13		0.1 N HNO ₃	-	×××				
129-2, Container 6	09/30/13	4	Acidified KMnO ₄	-	×				
129-3, Container 1	10/1/2013		Filter	-	×				
129-3, Container 3	10/1/2013		0.1 N HNO ₃	_	×				
129-3, Container 4	10/1/2013		H ₂ O ₂ /HNO ₃	2	×××				
129-3, Container 5	10/1/2013		0.1 N HNO ₃	-	×				
129-3, Container 6	10/1/2013	,	Acidified KMnO ₄	-	×				
gnature)	uc.				آ ي ي	Sample Custodian Re	Sample Custodian Remarks (Completed By Laboratory):	aboratory);	-
Doug Bopray 10/4/2013 9:00	Malall			10/7/13	100	QA/QC Level	Turnaround	Samp	Sample Receipt
Relinquished by: (Signature)	Received by: (Sig#ature)	â		Date:	Time:	Level	Routine	Total # Containers Received?	d?
Relinquished by: (Signature)	Received by: (Signature)	(a)		Date:	Time:		24 Hour	COC Seals Intact?	
						Gher C		Received Containers Intact?	2
White: Lab Copy Yellow: PM Copy	Pink: Field Copy		Gold: PM/QA/QC Copy						

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60284905-2100

AECOM Environment 1601 Prospect Parkway, For Colilins, CO 80525 970) 493-8878 Phone * (970) 493-0213 Fax

Project Name: SMMI	Project Number:	60284905-2100	-		Analysis Required	pa.		
Send Report To: John Rosburg	Sampler (Print Name):	John Rosburg					Page	2 of 4
Address: 20325 Moss Bend Ct	Sampler (Print Name):	Doug Bopray						
Lutz, FL 33558	Shipment Method:	FED EX			р			
	Airbill Number				ioA			
Phone: (970) 219-4904	Laboratory Receiving:	TestAmerica		i L	ono		Purchase Order No.	der No. 49212
Fax: (813) 948-7333					ildə-			
Field	Sample Date Time	Sample Matrix	Number of Containers	Mercu Cadm	Fead		Comments, Special Instructions, etc.	Lab Sample ID (to be completed by lab)
129-4, Container 1	10/02/13	Filter	1	× × ×				
129-4, Container 3	10/02/13	0.1 N HNO ₃		×				
129-4, Container 4	10/02/13	H ₂ O ₂ /HNO ₃	2	×				
129-4, Container 5	10/02/13	0.1 N HNO ₃	-	×				
129-4, Container 6	10/02/13	Acidified KMnO₄	1	×				
			-					
Blank, Container 8A	10/02/13	0.1 N HNO3	-	×				
Blank, Container 9	10/02/13	H ₂ O ₂ /HNO ₃	-	×××				
Błank, Container 10	10/02/13	Acidic KMnO ₄	1	×				
Blank, Container 12	10/02/13	Filter	-	×			P-9, P-10, P-11	
PEA1947	10/02/13	Filter	1	×			Audit Sample	
PEA1950	10/02/13	Impinger Solution	V	×			Audit Sample	
PEA1945	10/02/13	Filter	-	×			Audit Sample	
PEA1948	10/02/13	Impinger Solution	-	×			Audit Sample	
PEA1941	10/02/13	Impinger Solution	-		×		Audit Sample	
		1,0						
Relinquished by: (Signature)	Received by (Signature)		Date;	Time:	Sample Custodian Re	Sample Custodian Remarks (Completed By Laboratory):	aboratory):	
Doug Bopray 10/4/2013 9:00	Mahall		11/2/01	200	QA/QC Level	Turnaround	Sampl	Sample Receipt
Relinquished by: (Signature)	Received by: (Signature)		Date:	Пте:	[evel]	Routine	Total # Containers Received?	17
Relinquished by: (Signature)	Received by: (Signature)		Date:	Time:	revel	24 Hour	COC Seals Intact?	
					Cevel III	1 Week	Received Containers Intact?	
White: Lab Copy Yellow: PM Copy	Pink: Field Copy	Gold: PM/QA/QC Copy						

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AECOM Environment 1601 Prospect Parkway, Fort Collins, CO 80525 970) 493-8878 Phone * (970) 493-0213 Fax 905-2100

www.aecom.com

Project Name:	SMMI	Project Number:		60284905-2100			Analysis Required	ired		
Send Report To:	John Rosburg	Sampler (Print Name):		John Rosburg					Pade	3 of 4
Address:	20325 Moss Bend Ct	Sampler (Print Name)		Doug Bopray					· >	
	Lutz, FL 33558	Shipment Method:		FED EX		þ				
		Airbill Number				iοΑ				
Phone:	(970) 219-4904	Laboratory Receiving:	iving:	TestAmerica					Purchase Order No.	rder No. 49212
Fax:	(813) 948-7333									
Fie	Field Sample ID	Sample Date	Sample Time	Sample Matrix	Number of Containers	Particu Hydro			Comments, Special Instructions, etc.	Lab Sample ID (to be completed by lab)
15-1, Container 1		09/29/13		Filter	1	×				
15-1, Container 2		09/29/13		Acetone	-	×				
I5-1, Container 3		09/29/13		0.1 N H ₂ SO ₄	2	×				
15-2, Container 1		09/30/13		Filter	1	×				
15-2, Container 2		09/30/13		Acetone	1	×				
15-2, Container 3		09/30/13		0.1 N H ₂ SO ₄	7	×				
15-3, Container 1		10/01/13		Filter	1	×				
15-3, Container 2		10/01/13		Acetone	1	×				
f5-3, Container 3		10/01/13		0.1 N H ₂ SO ₄	7	×				
15-4, Container 1		10/02/13		Filter	1	×				
15-4, Container 2		10/02/13		Acetone	1	×				
15-4, Container 3		10/02/13		0.1 N H ₂ SO₄	2	×				
15-Blank, Container	ner 1	10/02/13		Filter	7***	×				
I5-Blank, Container 2	er 2	10/02/13		Acetone	y ~~	×				
15-Blank, Container 3	ner 3	10/02/13		0.1 N H ₂ SO₄	ļ	×				
Relinquished by: (Signature)	mature)	Received by (Signafure)	// //(eun;		Date:	Time:	Sample Custodian F	Sample Custodian Remarks (Completed By Laboratory):	boratory):	
Doug Bopray	10/4/2013 9:00	Mhu	1		10/7/11	200	QA/QC Level	Turnaround		Sample Receipt
Relinquished by: (Signature)	gnature)	Received by: (Signatére)	(dre)		Date:	Time:	Level I	Routine	Total # Containers Received? COC Seals Present?	¿pe
Relinquished by: (Signature)	nature)	Received by: (Signature)	nre)		Date:	Time:		24 Hour	COC Seals Intact?	
				2			Cither State	1 Week	Received Containers Intact?	23
White: Lab Copy	Yellow: PM Copy	Pink: Field Copy		Gold: PM/QA/QC Copy					1 ciliberature ?	

Chain of Custody Record

No. 60284905-2100

AECOM Environment

1601 Prospect Parkway, Fort Collins, CO 80525 970) 493-8878 Phone * (970) 493-0213 Fax

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नाजिल्या श्रवताल.	- 1	Project Number	60284905-2100			Analysis Regulred	Ş.			
Send Report To:	- 1	Sampler (Print Name):	John Rosburg					Page	4 of 4	
Address:	20325 Moss Bend Ct	Sampler (Print Name):	Doug Bopray			(†		-		_
	Lutz, FL 33558	Shipment Method:	FED EX			- 6 _d				
		Airbill Number) tei				
Рћопе:	(970) 219-4904	Laboratory Receiving:	TestAmerica			ηs		Purchase	Purchase Order No. 49212	
Fax:	(813) 948-7333				(여러)					
Ē	Field Sample ID	Sample Date Time	Sample Matrix	Number of Containers	Partic Lead Mercu	MI IM		Comments, Special Instructions, etc.	Lab Sample ID (to be completed by lab)	n
										и
Please provide	Please provide combined front and back half Method 29 Results.	aff Method 29 Results.								_
Cadmium (Cd),	Lead (Pb) and Mercury An	Cadmium (Cd), Lead (Pb) and Mercury Analysis for samples [29-1, 129-2, 129-	.2. 129-3, 129-4, Plex	3.129-4. Please combine front half and back half	front half and	back balf				,_,_
										_
Pag										
e										
G Filters: Please v	veigh filters (2 consecutive	Filters: Please weigh filters (2 consecutive weighings within 0.5 mg of each other) for Method 5 particulate analysis	ach other) for Meth	od 5 particula	ite analysis.					
Q Filters: Please v	Q Filters: Please weigh filters with out petri dishes.	ishes.								
25 Filters: Tare we	ights and associated run no	Filters: Tare weights and associated run numbers will be provided on separate weigh sheets.	sparate weigh shee	ts.						
Fifters: The ID o	of each filter is listed with a	Fifters: The ID of each filter is listed with a sharpie Marker on each petri dish and can be correlated to the tare weight sheet to be provided.	idish and can be co	prrelated to th	e fare weigh	t sheet to be provide	èd.			
		177								
Acetone Fractic	ns: Please provide particul.	Acetone Fractions: Please provide particulate mass gain per Method 5.								_
Please provide	digital results to John Rosb	Please provide digital results to John Rosburg at john.rosburg@aecom.com	com							
If you have any	questions or concerns rega	if you have any questions or concerns regarding the samples or instructions please call John Rosburg at (970) 219-4904 or (970) 420-0602	tions please call Joi	hn Rosburg a	t (970) 219-	1904 or (970) 420-06	302.			_
								- Advisor - Advi		
Relinquished by: (Signature)	gnature)	Received by (Signature)		Date:	Timg:	Sample Custodian Remarks (Completed By Laboratory):	arks (Completed By Lab	oratory):		
Doug Bopray	10/4/2013 9:00			10 /7/12	200	QA/QC Level	Turnaround		Sample Receipt	_
Relinquished by: (Signature)	gnature)	Received by: (Signature)		Date:	Time:	[[Total # Containers Received?		_
						Cevel	Routine	COC Seals Present?		
Relinquished by: (Signature)	gnature)	Received by: (Signature)		Date: 1	Time:		24 Hour	COC Seals Intact?		
1							1 week	Received Containers Intact?		
White: Lab Copy	Yellow: PM Copy	Pink: Field Copy	Gold: PM/QA/QC Copy				Omer	l emperature?		

AECOM

SUPPLIER NO: 9465

SUPPLIER:

TESTAMERICA LABORATORIES INC P.O. BOX 204290 DALLAS,TX 75320. United States

	PURCHASI	PORDER					
	ORDER NUMBER 212ACM	REVISION 0	PAGE 1 of 1				
This Purchase Order Number must appear on all order acknowledgements, invoices, packing lists, cartons and correspondence.							
This Purch acknowled	gements, invoices	, packing lists,	on all order cartons and				

ATE	OF ORDER 18-SEP-13	BUYER Bolfer	ill, Jennifer L		REQUESTO		opray, Douglas A	(Doug)	
MYA	ENTTERMS	SHIP VIA	F.O.B	DESTI	NATION		FREIGHT TERM		
ONE	1000年1000年1000年100日 1000日 1000日 1000日 1000日	BEPDESCRIPTION			DUANTITY	UOM	UNIT PRICE	EXTENDED.	TAX
1	All prices and amounts on this This Purchase Order is Subje-Continuing Services Agreeme Testamerica Laboratorias, Inc. Return Signed Purchase Order Doug.Bopray@aecom.com Remit Invoice To: Doug Bopra Doug.Bopray@aecom.com Samples 6 Samples Metals by ICPMS/4 Samples Particulate Matter 4 Samples Particulate Matter 5 Samples Method 26A Hydro-TestAmerica of Wast Sacram samples upon receipt, following column. Expenditure Type SUBC-Sul Project 60284905 Task 160	crite the Lerms and Core on to file with AECOM, it is a graph of the Core of t	300 is of air quality			AMT	995;	3,080.00	Z
1	THIS PURICHASE ORDER IS 9 18	113 Mala	ACHED TERMS MULLI LIER SIGNATUR	la 9		SUB	TOTAL \$ TAX \$ TOTAL \$	3,060.00 0.00 . 3,060.00)

Login Sample Receipt Checklist

Client: AECOM, Inc.

Job Number: 320-4473-1

Login Number: 4473 List Number: 1

List Source: TestAmerica Sacramento

Creator: Hytrek, Cheryl

Question	Answer	Comment
Radioactivity wasn't checked or is = background as measured by a survey meter.</td <td>True</td> <td></td>	True	
The cooler's custody seal, if present, is intact.	True	
Sample custody seals, if present, are intact.	N/A	
The cooler or samples do not appear to have been compromised or tampered with.	True	
Samples were received on ice.	True	
Cooler Temperature is acceptable.	True	
Cooler Temperature is recorded.	True	
COC is present.	True	
COC is filled out in ink and legible.	True	
COC is filled out with all pertinent information.	True	
Is the Field Sampler's name present on COC?	N/A	
There are no discrepancies between the containers received and the COC.	True	
Samples are received within Holding Time.	True	·
Sample containers have legible labels.	True	
Containers are not broken or leaking.	True	
Sample collection date/times are provided.	True	
Appropriate sample containers are used.	True	
Sample bottles are completely filled.	True	
Sample Preservation Verified.	N/A	•
There is sufficient vol. for all requested analyses, incl. any requested MS/MSDs	True	

True

True

True

N/A

<6mm (1/4").

Multiphasic samples are not present.

Residual Chlorine Checked.

Samples do not require splitting or compositing.

Containers requiring zero headspace have no headspace or bubble is





14 October 2013

John Rosburg AECOM 20325 Moss Benedict Lutz, FL 33558

Ph.: 970.219.4904

Email: john.rosburg@aecom.com

Subject: Certificate of Results

Dear John:

Attached to this narrative are the analytical results you requested on samples submitted for the determination of polychlorinated dibenzo-p-dioxins and dibenzofurans. The insert below summarizes the relevant information pertaining to your project. In particular, QC annotations bring to your attention specific analytical observations and assessments made during the sample handling and data interpretation phases. Results reported relate only to the items tested.

Project Information Summary	When applicable, see QC Annotations for details
Client Project No.	60284905-2100
SGS-AP Project #	· A6007
Analytical Protocol	Method 23
No. Samples Submitted	5
No. Samples Analyzed	5
No. Laboratory Method Blanks	1
No. OPRs / Batch CS3	1
No. Outstanding Samples	. 0
Date Received	7-Oct-2013
Condition Received	good
Temperature upon Receipt (C)	23 (Traps & Filters), 9 (Solvents)
Extraction within Holding Time	yes
Analysis within Holding Time	yes
Data meet QA/QC Requirements	See Below
Exceptions	See Below
Analytical Difficulties	See Below

ANALYTICAL PERSPECTIVES IS NOW PART OF SGS, THE WORLD'S LEADING INSPECTION, **VERIFICATION, TESTING AND CERTIFICATION COMPANY.**



QC Annotations:

1. See Appendix A & B for data qualifier, data attribute, and lab identifier information.

Analytical Perspectives Certification IDs

SOUTH CAROLINA	99054
ARKANSAS	88-0628
NEW JERSEY-NELAP SECONDARY	NC005
FLORIDA-NELAP PRIMARY	E87608
LOUISIANA	4024
NORTH CAROLINA	37783
WASHINGTON	C2027
NEW YORK	11988
VIRGINIA	460180
MINNESOTA	037-999-448
OREGON	pending
TEXAS	T104704484-10-1
PENNSYLVANIA-NELAP SECONDARY	68-01849

SGS-Analytical Perspectives remains committed to serving you in the most effective manner. Should you have any questions or need additional information and technical support, please do not hesitate to contact us.

The management and staff of SGS-Analytical Perspectives welcome customer feedback, both positive and negative, as we continually improve our services. Please visit our web site at www.ultratrace.com and click on the 'Leave Your Feedback Here!' link on the Home Page. Thank you for choosing SGS-Analytical Perspectives.

Sincerely,

Heather Distel, Ph.D.

Senior Project Scientist/Team Lead

Heather Llistel



	APPENDIX A: DATA QUALIFIERS / DATA ATTRIBUTES
*	The reported concentration exceeds the calibration range (upper point of the calibration curve).1
>	Indicates high recoveries. Shown with the numeric value at the top of the range.1
В	The analyte is found in the method blank, at a level that is <=10x the sample concentration.
С	Two or more congeners co-elute. In EDDs C denotes the lowest IUPAC congener in a co- elution group and additional co-eluters for the group are shown with the number of the lowest IUPAC co-eluter.
E	The reported concentration exceeds the calibration range (upper point of the calibration curve).
EMPC	Represents an Estimated Maximum Possible Concentration. EMPC's arise in cases where the signal/noise ratio is not sufficient for peak identification (the determined ion-abundance ratio is outside the allowed theoretical range), where there is a co-eluting interference, or where a single ion is utilized for quantitation due to PFK interference.
ETH	Indicates the presence of a diphenyl ether that appears to interfere with the quantitation of a furan. The reported concentration is the maximum.
H/h	If the standard recovery is below the method or SOP specified value "H" is assigned. If the obtained value is less than half the specified value "h" is assigned.
J	Indicates that an analyte has a concentration below the reporting limit (lowest point of the calibration curve).
ND	Indicates a non-detect.
NR	Indicates a value that is not reportable.
PR	Due to interference, the associated congener is poorly resolved.
QI	Indicates the presence of a quantitative interference.
Ra	The new ratio – [Ra] for 2,3,7,8-TCDD following the ³⁷ Cl ₄ -2,3,7,8-TCDD correction is shown between squared brackets in the DL column. ¹
SI	Denotes "Single Ion Mode" and is utilized for PCBs where the secondary ion trace has a significantly elevated noise level due to background PFK. Responses for such peaks are calculated using an EMPC approach based solely on the primary ion area(s) and may be considered estimates. ¹
U	The analyte was not detected. The estimated detection limit (EDL) may be reported for this analyte.
٧	The labeled standard recovery was found to be outside of the method control limits.
X	Indicates results reported from reinjection, refractionation, or repeat analyses.
	APPENDIX B: LAB ID IDENTIFIERS
AR	Indicates use of the archived portion of the sample extract.
CU	Indicates a sample that required additional clean-up prior to MS injection/processing.
D	Indicates a dilution of the sample extract. The number that follows the "D" indicates the dilution factor.
DE	Indicates a dilution performed with the addition of ES (extraction standard) solution.
DUP	Designation for a duplicate sample.
MS	Designation for a matrix spike.
MSD	Designation for a matrix spike duplicate.
RJ	Indicates a reinjection of the sample extract.
S	Indicates a sample split. The number that follows the "S" indicates the split factor.

Denotes data qualifiers/attributes whose use will be phased out over time

A6007 - TEQ Project ID: 6028 4905-2100

Sample Summary Part 1	SE	Aveatrine	AVALTICAL PERSPECTIVES		2	Method 23
Analyte	Method Blank A6007	l5-Blank	15-1	15-2	15-3	15.4
	bd	bd	bd	бd	bd	bd
2,3,7,8-TCDD	(1.54)	(1.68)	[2.34]	12.2	[6.58]	[6.42]
1,2,3,7,8-PeCDD	(2.17)	(1.7)	[6.45]	86.3	[25.8]	[21.5]
1,2,3,4,7,8-HxCDD	(2.18)	(1.76)	13	148	29.9	25.9
1,2,3,6,7,8-HxCDD	(2.16)	(1.93)	33.9	209	69.1	40.9
1,2,3,7,8,9-HxCDD	(2.32)	(1.94)	18.9	166	44.6	30.4
1,2,3,4,6,7,8-HpCDD	[4.13]	16	316	1670	750	395
ОСББ	22.2	30.1	546	2600	1640	989
2,3,7,8-TCDF	(0.927)	(0.9)	21.5	107	39.4	40.2
1,2,3,7,8-PeCDF	(966.0)	(1.05)	18	166	72.6	61.6
2,3,4,7,8-PeCDF	(0.917)	(0.978)	50	450	151	125
1,2,3,4,7,8-HxCDF	(1.29)	(1.41)	33.4	327	146	113
1,2,3,6,7,8-HxCDF	(1.25)	(1.31)	29.2	368	182	123
2,3,4,6,7,8-HxCDF	(1.24)	(1.38)	54.3	830	372	235
1,2,3,7,8,9-HxCDF	(1.5)	(1.72)	(1.71)	(4.95)	(4.76)	(4.22)
1,2,3,4,6,7,8-HpCDF	(1.73)	(1.34)	143	1630	871	574
1,2,3,4,7,8,9-HpCDF	(2.1)	(1.61)	27.6	173	199	102
OCDF	(3.06)	(2.29)	142	546	961	462
ITEF TEQ (ND=0; EMPC=0)	0.0222	0.191	51.9	542	188	139
ITEF TEQ (ND=0; EMPC=EMPC)	0.0634	S. 191	9.79	542	208	156
ITEF TEQ (ND=DL/2; EMPC=0)	2.26	2.36	53.0	542	190	
ITEF TEQ (ND=DIJ2; EMPC=EMPC)	2.29	2.36	57.5	. 542	208	156
ITEF TEQ (ND=DL; EMPC=EMPC)	4.52	4.53	57.6	543	208	156
Checkcode	480-593-ZVM	527-902-CWR	520-615-RKC	996-461-RVQ	800-863-YNS	633-277-HWN
Lab ID	MB1_11406_DF_SDS[/	A6007_11406_DF_001	MB1_11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_002 A6007_11406_DF_003 A6007_11406_DF_004 A6007_11406_DF_005	A6007_11406_DF_003	A6007_11406_DF_004	A6007_11406_DF_005

A6007 - WHO-2005-TEQ Project ID: 6028 4905-2100

Sample Summary Part 1	SE	Aveatrica	AVALTICAL PERSPECTIVES		Σ	Method 23
Analyte	Method Blank A6007	I5-Blank	1-51	7-91	15-3	15.4
	Вd	бd	Вd	бd	bd	bd
2,3,7,8-TCDD	(1.54)	(1.68)	[2.34]	12.2	[6.58]	[6.42]
1,2,3,7,8-PeCDD	(2.17)	(1.7)	[6.45]	86.3	[25.8]	[21.5]
1,2,3,4,7,8-HxCDD	(2.18)	(1.76)	13	148	29.9	25.9
1,2,3,6,7,8-HxCDD	(2.16)	(1.93)	33.9	209	69.1	40.9
1,2,3,7,8,9-HxCDD	(2.32)	(1.94)	18.9	166	44.6	30.4
1,2,3,4,6,7,8-HpCDD	[4.13]	16	316	1670	750	395
OCDD	22.2	30.1	546	2600	1640	686
2,3,7,8-TCDF	(0.927)	(6.0)	21.5	107	39.4	40.2
1,2,3,7,8-PeCDF	(0.996)	(1.05)	18	166	72.6	61.6
2,3,4,7,8-PeCDF	(0.917)	(0.978)	50	450	151	125
1,2,3,4,7,8-HxCDF	(1.29)	(1.41)	33.4	327	146	113
1,2,3,6,7,8-HxCDF	(1.25)	(1.31)	29.2	368	182	123
2,3,4,6,7,8-HxCDF	(1.24)	(1.38)	54.3	830	372	235
1,2,3,7,8,9-HxCDF	(1.5)	(1.72)	(1.71)	(4.95)	(4.76)	(4.22)
1,2,3,4,6,7,8-HpCDF	(1.73)	(1.34)	143	1630	871	574
1,2,3,4,7,8,9-HpCDF	(2.1)	(1.61)	27.6	173	199	102
OCDF	(3.06)	(2.29)	142	546	961	462
WHO-2005 TEQ (ND=0; EMPC=0)	0.00666	0.169	41.0	490	155	Ţ
WHO-2005 TEQ (ND=0; EMPC=EMPC)	0.0479	0.169	49.8	490	187	139
WHO-2005 TEQ (ND=DL/2; EMPC=0)	2.69	2.66	42.6	490	157	7
WHO-2005 TEQ (ND=DL/Z; EMPC=EMPC)	2.74	2.66	49.9	490	187	140
WHO-2005 TEQ (ND=DL: EMPC=EMPC)	5.38	5/4	90.09	490	188	140
Checkcode Lab ID	480-593-ZVM MB1_11406_DF_SDS	527-902-CWR A6007_11406_DF_001	520-615-RKC A6007_11406_DF_002	996-461-RVQ A6007_11406_DF_003	480-593-ZVM 527-902-CWR 520-615-RKC 996-461-RVQ 800-863-YNS 633-277-HWN MB1_11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_005	633-277-HWN A6007_11406_DF_005

A6007 - Totals Project ID: 6028 4905-2100

Sample Summary Part 2	SG		NATHCAL PERSPECTIVES		Σ	Method 23
Analyte	Method Blank A6007	I5-Blank	15-1	15-2	15-3	15.4
Totals	bd	6d	bd	бd	bd	6d
, CO OT	,		0	,		
Pecdos	2.44 0	0 0	99.8 210	509 1520	30.4 44.	133
HXCDDs	0	0	510	3490	854	516
HPCDDs	0 (16	653	3800	1440	845
	7:77	30.1	546	2600	1640	686
TCDFs	0	0	732	4090	1040	1070
PecDFs	0	0	419	4740	1500	1290
HxCDFs	0	0	303	4230	1940	1410
HpCDFs	0	0	257	2420	1760	1040
OCDF	0	0	142	546	961	462
Total PCDD/Fs (ND=0; EMPC=0)	24.6	46.1	3.870	28.000	11,600	8.010
Total PCDD/Fs (ND=0; EMPC=EMPC)	34.1	63.0	3,890	28,000	11,700	8,060
Total PCDD/Fs (2378-X ND=DL; EMPC=EMPC)	59.5	86.0	3,890	28,000	11,700	8,070
Total 23778 (ND=9: EMPC=9)	22.2	46.1	1.(50	0.57-5	055/5	3.320
Total 2378s (ND=1; EMPC=9)	0.05	0.07	067/1)			125°3
Total 2378s (ND=0; EMPC=1)	26.5	46.4	1.450	a) A Cua	5.500	13:1
Total 2378s (NP=0-5; EMPC=1) Total 2378s (NP=1 EMPC=1)	0.60	S.77.3	7,460	9.490	5,570	
Checkcode	480-593-7VM	527-902-CIMB	520_615_PKC	006 461 570	SINA 590 008	MANU 777 C23
Lab ID	MB1_11406_DF_SDS	A6007_11406_DF_001	A6007_11406_DF_002	A6007_11406_DF_003	MB1_11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_002 A6007_11406_DF_003 A6007_11406_DF_005 A6007_11406	A6007_11406_DF_005

A6007 - Others Project ID: 6028 4905-2100

Sample Summary Part 3	SE		L'Powergonyves		Š	Method 23
Analyte	Method Blank A6007	I5-Blank	15-1	15-2	£-9I	15.4
Octob DODD/For AND THE CAMPOON	бd	bd	бd	ΒĠ	Бd	B d
Other PCDD/rs (ND=0, EMPC=0)		((ļ		
Other ICDD Other PeCDD	2.44	o c	99.8	497 1440	301	133 245
Other HxCDD	0	0	444	2970	711	419
Other HpCDD	0	0	337	2120	069	450
Other TCDF	0	0	710	3990	1000	1030
Other PeCDF	0	0	351	4130	1280	1110
Other HxCDF	0	0	186	2710	1240	937
Other HpCDF	0	0	87.2	624	289	366
Other PCDD/Fs (ND=0, EMPC=EMPC)						
Other TCDD	2.44	1.81	107	516	157	155
Other PeCDD	0	0	214	1440	330	245
Other HxCDD	0	3.7	444	2970	711	419
Other HpCDD	5.39	£.	337	2120	069	450
Other TCDF	0	0	710	3990	1010	1040
Other PeCDF	0	0	351	4130	1280	1110
Other HxCDF	0	0	186	2710	1240	937
Other HpCDF	0	0	87.2	624	289	366
Checkcode Lab ID	480-593-ZVM MB1_11406_DF_SDS	527-902-CWR A6007_11406_DF_001	520-615-RKC A6007_11406_DF_002	996-461-RVQ A6007_11406_DF_003	480-593-ZVM 527-902-CWR 520-615-RKC 996-461-RVQ 800-863-YNS 633-277-HWN MB1_11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_002 A6007_11406_DF_003 A6007_11406_DF_005	633-277-HWN A6007_11406_DF_005

A6007 - DLs Project ID: 6028 4905-2100

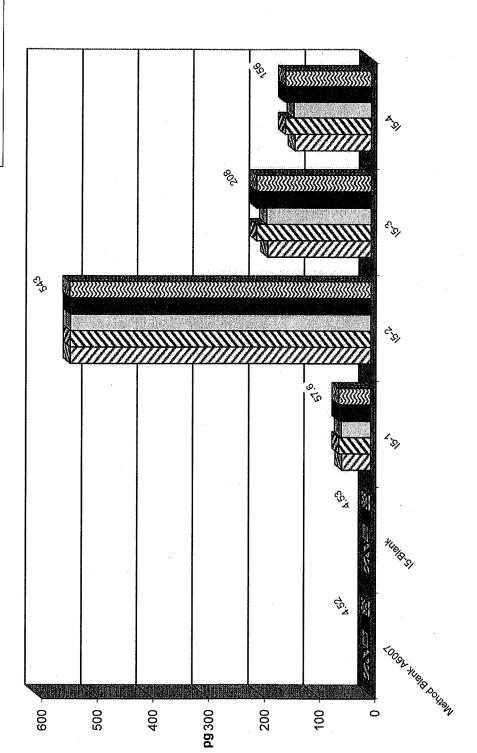
Sample Summary Part 5 (DLs)	SG	AWALTICA	AVALTICAL PERSPECTIVES		Σ	Method 23
Analyte	Method Blank A6007	l5-Blank	15-1	15-2	15-3	15.4
	Вd	bd	bd	bd	bd	bd
2,3,7,8-TCDD	1.54	1.68	1.25	1.72	1.7	2.32
1,2,3,7,8-PeCDD	2.17	1.7	1.74	2.01	2.53	3.21
1,2,3,4,7,8-HxCDD	2.18	1.76	2	2.21	3.23	3.73
1,2,3,6,7,8-HxCDD	2.16	1.93	2.05	2.28	3.56	3.72
1,2,3,7,8,9-HxCDD	2.32	1.94	2.1	2.37	3.56	3.92
1,2,3,4,6,7,8-HpCDD	2.49	2.47	3.02	3.79	5.22	4.18
OCDD	5.94	4.91	4.15	5.86	6.21	4.62
2,3,7,8-TCDF	0.927	6.0	0.862	1.68	1.19	1.37
1,2,3,7,8-PeCDF	966.0	1.05	1.55	4.69	3.25	2.5
2,3,4,7,8-PeCDF	0.917	0.978	4.	4.3	3.2	2.42
1,2,3,4,7,8-HxCDF	1.29	1.41	1.46	4.21	3.85	3.26
1,2,3,6,7,8-HxCDF	1.25	1.31	1.43	4.06	3.83	3.17
2,3,4,6,7,8-HxCDF	1.24	1.38	1.48	4.04	4.13	3.37
1,2,3,7,8,9-HxCDF	1.5	1.72	1.71	4.95	4.76	4.22
1,2,3,4,6,7,8-HpCDF	1.73	1.34	1.92	4.2	3.58	3.06
1,2,3,4,7,8,9-HpCDF	2.1	1.61	2.19	4.94	4.36	3.89
OCDF	3.06	2.29	2.13	3.39	3.54	3.63
Total TCDD	1.54	1.68	1.25	1.72	1.7	2.32
Total PeCDD	2.17	1.7	1.74	2.01	2.53	3.21
Total HxCDD	2.21	1.87	2.04	2.28	3.43	3.77
Total HpCDD	2.49	2.47	3.02	3.79	5.22	4.18
Total TCDF	0.927	6.0	0.862	1.68	1.19	1.37
Total PeCDF	0.956	1.01	1.48	4.49	3.23	2.46
Total HxCDF	1.31	1.44	1.51	4.29	4.12	3.48
Total HpCDF	1.9	1.47	2.05	4.55	3.94	3.46
Checkcode I ab ID	480-593-ZVM 527-902-CWR 520-615-RKC 996-461-RVQ 800-863-YNS 633-277-HWN 617 11406 DF 901 A6007 11406 DF 903 A6007 11406 DF 903 A6007 11406 DF 903 A6007 11406 DF 905	527-902-CWR A6007 11406 DF 001	520-615-RKC A6007 11406 DF 002	996-461-RVQ A6007 11406 DF 003	800-863-YNS A6007 11406 DF 004	633-277-HWN A6007 11406 DF 005
					– – –	

ITEF-TEQ Project ID: 6028 4905-2100 A6007

■ND=DL/2; EMPC=EMPC BND=DL; EMPC=EMPC

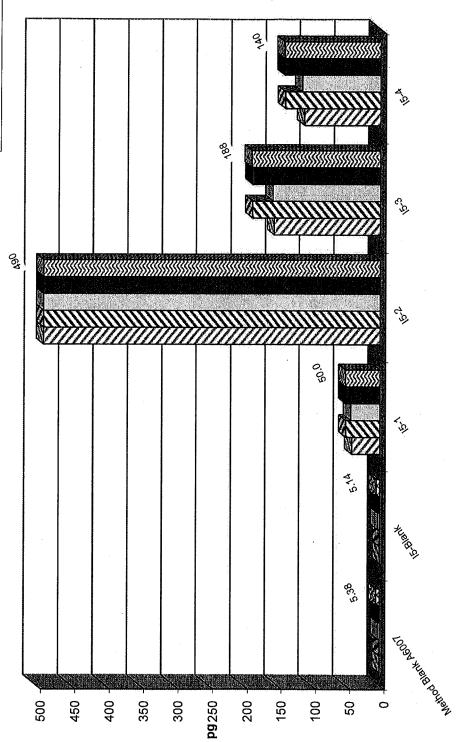
IS ND=0; EMPC=EMPC IS ND=DL/2; EMPC=0

BND=0; EMPC=0



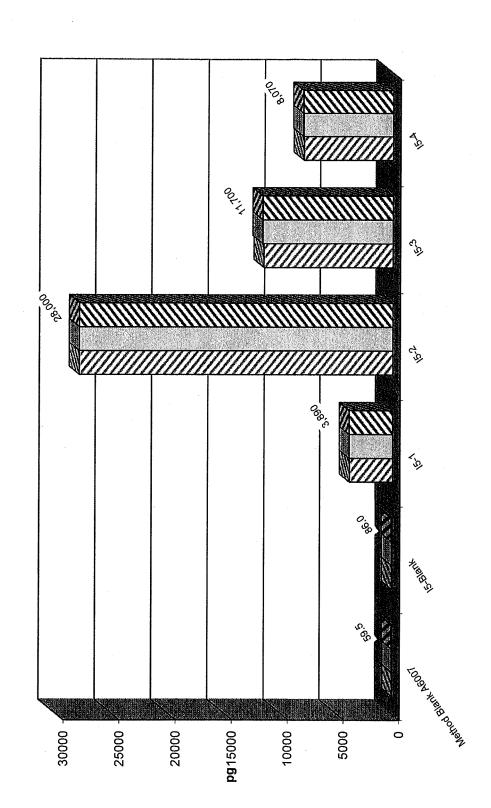
WHO-2005-TEQ Project ID: 6028 4905-2100 A6007





Totals Project ID: 6028 4905-2100 A6007





& X Polyo 402.38 180 Ja ç, 0/ col ke ₹ % ODOTA DEL ODO ODO OCO/JEV 9 8 8 70 9 20 4 3 20 9 0 % Rec.

□ Std. Dev.

⊡Mean

Mean Recoveries of Extraction Standards (N=6)

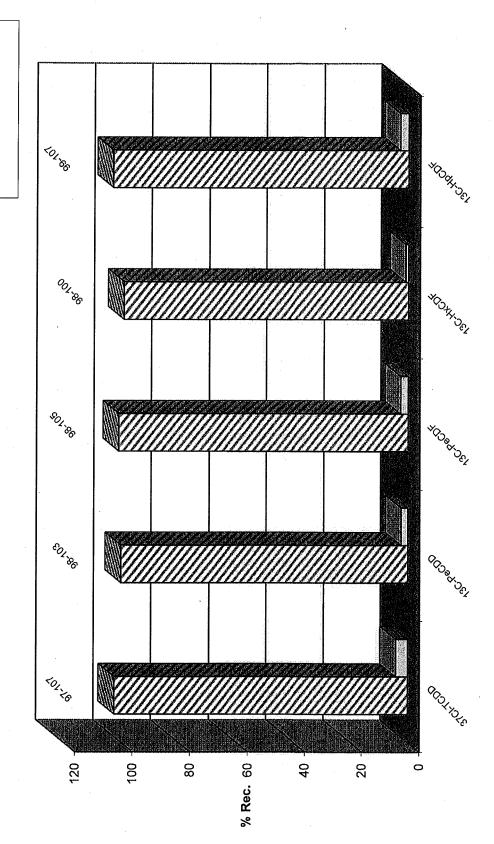
Project ID: 6028 4905-2100

Method Specification Limits: Tetra-Hexa ES: 40-130%, Hepta-Octa ES: 25-130% (F = fail)

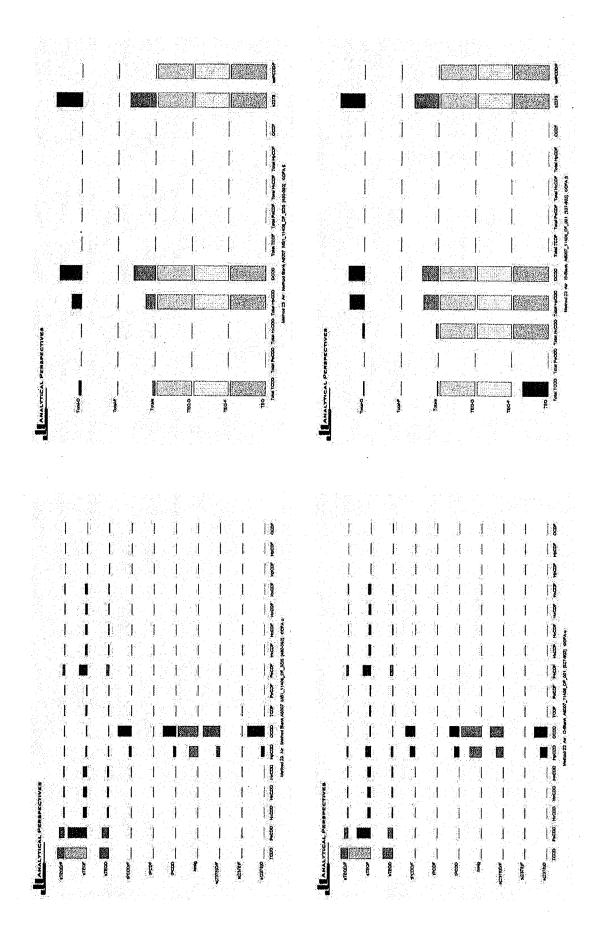
Mean Recoveries of Sampling Standards (N=6) Project ID: 6028 4905-2100 A6007

Std. Dev.

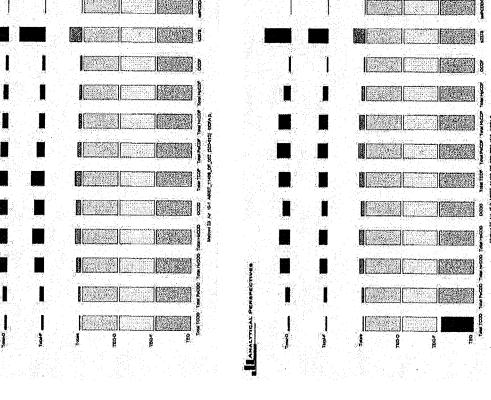
⊡Mean



Method Specification Limits: Tetra-Octa SS: 70-130% (F = fail)



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	· 합교육, 현대 발활하실하는 것으로 있었다면서 및 사이지가 있는데 ***
	- 1.25mg(檀水中,麦) 人名 7 马鹳(金融)(25mg)())(複數)(2000年)(2000年)(

Sample ID:	Method Blank A6007	nk A6007				Me	Method 23
Client Data		Sample Data		Laboratory Data	ata		
Name:	AECOM	Matrix:	Air	Lab Project ID:	A6007	Date Received:	n/a
Project ID:	6028 4905-2100	Weight/Volume:	τ-	Lab Sample ID MB1	MB1_11406_DF_SDS		08-Oct-2013
Date Collected:	n/a			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:		Time Analyzed:	16:03:53
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	ND III	1.54		200 (200)	ES 2378-TCDD	98.1	
12378-PeCDD	Α	2.17			ES 12378-PeCDD	102	Removed Bridge Bridge Bridge and Bridge and Bridge
123478-HxCDD	Ŋ	2.18			ES 123478-HxCDD	194	
123678-HxCDD	Q	2.16			ES 123678-HxCDD	102	neste a debestika sudi adijaka da Birijaka ini mangana da Conjunta da Conjunta da Conjunta da Conjunta da Conj
123789-HKCDD	ND Comment	2.32			ES 123789-HxCDD	[6]	
1234678-HpCDD	EMPC		4.13	-	ES 1234678-HpCDD	98.2	
OCDD	22.2				ES OCDD	89.3	
2378-TCDF		0.927			ES 2378-TCDF	102	
12378-PeCDF	ND N	0.996			ES 12378-PeCDF	104	colours and the first the manage beautiful and the second of the second
23478-PeCDF		0.917			ES 23478-PeCDF	102	
123478-HxCDF	ND	1.29	consulta el la codo de Londona en despais coloren por describio de la codo de		ES 123478-HxCDF	92.6	
123678-HxCDF	QN	1.25			ES 123678-HxCDF	98.6	The second secon
234678-HxCDF		1.24			ES 234678-HxCDF	101	
123789-HxCDF	ND	1.5			ES 123789-HxCDF	98.6	
1234678-HpCDF		1.73			ES 1234678-HpCDF	6.76	A THE CONTRACT OF THE PROPERTY
1234789-HpCDF	2	2.1			ES 1234789-HpCDF	98.7	
OCDF	QN	3.06			ES OCDF	88	
Totals					Standard	SS/AS Recoveries	S
The state of the s				A CONTRACTOR OF THE CONTRACTOR	SS 37CI-2378-TCDD	6.86	
Total TCDD	2.44		2.44		SS 12347-PeCDD	98.6	Carried State Conference on the Conference of the Conference on th
Total PeCDD	No	2.17	Ŋ		SS 12346-PeCDF	100	
Total HxCDD	۵N	2.21	Q	Control of the second s	SS 123469-HxCDF	100	Control of the Contro
Total HpCDD	N		9.51		SS 1234689-HpCDF	104	Miles and the second se
Total TCDE	UN	7600		The state of the s	AS 1368-TCDD	105	
Total Pacing		0.056	CN				
Total HxCDF	S. L.	7.31		41			
Total HpCDF	NO	1.9	Q				And the second s
Total PCDD/Fs	24.6		34.1				
ITEF TEQS							
TEQ: ND=0	0.0222		0.0634			271	2714 Exchange Drive
TEQ: ND=DL/2	2.26	2.24	2.29		<i>y,</i>	Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	4.5	4.49	4.52		ANALYTICAL PERSONECTIVES		www.us.sgs.com
					Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ree 866 846-8290; Fax	+1 910 794-3919

Report Created: 14-Oct-2013 11:52 Analyst: MC

Checkcode: 480-593-ZVM

Sample ID:	15-Blank					Me	Method 23
Client Data		Sample Data		Laboratory Data	ıta		
Name:	AECOM	Matrix:	Air	Lab Project ID:	— A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:		Lab Sample ID A6007	A6007	_11406_DF_001 Date Extracted:	08-Oct-2013
Date Collected:	02-Oct-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:	•	Time Analyzed:	16:56:31
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	N	1.68		The second secon	ES 2378-TCDD	97.4	
12378-PeCDD	N	1.7			ES 12378-PeCDD	9.76	
123478-HxCDD	ND	1.76			ES 123478-HxCDD	97.4	
123678-HxCDD	NO	1.93			ES 123678-HxCDD	95.1	
123789-HxCDD		1.94		The State Should the State	ES 123789-HxCDD	92.9	
1234678-HpCDD	16		for the specific property constitutions and described by property of the specific sp	JB	ES 1234678-HpCDD	92.7	
OCDD	30.1			JB	ES OCDD THE STATE OF THE STATE	81.9	
2378-TCDF	UN PORTE	6.0			ES 2378_TODE		
12378-PeCDF	ND	1.05			ES 12378-PeCDF	101	
23478-PeCDF	ND	826.0			ES 23478-PeCDF	001	
123478-HxCDF		1.41		C. King to the Company of the Compan	ES 123478-HxCDF	93.7	
123678-HxCDF	NO POLICE	1.31			ES 123678-HxCDF	93.4	The second secon
234678-HxCDF	and to the control of	1.38			ES 234678-HxCDF	94.4	
123789-HxCDF	N	1.72		lie o	ES 123789-HxCDF	- 93	
1234678-HpCDF	And the second s	1.34			ES 1234678-HpCDF	6.06	
1234789-HpCDF	NO	1.61			ES 1234789-HpCDF	94.9	
OCDF	QN	2.29			ES OCDF	86.2	
Totals					Standard	SS/AS Recoveries	S
		A CONTRACTOR OF THE CONTRACTOR			SS:37CI-2378-TCDD	101	and the second s
Total TCDD	N	C STATE OF THE STA	1.81		SS 12347-PeCDD	103	
Total PeCDD	ND	17	2		SS 12346-PeCDF	99,4	
Total HxCDD	ND NO	Hills: All disputer by chine (C. 1) to CO	3.7		SS 123469-HxCDF	9.66	
Total HpCDD	16		27.4		SS 1234689-HpCDF	102	
			4		AS 1368-TCDD	101	
			ביים		AS 1368-1CUF	6.76	
Total PeCDF	ON XX	1.01	QN				
Total HxCDF		144	2				
Total HpCDF	Q	1.47	ND		A PER A PER		
Total PCDD/Fs	46.1		63				
ITEF TEQS							
TEQ: ND=0	0.191		0.191	Č	7	271	2714 Exchange Drive
TEQ: ND=DL/2	2.36	2.18	2.36		7.	Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	4.53	4.37	4.53		ANALTHCAL PERSPECTIVES		www.us.sgs.com
					Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ree 866 846-8290; Fax	: +1 910 794-3919

Report Created: 14-Oct-2013 11:53 Analyst: MC

Checkcode: 527-902-CWR

Sample ID:	15-1		a			Me	Method 23
Client Data		Sample Data		Laboratory Data	ıta		
Name:	AECOM	Matrix:	Air	Lab Project ID:	A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	~	Lab Sample ID A6007	_11406_DF	_002 Date Extracted:	08-Oct-2013
Date Collected:	29-Sep-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:	•	Time Analyzed:	17:48:37
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
237&-TCDD	OdWE		2.34	in a star for	ES 2378-TCDD	87.2	100 May 100 Ma
12378-PeCDD	EMPC		6.45	A MANAGEMENT OF THE CONTRACTOR	ES 12378-PeCDD	86	Annahidration for the extraction of the control of
123478-HxCDD	13				ES 123478-HxCDD	89.4	PROPERTY OF THE PROPERTY OF TH
123678-HxCDD	33.9		"A PROPERTY (NATE - COUNTY AND A ROOM AND A		ES 123678-HxCDD	06	
123789-HxCDD	18.9				ES 123789-HxCDD	88.5	
1234678-HpCDD	316	Control and the control of the contr	destillation skielden stoken fan y seetlich in het in mean 2000 oas die seeslik		ES 1234678-HpCDD	88.6	
OCDD	246					76.7	
2378-TCDF	215				ES 237&TCDF	906	
12378-PeCDF	18				ES 12378-PeCDF	92.2	
23478-PeCDF	20				ES 23478-PeCDF	1 16	
123478-HxCDF	33.4				ES 123478-HXCDF	. 85.2	See and the second seco
123678-HxCDF	29.2				ES 123678-HxCDF	843	
234678-HxCDF	54,3				ES 234678-HxCDF	85.2	
123789-HxCDF	Ŋ	1.71			ES 123789-HxCDF	873	
1234678-HpCDF	143				ES 1234678-HpCDF	80.8	
1234789-HpCDF	27.6				ES 1234789-HpCDF	88.4	
OCDF	142				ES OCDF	81.4	de Ouraines de la Contraction de Colon Camparataire de La Bellion de La Bellion de La Bellion de La Bellion de
Totals					Standard	SS/AS Recoveries	S
			e ga e a santa a paga e a santa a santa a santa a santa a santa a santa a santa a santa a santa a santa a santa		SS 37CI-2378-TCDD	۷0٤	
Total TCDD	8.66	AND ROWS IN THE SEC. SEC. SEC. SEC. SEC. SEC. SEC. SEC	109		SS 12347-PeCDD	98.1	100 May 100 May 100 May 100 May 100 May 100 May 100 May 100 May 100 May 100 May 100 May 100 May 100 May 100 May
Total PeCDD	210		221		SS 12346-PeCDF	99.7	
Total HxCDD	510	A TO A TO SERVICE AND SERVICE	510	4 m	SS 123469-HxCDF	98.8	
Total HpCDD	653		653		SS 1234689-HpCDF	105	
Mississing at 1990 cm 21 colored Color	CONTROL OF TAXABLE DESCRIPTION OF CONTROL OF THE CO	And the second s	And Statistics (All Serve Information Constitution Constitution)	APPENDING TO APPEN	AS 1368-TCDD	91	
Total TCDF	732	Stational Manage (1978) (State Selling)	732		AS 1368-TCDF	92.6	
Total PeCDF	419	CO. THE CO. HER AND THE ANALYSIS CONTROL STATE OF THE CO.	419	to the time and the constitution of the second of the second all the second and the second all the second and t	And Self Control of Annual Control of Control of Control of Control of Annual Control of	Control of the second s	
Total HxCDF	303		303				(A) 的名称形式精艺的
Total HpCDF	257		257	CONTROL TO THE STATE OF THE STA	in the conduction which constructions are not used in the COSTANT CONTROL (The COSTANT CONTROL COSTANT	estimosti deliminos varimentos y en entratas de comensos de confermos de como dos confermos de como de confermos de como de confermos de como	Zootzanden in kunden od nijedelijke projektera, ky de 1985 indel den 1990 on on on on on on on on on on on on o
Total PCDD/Fs	3870		3890				
ITEF TEQS							and the amenda delicated the amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and an amenda delicated and a
TEQ: ND=0	51.9		57.5	Č		271	2714 Exchange Drive
TEQ: ND=DL/2	53	2.14	57.5		7/2	Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	54.2	4.28	9.75		ANALYTICAL PERSPECTIVES		www.us.sgs.com
					Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ree 866 846-8290; Fax	: +1 910 794-3919

Report Created: 14-Oct-2013 11:53 Analyst: MC

Checkcode: 520-615-RKC

Sample ID:	: 15-2					Me	Method 23								
Client Data		Sample Data		l aboratory Data	<u></u>										
Name:	AECOM	Matrix:	Ąi	Lab Project ID:	A6007	Date Received	07-Oct-2013								
Project ID:	6028 4905-2100	Weight/Volume:	· ·	Lab Sample ID A6007			08-001-2013								
Date Collected:	30-Sep-2013)		QC Batch No:	11406	Date Analyzed:	13-Oct-2013								
		Split:	2	Dilution:	•	Time Analyzed:	18:41:14								
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers								
2378-TCDD	12.2				ES 2378-TCDD	6.06									
12378-PeCDD	86.3	BESTELEBROOK ARBESTANKELERA KOVIJANAONON VANAROKA (1857)	dadalah dahadan kataman kataman kataman kataman dari kan kataman dari dari kan kataman dari kan kataman dari ka	Podráce Toka (Million a matemánia dal matemánia de la desenda de la dese	ES 12378-PeCDD	94.1									
123478-HxCDD	148				ES 123478-HxCDD	95.2									
123678-HxCDD	209			A CONTRACTOR OF THE CONTRACTOR	ES 123678-HxCDD	94.4									
123789-HxCDD	166				ES 123789-HXCDD	95									
1234678-HpCDD	1670				ES 1234678-HpCDD	94.7									
OCDD	2600				ES OCDD	1 8 4.3									
edele edite delete de l'Assertiment d'Assertiment d'Assertiment de la company de la company de l'Assertiment d	en das immo i sacreti i ve i seje spelosje ogdosje jej opfisjel dog z Cott sje blata, na žite su jesiolobe se	Commission and Association (Commission and Commission Commission)	e etimen de marin i i i i i i i i i i i i i i i i i i		THE CONTRACTOR CONTRACTOR AND ADMINISTRATION OF THE LIBERTY PROPERTY AND ADMINISTRATION OF THE ADMINISTRATION OF THE CONTRACTOR AND ADMINISTRATION OF THE CONTRACTOR		-								
2378-TCDF	107				ES 237&-TCDF	95.5	all the second s								
12378-PeCDF	166		No. 10 to 10	and the state of t	ES 12378-PeCDF	90.9									
23478-PeCDF	450				ES 23478-PeCDF	93.2									
123478-HxCDF	327				ES 123478-HxCDF	91.1									
123678-HxCDF	398				ES 123678-HxCDF	. 64									
234678-HxCDF	830	AND THE RESIDENCE OF THE PROPERTY OF THE PROPE		A CANADA	ES 234678-HxCDF	93.9	o Na nobolica di Naciona di Braza di Braza di Braza di Braza di Mala.								
123789-HxCDF	N	4.95			ES 123789-HxCDF	94.9									
1234678-HpCDF	1630	in the comment of the property of the comment of th	er de la companya de la companya de la companya de la companya de la companya de la companya de la companya de		ES 1234678-HpCDF	90.6									
1234789-HpCDF	173				ES 1234789-HpCDF	91.9									
OCDF	546				ES OCDF	87.5	AV STANTON STA								
Totals			-		Standard	SS/AS Recoveries	s								
					SS 37CI-2378-TCDD	103									
Total TCDD	209		528		SS 12347-PeCDD	98.9									
Total PeCDD	1520		1520	i in	SS 12346-PeCDF	103									
Total HxCDD	3490		3490		SS 123469-HxCDF	97.7	V CO TRANSPORTED THE NAME OF THE PROPERTY OF T								
Total HpCDD	3800		3800		SS 1234689-HpCDF	101									
ADDRESS OF METAL PROPERTY OF THE PROPERTY OF T	TO ME DOUTS OF THE PERSON OF THE STREET WAS THE OWN TO A CONTRACT OF THE OWN THE STREET WAS THE				AS 1368-TCDD	95.8									
Total TCDF	4090		4090		AS 1368-TCDF	94.8									
Total PeCDF	4740		4740				To prove the first of the first of the constitution of the constit								
Total HxCDF	4230		4230												
Total HpCDF	2420		2420	de la companya del companya del companya de la comp	ende wy de feren, a menti fennew koladia de war de ande and de ande ande and de ande an	For Obliganisasse South and Color an	Challes and Manager (All and All	Total PCDD/Fs	28000		28000				
ITEF TEQS															
TEQ∵ND=0	542		542			271	2714 Exchange Drive								
TEQ: ND=DL/2	542	3.92	542			Wilmingtor	Wilmington, NC 28405, USA								
TEQ: ND=DL	243	7.83	543		Tel: +1 910 794-1613: Toll-E	MWW.US.Sgs.com 94/0 704_1612* Trail_Free RRR RAR_R700 Fav. +1 040 704_3019	www.us.sgs.com								
					101. 1010. 14. 1010	55 000 040-0200, 1 av	200								
Checkcode: 996-461-RVQ	ď	SGS AP D/F 2013 Rev. 2.6	v. 2.6		Report C	Report Created: 14-Oct-2013 11:53 Analyst: MC	1:53 Analyst: MC								

Sample ID:	: 15-3			.`		Me	Method 23
01204		Court Date					
Client Data		Sample Data		Laboratory Data			
Name:	AECOM	Matrix:	Air	Lab Project ID:	A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	-	Lab Sample ID A6007		11406 DF 004 Date Extracted:	08-Oct-2013
Date Collected:	01-Oct-2013			OC Batch No.		Date Analyzed	13-04-2013
		Split:	2	Dilution:		Time Analyzed:	19:33:47
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	EMPC		6.58	11 A	ES 2378-TCDD	88.5	
12378-PeCDD	EMPC	TO EXPERIT STAND CONTROL OF THE CONT	25.8		ES 12378-PeCDD	89.9	And the state of t
123478-HxCDD	29.9			Little Little Million St. 1997	ES 123478-HxCDD	6 J 6	
123678_HXCDD	60 1	Andrew Schoolster St. London Market St. Landschafter			ES 123878 UVODO	7 00	
420710-11:000					ES 123070-UXCDD	7.80	
1.23/88-TXCUD	44.0				ES 123789-HXCDD	90.5	
1234678-HpCDD		Production of the section of the sec		The state of the s	ES 1234678-HpCDD	91.7	
OCDD	1640				ES OCDD	83.1	
		The second secon					
237& CDF	39.4				ES 2378-TCDF	92.3	
12378-PeCDF	72.6				ES 12378-PeCDF	9.68	
23478-PeCDF	151 181				ES 23478-PeCDF	91.2	
123478-HxCDF	146			CONTRACTOR CONTRACTOR	ES 123478-HxCDF	87.9	and and the second seco
123678-HXCDF	182				ES 123678-HxCDF	6 Z8	
23/878_HVCDE	377	Control of the Contro	And the second s	AN AREA SELECTION AND AREA SELECTION AND ASSESSMENT OF THE SELECTION ASSESSMENT OF THE SELECTI	EC 224670 HVODE	0.70	
201011001	210					0.70	
123/88-AXCUT		4.75	Color Color		ES 123789-HXCDF	88.7	
1234678-HpCDF					ES 1234678-HpCDF	87.8	The season of th
1234789-HpCDF	199				ES 1234789-HpCDF	9.28	
OCDF	961				ES OCDF	83.9	
Totals					Standard	SS/AS Recoveries	Ş
	(A) (A) (A) (A) (A) (B) (B) (B) (B) (B) (B) (B) (B) (B) (B				SS 37CI-2378-TCDD	26	
Total TCDD	144	energickische seun ereichte Friedricht februik der erbeit op ereichte spein der der der der der der der der der der	164		SS 12347-PeCDD	98.8	28 deposed felomina (1975 for 4 America) in manifestal additions, about
Total PeCDD	301		355		SS 12346-PeCDF	98.3	
Total HxCDD	854	And the second of the second o	854		SS 123469-HxCDF	99.1	Section 2015 and applications of the section of the
Total HpCDD	1240		1440		SS 1234689-HpCDF	665	
					AS 1368-TCDD	95	
Total TCDF	1040		1050		AS 1368-TCDF	92.3	
Total PeCDF	1500		1500	A second entrance in 18 million in confilm that includes the confirmation of the confi		And the state of t	
Total HxCDF	1940	Simple Control of the	1940				
Total HpCDF	1760		1760		A company of the comp	The first of the control of the cont	
Total PCDD/Fs	11600		11700				
ITEF TEQS							
TEO: ND=0			208			7.6	2744 Evohoped Drive
TEO: NO-0	100	10 C	200	C	7		4 Challange Diffe
TEQ. ND-012	26-	50.0	200	うつ	ANALTHCAL PERSPECTIVES		Willington, 10C 20403, USA
	781	80.7	700		fel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ree 866 846-8290; Fax	: +1 910 794-3919
WY 620 000 Free Jee 40		7,4 4,000	Q Q		-		
Checkcode: 800-863-11NS	n	SGS AP U/F 2013 Rev. 2.6	ev. z.b		Nepoli C	Report Created: 14-Oct-2013 11:53 Analyst: MC	1:53 Analyst: เพเบ

Sample ID:	15-4					M	Mothod 22
	- 1						TILOG FO
Client Data		Sample Data		Laboratory Data	ita I		
Name:	AECOM	Matrix:	Air	Lab Project ID:	A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	_	Lab Sample ID	A6007_11406_DF_005 Date Extracted:	Date Extracted:	08-Oct-2013
Date Collected:	02-Oct-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:	•	Time Analyzed:	20:26:26
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	EMPC		6.42		ES 2378-TCDD	93.5	
12378-PeCDD	EMPC		21.5	7	ES 12378-PeCDD	94.8	inderende in de la company de la company de la company de la company de la company de la company de la company
123478-HxCDD	25.9				ES 123478-HxCDD	93.8	
123678-HxCDD	40.9	i de de la compresa como constituir de la compresa del la compresa del la compresa del la compresa de la compresa de la compresa de la compresa de la compresa de la compresa de la compresa de la compresa de la compresa de la compresa del la compr		7	ES 123678-HxCDD	93.4	Commence of the Commence of th
123789-HxCDD	30.4				ES 123789-HxCDD	93.4	Service Designation of the Service Ser
1234678-HpCDD	TOP STATE COURT THE STAT		and the supplication of the particular contradiction of the pa		ES 1234678-HpCDD	90.2	
OCDO	986				ES OCDD	82.3	
	en eren et de Person New Antales Annales Annales and Annales Parts (Annales	AND THE PROPERTY AND THE PROPERTY OF THE PROPE		NA AA JEGOTOOL OO OO OO OO OO OO OO OO OO OO OO OO		e e e e e e e e e e e e e e e e e e e	
2378-TCDF	40.2				ES 2378-TCDF	- 96.5	
12378-PeCDF	61.6	And the control of th	11 · · · · · · · · · · · · · · · · · ·		ES 12378-PeCDF	98.7	placify of challed and of challed with the state of and alternative factor of and finite
23478-PeCDF	125				ES 23478-PeCDF	96.2	
123478-HxCDF	113	THE RESIDENCE OF A PUBLICATION OF A PUBL			ES 123478-HxCDF	91.7	
123678-HxCDF	123				ES 123678-HxCDF	92.6	
234678-HxCDF	235	777			ES 234678-HxCDF	91.7	Francisco America (See Alexandra) and Frankis and Frankis and America (See Alexandra)
123789-HxCDF	N	4.22			ES 123789-HxCDF	92.3	
1234678-HpCDF	574				ES 1234678-HpCDF	84.8	
1234789-HpCDF	102				ES 1234789-HpCDF	92.2	
OCDF	462				ES OCDF	84.3	
Totals					Standard	SS/AS Recoveries	S
					SS 37CI-2378-TCDD	107	
Total TCDD	133		161	e de commune e com motor de Arque Cade e Califación actività de la participación de la	SS 12347-PeCDD	103	CONTRACTOR AND A MANAGEMENT OF THE PROPERTY OF
Total PeCDD	245		266	THE PROPERTY OF STREET	SS 12346-PeCDF	105	
Total HxCDD	516	HOLD STATE AND AND AND AND AND AND AND AND AND AND	516	A. The Control of the Assessment for the Parket of Spiritual of	SS 123469-HxCDF	100	This is where the country of the first Artifaction (The Artifaction Chandle) and the Artifaction of Artifaction (The Artifaction Chandle) and the Artifaction (T
Total HpCDD	845		845		SS 1234689-HpCDF	107	
			And the second s		AS 1368-TCDD	100	THE COLD IS LED VA.
			INSA		AS 1368-1CDF	66	
lotal PeCDF	1290	The second secon	1290			And the second of the second o	And the first on the own and the section of the finding of the section of the sec
Total HxCDF	1410		1410				
Total HpCDF	1040		1040				Continued to the contin
Total PCDD/Fs	8010		8060				
ITEF TEQS	tende destri de des risto de la resta de la desta de la resta de						
TEQ: ND=0	139		156			271	2714 Exchange Drive
TEQ: ND=DL/2	141	4.03	156	J.		Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	143	8.06	156		ANALYTICAL PERSONAL		www.us.sas.com
		-			Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ee 866 846-8290: Fax	+1 910 794-3919

Checkcode: 633-277-HWN

A6007 - TEQ Project ID: 6028 4905-2100

Sample Summary						
Part 1		NVATTICAL	LYTICAL PERSPECTIVES		Σ	Method 23
Analyte	Method Blank A6007	I5-Blank	15-1	15-2	15-3	15-4
	Вd	bd	bd	bd	pg	bd
2,3,7,8-TCDD	(1.54)	(1.68)	[2.34]	12.2	[8:58]	[6.42]
1,2,3,7,8-PeCDD	(2.17)	(1.7)	[6.45]	86.3	[25.8]	21.5
1,2,3,4,7,8-HxCDD	(2.18)	(1.76)	13	148	29.9	25.9
1,2,3,6,7,8-HxCDD	(2.16)	(1.93)	33.9	209	69.1	40.9
1,2,3,7,8,9-HxCDD	(2.32)	(1.94)	18.9	166	44.6	30.4
1,2,3,4,6,7,8-HpCDD	[4.13]	16	316	1670	750	395
ocop	22.2	30.1	546	2600	1640	686
2,3,7,8-TCDF	(0.927)	(0.9)	21.5	107	39.4	40.2
1,2,3,7,8-PeCDF	(0.996)	(1.05)	. 8	166	72.6	61.6
2,3,4,7,8-PeCDF	(0.917)	(0.978)	20	450	151	125
1,2,3,4,7,8-HxCDF	(1.29)	(1.41)	33.4	327	146	113
1,2,3,6,7,8-HxCDF	(1.25)	(1.31)	29.2	368	182	123
2,3,4,6,7,8-HxCDF	(1.24)	(1.38)	54.3	830	372	235
1,2,3,7,8,9-HxCDF	(1.5)	(1.72)	(1.71)	(4.95)	(4.76)	(4.22)
1,2,3,4,6,7,8-HpCDF	(1.73)	(1.34)	143	1630	871	574
1,2,3,4,7,8,9-HpCDF	(2.1)	(1.61)	27.6	173	199	102
OCDF	(3.06)	(2.29)	142	546	961	462
ITEF TEQ (ND=0; EMPC=0)	0.0222	0.191	51.9	542	188	139
ITEF TEQ (ND=0; EMPC=EMPC)	0.0634	0.191	57.5	542	-208	156
ITEF TEQ (ND=DL/2; EMPC=0)	2.26	2.36	53.0	542	190	7
ITEF TEQ (ND=DL/2; EMPC=EMPC)	2.29	2.36	5.75	542	208	
ITEF TEQ (ND=DL; EMPC=EMPC)	4.52	4.53	57.6	543	208	156
Checkcode Lab ID	480-593-ZVM MB1_11406_DF_SDS	527-902-CWR A6007_11406_DF_001	480-593-ZVM 527-902-CWR 520-615-RKC 996-461-RVQ 800-863-YNS 633-277-HWN MB1_11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_003 A6007_11406_DF_004 A6007_11406_DF_005	996-461-RVQ A6007_11406_DF_003	800-863-YNS A6007_11406_DF_004	633-277-HWN A6007_11406_DF_005

A6007 - WHO-2005-TEQ Project ID: 6028 4905-2100

Sample Summary Part 1	398	ANMACTICAL	ANALTICAL PERSPECTIVES		M	Method 23
Analyte	Method Blank A6007	l5-Blank	15-1	15-2	15-3	15-4
	bd	bd	bd	бd	bd	bd
2,3,7,8-TCDD	(1.54)	(1.68)	[2.34]	12.2	[6.58]	[6.42]
1,2,3,7,8-PeCDD	(2.17)	(1.7)	[6.45]	86.3	[25.8]	[21.5]
1,2,3,4,7,8-HxCDD	(2.18)	(1.76)	13	148	29.9	25.9
1,2,3,6,7,8-HxCDD	(2.16)	(1.93)	33.9	209	69.1	40.9
1,2,3,7,8,9-HxCDD	(2.32)	(1.94)	18.9	166	44.6	30.4
1,2,3,4,6,7,8-HpCDD	[4.13]	16	316	1670	750	395
OCDD	22.2	30.1	546	2600	1640	686
2,3,7,8-TCDF	(0.927)	(0.9)	21.5	107	39.4	40.2
1,2,3,7,8-PeCDF	(0.996)	(1.05)	18	166	72.6	61.6
2,3,4,7,8-PeCDF	(0.917)	(0.978)	50	450	151	125
1,2,3,4,7,8-HxCDF	(1.29)	(1.41)	33.4	327	146	113
1,2,3,6,7,8-HxCDF	(1.25)	(1.31)	29.2	368	182	123
2,3,4,6,7,8-HxCDF	(1.24)	(1.38)	54.3	830	372	235
1,2,3,7,8,9-HxCDF	(1.5)	(1.72)	(1.71)	(4.95)	(4.76)	(4.22)
1,2,3,4,6,7,8-HpCDF	(1.73)	(1.34)	143	1630	871	574
1,2,3,4,7,8,9-HpCDF	(2.1)	(1.61)	27.6	173	199	102
OCDF	(3.06)	(2.29)	142	546	961	462
WHO-2005 TEQ (ND=0; EMPC=0)	999000	0.169	41.0	490	155	111
WHO-2005 TEQ (ND=0; EMPC=EMPC)	0.0479	0.169	49.8	490	187	139
WHO-2005 TEQ (ND=DL/2; EMPC=0)	2.69	2.66	42.6	490	157	114
WHO-2005 TEQ (ND=DLZ; EMPC=EMPC)	2.71	2.66	49.9	490	187	140
WHO-2005 TEQ (ND-DL; EMPC=EMPC)	5.38	5.14	20.0	490	188	140
Checkcode	480-593-ZVM	527-902-CWR	520-615-RKC	996-461-RVQ	800-863-YNS	633-277-HWN
Lab ID	MB1_11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_002 A6007_11406_DF_003 A6007_11406_DF_004 A6007_11406_DF_005	46007_11406_DF_001	A6007_11406_DF_002	A6007_11406_DF_003	A6007_11406_DF_004	A6007_11406_DF_005

A6007 - Totals Project ID: 6028 4905-2100

Sample Summary Part 2	SE	ANALTECA	NALTICAL PERSPECTIVES		Σ	Method 23
Analyte	Method Blank A6007	I5-Blank	12-1	15-2	15-3	15.4
Totals	bd	bd	bd	бd	бd	бd
TCDDs	2.44	0	8.66	509	144	133
PeCDDs	0	0	210	1520	301	245
HXCDDs	0	.0	510	3490	854	516
НрСDDs	0	16	653	3800	1440	845
ОСББ	22.2	30.1	546	2600	1640	686
TCDFs	0	0	732	4090	1040	1070
PeCDFs	0	0	419	4740	1500	1290
HXCDFs	0	0	303	4230	1940	1410
HpCDFs	0	0	257	2420	1760	1040
OCDF	0	0	142	546	961	462
Total PCDD/Fs (ND=0: EMPC=0)	24.6		3.870	28.000		
Total PCDD/Fs (ND=0; EMPC=EMPC)	34.1	63.0	3,890	28,000	11,700	8,060
Total PCDD/Fs (2378-X ND=DL; EMPC=EMPC)	59.5	86.0	3,890	28,000	11,700	8,070
FORIZARS (ND=0, EMPC=0)	22.2	1,467	158	9,490	5,540	3.720
Total 23785 (NE=0'S EMPC=0) Total 23788 (NE=1:TRIPC=0)	36. I	77.0	15/1 15/1	0076		
Total 23788 (ND=0-5, EMPC=0)	0.60	46.1	169.7		105.5 105.5	
Total 2378s (NE=1; EMPC=1)	215		0971	9,490	07.5S	3,550
Checkcode	480-593-ZVM	527-902-CWR	520-615-RKC	996-461-RVQ	800-863-YNS	633-277-HWN
LabID	MB1_11406_DF_SDS	A6007_11406_DF_001	A6007_11406_DF_002	A6007_11406_DF_003	MB1_11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_002 A6007_11406_DF_003 A6007_11406_DF_004 A6007_11406_DF_005	A6007_11406_DF_005

A6007 - Others Project ID: 6028 4905-2100

Sample Summary Part 3	SG	AMMATTERS	ANALTICAL PERSPECTIVES		Ň	Method 23
Analyte	Method Blank A6007	I5-Blank	15-1	15-2	15-3	15-4
Other DCDD/Es /ND-0 EMBC-0	бd	δd	Вd	bd.	6d	Вd
Other PCDD/rs (ND-v, EMPC-V)						
Other TCDD	2.44	0	8.66	497	144	133
Other PeCDD	0 0	0 0	210	1440	301	245
Other HpCDD	0	0 0	337	2120	069	419
Other TCDF	0	C	710	3990	1000	1030
Other PeCDF	0		351	4130	1280	1110
Other HxCDF	0	0	186	2710	1240	937
Other HpCDF	0	0	87.2	624	687	366
Other PCDD/Fs (ND=0, EMPC=EMPC)						-
Other TCDD	2.44	1.81	107	516	157	155
Other PeCDD	0	0	214	1440	330	245
Other HxCDD	0	3.7	444	2970	711	419
Other HpCDD	5.39	11.3	337	2120	069	450
Other TCDF	0	0	710	3990	1010	1040
Other PeCDF	0	0	351	4130	1280	1110
Other HxCDF	0	0	186	2710	1240	937
Other HpCDF	0	0	87.2	624	687	366
Checkcode Lab ID	480-593-ZVM MB1 11406 DF SDS	527-902-CWR A6007_11406_DF_001	480-593-ZVM 527-902-CWR 520-615-RKC 996-461-RVQ 800-863-YNS 633-277-HWN WB1 11406 DF SDS A6007_11406 DF 001 A6007_11406 DF_002 A6007_11406 DF_003 A6007_11406 DF_005	996-461-RVQ A6007_11406_DF_003	800-863-YNS A6007 11406 DF 004	633-277-HWN A6007 11406 DF 005
		! ! !				

A6007 - DLs Project ID: 6028 4905-2100

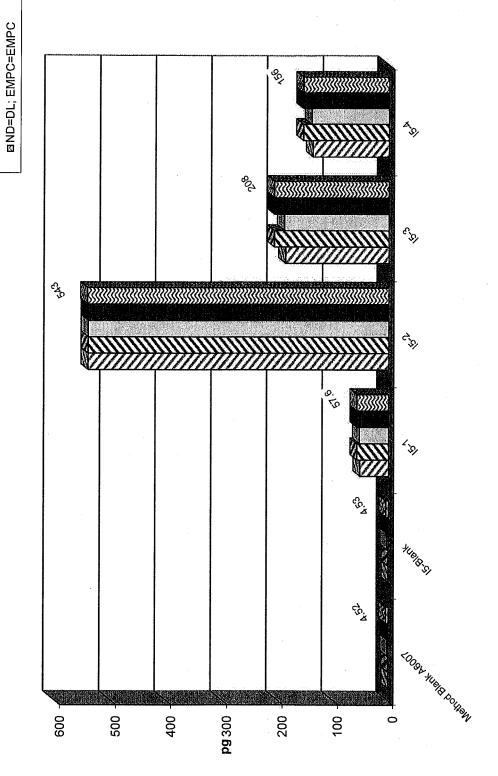
Sample Summary						
Part 5 (DLs)		AMALTITICAL	ANALYTICAL PERGPECTIVES		Σ	Method 23
Analyte	Method Blank A6007	I5-Blank	15-1	7-91	15-3	15.4
	Bd	bd	Вd	pg	bd	bd
2,3,7,8-TCDD	1.54	1.68	1.25	1.72	1.7	2.32
1,2,3,7,8-PeCDD	2.17	1.7	1.74	2.01	2.53	3.21
1,2,3,4,7,8-HxCDD	2.18	1.76	2	2.21	3.23	3.73
1,2,3,6,7,8-HxCDD	2.16	1.93	2.05	2.28	3.56	3.72
1,2,3,7,8,9-HxCDD	2.32	1.94	2.1	2.37	3.56	3.92
1,2,3,4,6,7,8-HpCDD	2.49	2.47	3.02	3.79	5.22	4.18
ocpp	5.94	4.91	4.15	5.86	6.21	4.62
2,3,7,8-TCDF	0.927	6.0	0.862	1.68	1.19	1.37
1,2,3,7,8-PeCDF	0.996	1.05	1.55	4.69	3.25	2.5
2,3,4,7,8-PeCDF	0.917	0.978	1.4	4.3	3.2	2.42
1,2,3,4,7,8-HxCDF	1.29	1.41	1.46	4.21	3.85	3.26
1,2,3,6,7,8-HxCDF	1.25	1.31	1.43	4.06	3.83	3.17
2,3,4,6,7,8-HxCDF	1.24	1.38	1.48	4.04	4.13	3.37
1,2,3,7,8,9-HxCDF	1.5	1.72	1.71	4.95	4.76	4.22
1,2,3,4,6,7,8-HpCDF	1.73	1.34	1.92	4.2	3.58	3.06
1,2,3,4,7,8,9-HpCDF	2.1	1.61	2.19	4.94	4.36	3.89
OCDF	3.06	2.29	2.13	3.39	3.54	3.63
Total TCDD	1.54	1.68	1.25	1.72	1.7	2.32
Total PeCDD	2.17	1.7	1.74	2.01	2.53	3.21
Total HxCDD	2.21	1.87	2.04	2.28	3.43	3.77
Total HpCDD	2.49	2.47	3.02	3.79	5.22	4.18
Total TCDF	0.927	6.0	0.862	1.68	1.19	1.37
Total PeCDF	0.956	1.01	1.48	4.49	3.23	2.46
Total HxCDF	1.31	1.44	1.51	4.29	4.12	3.48
Total HpCDF	1.9	1.47	2.05	4.55	3.94	3.46
Checkcode	480-593-ZVM	527-902-CWR	520-615-RKC	996-461-RVQ	800-863-YNS	633-277-HWN
Lab ID	MB1 11406 DF SDS	A6007_11406_DF_001	// 11406_DF_SDS A6007_11406_DF_001 A6007_11406_DF_002 A6007_11406_DF_003 A6007_11406_DF_004 A6007_11406_DF_005	A600/_11406_DF_003	A6007_11406_DF_004	A600/_11406_DF_005

ITEF-TEQ Project ID: 6028 4905-2100 A6007

■ND=DL/2; EMPC=EMPC

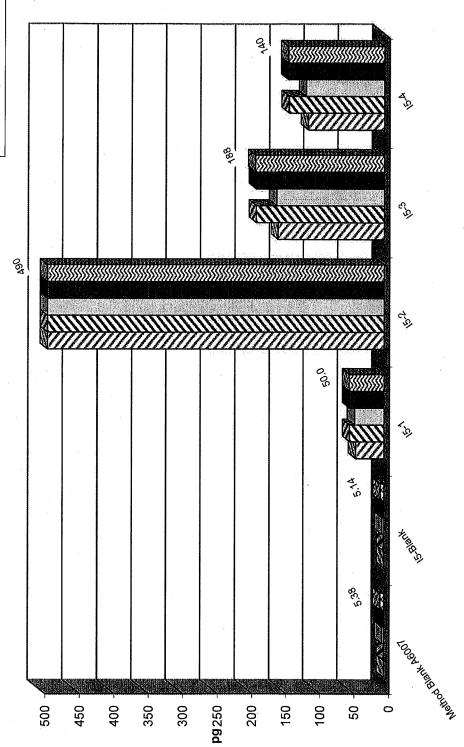
S ND=0; EMPC=EMPC ND=DL/2; EMPC=0

ND=0; EMPC=0



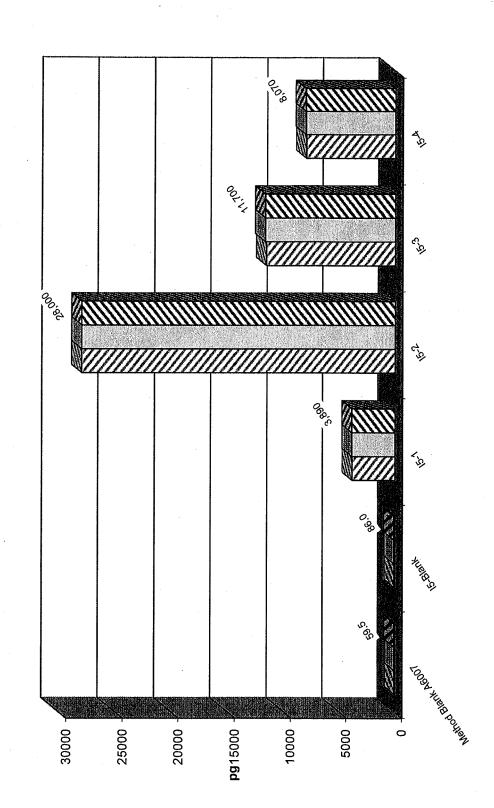
WHO-2005-TEQ Project ID: 6028 4905-2100 A6007

■ND=DL/2; EMPC=EMPC MND=DL; EMPC=EMPC ND=0; EMPC=EMPC END=DL/2; EMPC=0 BND=0; EMPC=0



TotalsProject ID: 6028 4905-2100
A6007





Dev. Std. *(0,00,0_{0,0}0,0 1%, ⊡ Mean & Zo! PO. 70 401.38 (%)* &. C. 0/ 160₀₀ ODOTA DEL O(D)BADE/ OCO VOEV 9 8 8 2 9 20 64 3 20 9 0 Rec.

%

Mean Recoveries of Extraction Standards (N=6)

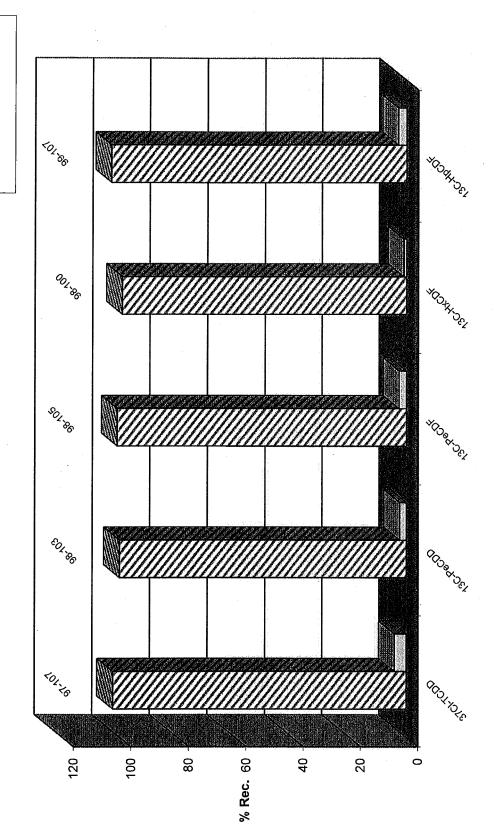
Project ID: 6028 4905-2100

Method Specification Limits: Tetra-Hexa ES: 40-130%, Hepta-Octa ES: 25-130% (F = fail)

Mean Recoveries of Sampling Standards (N=6) Project ID: 6028 4905-2100 A6007

Std. Dev.

⊡Mean



Method Specification Limits: Tetra-Octa SS: 70-130% (F = fail)

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	- "쿡
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South Contraction of the Contrac

	Authoritical Person

Sample ID:	Method BI	ank A6007				Me	Method 23
Client Data		Sample Data		Laboratory Data	ta		
Name:	AECOM	Matrix:	Air	Lab Project ID:	— A6007	Date Received:	n/a
Project ID:	6028 4905-2100	Weight/Volume:	,	Lab Sample ID MB1	-	Date Extracted:	08-Oct-2013
Date Collected:	n/a			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:	1	Time Analyzed:	16:03:53
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	N	1.54		F-50	ES 2378-TCDD	98.1	
12378-PeCDD	ND	2.17		of the constitution for the state of the constitution of the const	ES 12378-PeCDD	102	and an analysis of the second
123478-HxCDD	_ND	2.18			ES 123478-HxCDD	104	
123678-HxCDD		2.16	franch is harfan simmaran ing ing ing harfannak in kalanas anda kalanas ing ing ing ing ing ing ing ing ing ing	and the fact of the factor of	ES 123678-HxCDD	102	
123789-HxCDD	Ŋ	2.32			ES 123789-HxCDD	101	
1234678-HpCDD	EMPC	se promoving community is was a promoved by the promoved of th	4.13		ES 1234678-HpCDD	98.2	
OCDD	22.2				ESOCDD	89.3	
2378_TCDE	<u>UN</u>	2/2010	The second secon		ES.3278 TODE	400	
12378-PACDE	CN CN	0 008			ES 19278 DACHE	701	No. of the control of
23478-PeCDF	Q	0.935			ES 2347&PeCDE	407 407	T rate of the Hillings
123478-HxCDF		1.29			ES 123478-HXCDF	97.6	
123678-HxCDF		7.25			ES 123678-HxCDF	986	
234678-HxCDF		1.24			ES 234678-HxCDF	101	
123789-HxCDF	N	1.5			ES 123789-HxCDF	98.6	100 高
1234678-HpCDF		1.73	den kan kanala dan seriasan keruangan keruangan keruangan keruangan keruangan dan dan kananan dan keruangan da		ES 1234678-HpCDF	97.9	
1234789-HpCDF	9	2.1			ES 1234789-HpCDF	2'86	
OCDF	ND	3.06			ES OCDF	88	
Totals	-				Standard	SS/AS Recoveries	Ş
				The second second second	35 37CI-2378-TCDD	6.86	
Total TCDD	2.44	Company of the control of the contro	2.44		SS 12347-PeCDD	98.6	
Total PeCDD		2.17	ND	The same of the sa	SS 12346-PeCDF	100	
Total HxCDD	N.	2.21	2		SS 123469-HxCDF	100	
Total HpCDD	N		9.51		SS 1234689-HpCDF	104	
		1.600	GIA		AS 1368-TCDD	105	
A COLUMN		0.00			AS 1308-1 CPF	102	
Total Pecur		0.956	מכ				
Total Uncol		2.	ON CIV			The state of the s	iliatio magnitus a accommentation, confirmi magnitus propriessos confirmings and confirming confirm
Total ripodr	צם	P. A. C. Sanderson	מען -			Local Control	
Total PCDD/Fs	24.6		34.1				
ITEF TEQS	El de de l'est en version est de de l'été débit de l'été de l'été de la débit de l'été de l'é	Labeth at Stell and Stells with the with the second Stellar of Stellar Co.	N. HALFA-ACHITARISMENT AND ANNIH MATERIAL MATERIAL NA PROPERTIES AND ANNIH MATERIAL MATERIAL MATERIAL NA PROPERTIES AND ANNIH MATERIAL MATERIAL MATERIAL NA PROPERTIES AND ANNIH MATERIAL MATERI				
TEQ: ND=0	0.0222		0.0634	Č		271	2714 Exchange Drive
TEQ: ND=DL/2	2.26	2.24	2.29			Wilmington	Wilmington, NC 28405, USA
TEQ: ND=DL	7.2	4.49	4.52		ANALYTICAL PERSPECTIVES		www.us.sgs.com
					Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ree 866 846-8290; Fax	: +1 910 794-3919

Report Created: 14-Oct-2013 11:52 Analyst: MC

SGS AP

Checkcode: 480-593-ZVM

Sample ID:	I5-Blank					Me	Method 23
Client Data		Sample Data		Laboratory Data	ata		
Name:	AECOM	Matrix:	Air	Lab Project ID:	A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	_	Lab Sample ID A6007	A6007_11406_DF_001 Date Extracted:	Date Extracted:	08-Oct-2013
Date Collected:	02-Oct-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
·		Split:	2	Dilution:	•	Time Analyzed:	16:56:31
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
237&-TCDD	ND	1.68			ES 2378-TCDD	4.26 F. T.	
12378-PeCDD	N	1.7			ES 12378-PeCDD	92.6	THE PROPERTY AND VALUE OF THE PROPERTY OF THE
123478-HxCDD	ND	1.76			ES 123478-HxCDD	97.4	
123678-HxCDD	QN.	1.93	de de la factoria de la destac	Accession on the separate and the separate separ	ES 123678-HxCDD	95.1	
123789-HxCDD	QN	1.94			ES 123789-HxCDD	92.9	
1234678-HpCDD	16			AB.	ES 1234678-HpCDD	92.7	
OCDD		1000		j B	ES.OCDD	81.9	
2378-TCDF	ND	6.0			ES 2378-TCDF	100	
12378-PeCDF		1.05	Statem of advanced definition for a large of the statement of advanced by State (1) and State (1) an	And the state of t	ES 12378-PeCDF	101	
23478-PeCDF	ND COL	0.978			ES 23478-PeCDF	100	
123478-HxCDF	Q	1.41			ES 123478-HxCDF	93.7	
123678-HxCDF	Q	1.31			ES 123678-HxCDF	93.4	
234678-HxCDF	QN	1.38			ES 234678-HxCDF	94.4	AK OTOK KAROLIN KAROLIN KAROLIN KARONIN KAROLIN KAR
123789-HxCDF	ND	1.72			ES 123789-HxCDF	93	
1234678-HpCDF		1.34	TO SECTION AND ADDRESS OF THE PROPERTY OF THE		ES 1234678-HpCDF	6.06	
1234789-HpCDF	ND	1.61			ES 1234789-HpCDF	94.9	
OCDF	QN	2.29			ES OCDF	86.2	
Totals					Standard	SS/AS Recoveries	S
					SS 37CI-2378-TCDD	101	
Total TCDD			1.81		SS 12347-PeCDD	103	
Total PeCDD		1.7	Q		SS 12346-PeCDF	99,4	
Total HxCDD			3.7	CONTRACTOR WITHOUT WITH WITHOUT WITHOUT WITHOUT WITHOUT WITHOUT WITH WITHOUT WITH WITH WITHOUT WITH WITH WITH	SS 123469-HxCDF	9.66	
Total HpCDD	16		27.4		SS 1234689-HpCDF	102	
		0			AS 1368-TCDD	101	
משו וספו		S.	2	A 1912 Chief Shift Sharper and a second state of the second state	AS 1368-1CUF	9 S	
Total PeCDF	ON	1.01	Q :				
Total HXCDF		T.44	Q			A STATE OF THE PARTY OF THE PAR	
Total HpCDF	ON.	1.47	Q.		And the second s		
Total PCDD/Fs	46.1		63				
ITEF TEQS					-		
TEQ: ND=0	0.197		0.191		7	271	2714 Exchange Drive
TEQ: ND=DL/2	2.36	2.18	2.36	j.	7	Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	4.53	4.37	4.53		ANALYTICAL PERSPECTIVES		www.us.sgs.com
					Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ee 866 846-8290; Fax	: +1 910 794-3919

Checkcode: 527-902-CWR

Report Created: 14-Oct-2013 11:53 Analyst: MC

Sample ID:	15-1					Me	Method 23
Client Data		Sample Data		Laboratory Data	ata		
Name:	AECOM	Matrix:	Air	Lab Project ID:	. A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	· ·	Lab Sample ID A6007	A6007_11406_DF_002		08-Oct-2013
Date Collected:	29-Sep-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:	•	Time Analyzed:	17:48:37
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	EMPC	AND ADDRESS OF THE PARTY OF THE	2.34	ſ	ES 2378-TCDD	87.2	
12378-PeCDD	EMPC		6.45		ES 12378-PeCDD	Se mille authorite and and a second and a se	millionerando politica de distina la mendenada de da
123478-HxCDD	13				ES 123478-HxCDD	89.4	
123678-HxCDD	33.9			· ·	ES 123678-HxCDD	06	And the control of th
123789-HxCDD	18.9				ES 123789-HxCDD	88.5	
1234678-HpCDD	316			A CONTRACTOR OF THE PROPERTY O	ES 1234678-HpCDD	88.6	
OCDD	546				ES OCDD	7.97	
2378-TCDF	21.5				ES 2378-TCDF	9.06	
12378-PeCDF	18		The state of the s	7	ES 12378-PeCDF	92.2	
23478-PeCDF	50				ES 23478-PeCDF	91.1	
123478-HxCDF	33.4			7	ES 123478-HxCDF	85.2	CONTRACTOR OF THE PROPERTY OF
123678-HxCDF	29.2				ES 123678-HxCDF	84.3	
234678-HxCDF	54.3	The state of the s			ES 234678-HxCDF	85.2	
123789-HxCDF	N				ES 123789-HxCDF	87.3	
1234678-HpCDF	143				ES 1234678-HpCDF	80.8	er (CV) kery (CV) min Christian den den den den den den den den den de
1234789-HpCDF	27.6			-	ES 1234789-HpCDF	88.4	
OCDF	142				ES OCDF	81.4	
Totals					Standard	SS/AS Recoveries	Ş
A Company of the Comp			Market 12 Total	THE SEC. (12)	SS:37CI-2378-TCDD	107	
Total TCDD	8.66	Selling Co. (1997) CO. (1998) Selling Co. (1998) Co. (1998) Selling Co	109		SS 12347-PeCDD	98.1	
Total PeCDD	210		221		SS 12346-PeCDF	99.7	
Total HxCDD	510	Additional Communication (A. Landerschaft General Company (American Company) (American Company)	510		SS 123469-HxCDF	98.8	
Total HpCDD	653 ·····		653	10 1 11 10 10 10 10 10 10 10 10 10 10 10	SS 1234689-HpCDF	105	
Wilder Control of the	A COLOR STATE OF THE STATE OF T				AS 1368-TCDD	91	
lotal ICUF	(32	A Colombia C	727		AS 1368-TCDF	92.6	Section (1977) and the section of th
Total PeCDF	419		419			The second secon	
Total HxCDF	303		303				
Total HpCDF	257		257	TO THE CONTRACT OF THE CONTRAC	CHEST CONTRACTORY OF CONTRACTOR AND CONTRACTOR AND CONTRACTOR AND CONTRACTOR AND CONTRACTOR AND CONTRACTOR CONTRACTOR AND CONT		
Total PCDD/Fs	3870		3890				
TEFTEOS	NETERIECALADAM AMAZINA MENANDALISMA P. M. SE MENIN MENINTERIA MENI	TO ALL OF ALL YELD DELWAY, EACH ON COURT HOW COME THAT ALL WAY, ADDITY A VENOUS AND ALL YELD DELWAY,	estimate de destación de la company de la company de la company de la company de la company de la company de la				
TEQ: ND=0	51.9		57.5			271	2714 Exchange Drive
TEQ: ND=DL/2	53	2.14	57.5		7,	Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	54.2	4.28	57.6		ANALTHCAL PICEFECTIVES		www.us.sgs.com
					Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ee 866 846-8290; Fax	:: +1 910 794-3919

Report Created: 14-Oct-2013 11:53 Analyst: MC

Checkcode: 520-615-RKC

Sample ID:	: 15-2					Me	Method 23
Client Data		Sample Data		Laboratory Data	ta		
Name:	AECOM	Matrix:	Air	Lab Project ID:		Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	_	Lab Sample ID A6007		Date Extracted:	08-Oct-2013
Date Collected:	30-Sep-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:		Time Analyzed:	18:41:14
Analyte	Conc. (pg)	DF (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	12.2				ES 2378-TCDD	6.06	
12378-PeCDD	86.3	ACON OR AND STRANGE STREET, THE STREET STREET, THE STREET STREET, THE STREET,	operation of a finite of the contract of the second of the contract of the con	of Controllarian with 18 Addition from the Controllarian and the controllarian and	ES 12378-PeCDD	94.1	- School and Milliam House Commission of the Com
123478-HxCDD	148				ES 123478-HxCDD	95.2	
123678-HxCDD	209	e de la desta de la facto de la facto de la facto de la facto de la facto de la facto de la facto de la facto d		eal talent in the figure of the following the figure of th	ES 123678-HxCDD	94.4	
123789-HxCDD	166				ES 123789-HxCDD	- 35	
1234678-HpCDD	1670				ES 1234678-HpCDD	94.7	
OCDD	2600				ES OCDD	84.3	
						TO CAMP TO THE PROPERTY OF THE	of Autoritical Contributed Contributed Automotivale Automotivale value for the last
2378-TCDF	201	Control of the Contro			ES 2378-TCDF	95.5	And an other from a first first first first
12378-PeCDF	166	AND ALL MAYON ARREST ONLY DESIGNATION OF A STATE OF A S	Additional de la cité de la contraction au contraction de la contraction de la cité de la cité de la contraction de la c	i golimani i sporimentara indica adapti in princita. Na popula dentifica ballana di disabata	ES 12378-PeCDF	90.9	The control of the co
23478-PeCDF	450			1000年の第二日の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本	ES 23478-PeCDF	93.2	
123478-HxCDF	327	a de la companya del la companya de		inde de la companya d	ES 123478-HxCDF	91.1	and it is interpreted to the control of the control
123678-HxCDF	368				ES 123678-HxCDF	94	
234678-HxCDF	830	A manifest Transford provides spendidge to through the period of the second spendidge of the contract of the c	kais perekti relika Virazitatek Chika tande, milani kan		ES 234678-HxCDF	93.9	
123789-HxCDF		4.95			ES 123789-HxCDF	94.9	
1234678-HDCDF	1630				FS 1234678-HnCDF	90.6	
1234789-HnCDF					ES 1234789-HnCDE	91.0	e all the season of the fell of the season of the
OCDE	715 546				ES OCHE	9.1.9 A 7.0	
. ,	2					5.10	
lotais		And the second of the second o			Standard	SS/AS Recoveries	S
					SS 37CI-2378-TCDD	103	
Total TCDD	206	enderveldenen. Westerbijderen de minden, det die kontre einst hat die Spalan in 1900.	528	Section and the section of the secti	SS 12347-PeCDD	98.9	
Total PeCDD	1520		1520		SS 12346-PeCDF	The 103	
Total HxCDD	3490		3490		SS 123469-HxCDF	97.7	
Total HpCDD	3800		3800		SS 1234689-HpCDF	101	
					AS 1368-TCDD	95.8	
Total TCDF	4090		4090		AS 1368-TCDF	94.8	
Total PeCDF	A 740	o distribution de la company d	4740	OF THE AND STATES AND STATES AND AND AND AND AND AND AND AND AND AND	pirobili Kasilini dalifannak vanabbalka ore alba kenda bar kanake karake uri est och banana.	o Norwick of continues on the Millian Davids, who were a mathematical data for the continues.	nin aya igasanan ahan aya mada baharan in isan dara Abada in i
Total HxCDF	4230		4230				
Total HpCDF	2420	A MORNING AND THE STATE OF THE	2420	en de de la company de la comp	en et engelegende der der der der de der de de de de de de de de de de de de de	de constitucionale de la Transaction de companya de la companya de la companya de la constitución de propositi	CONFIT WORKS AND AND AN FIRM MICHARM CONCOUNT AND AND AND AND AND AND AND AND AND AND
Total PCDD/Fs	28000		28000				
ITEF TEQS							
TEQ: ND=0	542		542	Č		271	2714 Exchange Drive
TEQ: ND=DL/2	542	3.92	542		J	Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	543	7.83	543		MWW.US.SGS.COM Tel: +1 910 794-1613: Toll-Free 866 846-8290: Fax: +1 910 794-3919	Pe 866 846-8290 Fax	www.us.sgs.com
Checkcode: 996-461-RVQ	ď	SGS AP D/F 2013 Rev. 2.6	ev. 2.6		Report C	Report Created: 14-Oct-2013 11:53 Analyst: MC	1:53 Analyst: MC

Sample ID:	15-3					Me	Method 23
Client Data		Sample Data		Laboratory Data	ıta		
Name:	AECOM	Matrix:	Air	Lab Project ID:	— A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	-	Lab Sample ID A6007	- 1	Date Extracted:	08-Oct-2013
Date Collected:	01-Oct-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:	3	Time Analyzed:	19:33:47
Analyte	Conc. (pg)	DL (pg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	EMPC	50 120	6.58	Service Services	ES 2378-TCDD	88.5	
12378-PeCDD	EMPC	AND AND AND AND AND AND AND AND AND AND	25.8		ES 12378-PeCDD	89.9	i o na strikenska prok nast Norde, malasia k Releia di Salasia.
123478-HxCDD	Service 129.9				ES 123478-HxCDD	91.9	
123678-HxCDD	69.1	את היא לאחרים את היא היא היא היא היא היא היא היא היא היא			ES 123678-HxCDD	89.4	
123789-HxCDD	44.6				ES 123789-HxCDD	90.5	
1234678-HpCDD	750				ES 1234678-HpCDD	91.7	
OCDD	1640				ESOCDD	83.1	
	i kirk jak k. jak saatingges o dgest despessentense op kenne proposition og den skrivet og den skrivet og den skrivet		KTOFFFFFFOR SCHOOLSCHOOL STREETING STOT KNOCK, WASHING STAGE OF THE SCHOOL OF THE	Total contraction and active contraction and a sake district contraction of the contracti	ANALYSIAN ANALYSIAN TANANAN ANALYSIAN ANALYSIAN ANALYSIAN ANALYSIAN ANALYSIAN ANALYSIAN ANALYSIAN ANALYSIAN AN	NA FRANKLIK (Fr & NY KALIMY V CANDELLE KARLAN) KITATO KONJOGA FANYANINA	desidada one de sudas see de esta esta designada esta designada de se sus estados.
2378-TCDF	39,4	214			ES 2378-TCDF	92.3	
12378-PeCDF	72.6				ES 12378-PeCDF	89.6	VA. Printisti, in cell Conf. co. indicate. V. c. Anti. additional and department of the conf. of the cell and cell a
23478-PeCDF	151				ES 23478-PeCDF	91.2	
123478-HxCDF	146				ES 123478-HxCDF	87.9	And hard grade and an experience of the control of
123678-HxCDF	182				ES 123678-HxCDF	87.9	State of the state
234678-HxCDF	entraperspecies production for the final section of	TO WELL WITH THE THE PROPERTY OF THE PROPERTY			ES 234678-HxCDF	87.6	
123789-HxCDF	N	4.76			ES 123789-HxCDF	88.7	
1234678-HpCDF		en en en en en en en en en en en en en e	and deposits the fall with the second to the second second second second second second second second second se	opportune Anthonomis in wants subsidiated that should be subsidiated to the subsidiate of the subsidiated to the subsidiate of the subsidiated to the subsidiate of the subsidiate of the subsidiated to the subsidiate of the subsi	ES 1234678-HpCDF	87.8	
1234789-HpCDF	199				ES 1234789-HpCDF	87.6	
OCDF	961				ES OCDF	83.9	
Totals					Standard	SS/AS Recoveries	·
	Applications of the second second second second second second second second second second second second second				SS 37CI-2378-TCDD	26	
Total TCDD	144		164		SS 12347-PeCDD	98.8	
Total PeCDD	301		355		SS 12346-PeCDF	98.3	in the second se
Total HxCDD	854		854		SS 123469-HxCDF	99.1	
Total HpCDD	1440		1440	And the second s	SS 1234689-HpCDF	99.3	
		Service Conservation Conservati			AS 1368-TCDD	95	
Total TCDF	1040	Medition the Manager of the Assessment of the As	1050		AS 1368-TCDF	92.3	
Total PeCDF	1500		1500			The second and week the second for the second for the second seco	The state of the s
Total HxCDF	1940		1940			And the second s	
Total HpCDF	1760		1760				
Total PCDD/Fs	11600		11700				
ITEF TEQS							
TEQ: ND=0			208			271	2714 Exchange Drive
TEQ: ND=DL/2	190	3.84	208	J,		Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	192	7.68	208		ANALTICAL PIDEFECTIVES		www.us.sgs.com
THE RESERVE AND ADDRESS OF THE PROPERTY OF THE	And the second section of the second section is the second section of the second section is the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the second section is the second section in the second section in the section is the second section in the section is the second section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is the section in the section is t	der Arte der der der der der der der der der de	ade hade adequate titler of a base and september and representative expression of a constructive and a const		Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ree 866 846-8290; Fax	: +1 910 794-3919

Report Created: 14-Oct-2013 11:53 Analyst: MC

Checkcode: 800-863-YNS

Sample ID:	: 15-4					Me	Method 23
Client Data		Sample Data		Laboratory Data	ıta		
Name:	AECOM	Matrix:	Air	Lab Project ID:	A6007	Date Received:	07-Oct-2013
Project ID:	6028 4905-2100	Weight/Volume:	Ψ-	Lab Sample ID A6007	_11406_DF	005 Date Extracted:	08-Oct-2013
Date Collected:	02-Oct-2013			QC Batch No:	11406	Date Analyzed:	13-Oct-2013
		Split:	2	Dilution:		Time Analyzed:	20:26:26
Analyte	Conc. (pg)	DF (bg)	EMPC (pg)	Qualifiers	Standard	ES Recoveries	Qualifiers
2378-TCDD	SMPC		6.42	5	ES 2378-TCDD	93.5	
12378-PeCDD	EMPC		21.5	_	ES 12378-PeCDD	94.8	Koliniski kantili ishinda darimba darimba darimba darimba darimba darimba darimba darimba darimba darimba dari
123478-HxCDD	25.9				ES 123478-HxCDD	93.8	
123678-HxCDD	40.9	We describe of factor applications are to be a solution of the factor of			ES 123678-HxCDD	93.4	
123789-HxCDD	30.4				ES 123789-HXCDD	93.4	
1234678-HpCDD	395	CONTRACTOR OF THE PROPERTY OF			ES 1234678-HpCDD	90.2	
ОСОО	686				ES OCDD	82.3	
2378-TCDF	40.2				ES 2378-TCDF	96.5	
12378-PeCDF	61.6				ES 12378-PeCDF	98.7	
23478-PeCDF	125				ES 23478-PeCDF	96.2	
123478-HxCDF	113	edetrorous action of a file of the composition of t			ES 123478-HxCDF	91.7	
123678-HxCDF	123				ES 123678-HxCDF	92.6	
234678-HxCDF	235				ES 234678-HxCDF	91.7	District of a summer of order of the control of the
123789-HxCDF	ND	4.22			ES 123789-HxCDF	92.3	
1234678-HpCDF	574			employees an un consequent conseq	ES 1234678-HpCDF	84.8	i na Pandalatan ya ka ka ka ka ka ka ka ka ka ka ka ka ka
1234789-HpCDF	**************************************			A Million about the second of	ES 1234789-HpCDF	92.2	
OCDF	462				ES OCDF	84.3	
Totals					Standard	SS/AS Recoveries	ý
					SS 37CI-2378-TCDD	107	
Total TCDD	133	el promptograpo propo i deserá el Compa de Compa de Compa de Compa de Compa de Compa de Compa de Compa de Comp	161	The second secon	SS 12347-PeCDD	103	
Total PeCDD	245		266		SS 12346-PeCDF	105	
Total HxCDD	516		516		SS 123469-HxCDF	100	
Total HpCDD	845		845		SS 1234689-HpCDF	107	
	And the second s				AS 1368-TCDD	100	
lotal ICUF		A STATE OF THE PARTY OF THE PAR	1080	M. 1	AS 1368-TCDF	66	And the second s
Total PeCDF	1290	Control of the Contro	1290	h) / dell' = 1.0 4 del Cilinate - c. al dend'i pupili di 17 consent del Cilinate - c. al dell'anni di pupili di	2004 w haarin Wahaa aadda Offiadh waa aadh mee' Noo ya go badh ah ma'a ab dadabha dhaan dha in bhaba	en endigeneemble optimisel ook besteld ook ontdoor op de ook 2000 ook 00000	The control of the co
Total HxCDF	1410		1410				
Total HpCDF	1040		1040				
Total PCDD/Fs	8010	A CONTROL OF THE CONT	8060				
ITEF TEQS	,						
TEQ::ND=0	139		156			271	2714 Exchange Drive
TEQ: ND=DL/2	141	4.03	156		7	Wilmingtor	Wilmington, NC 28405, USA
TEQ: ND=DL	143	8.06	156		ANALYTICAL PERSPECTIVES		www.us.sgs.com
					Tel: +1 910 794-1613; Toll-Free 866 846-8290; Fax: +1 910 794-3919	ee 866 846-8290; Fax	: +1 910 794-3919

Checkcode: 633-277-HWN

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SGS AP D/F 2013 Rev. 2.6

Report Created: 14-Oct-2013 11:54 Analyst: MC

AECOM Environment

Appendix C

Calibration Data

Clean Air Engineering - Meter Box Full Test Calibration

O.Lavrov 06/11/13 R.Redel Reviewed By: Calibrated By: Date of Calibration: AECOM n/a n/a Client: ID No: Dept No:

28.99 in. Hg W12637 Barometer Serial No: Barometric Pressure: in. H₂O 06/11/14 1.0 Due Date of Calibration: Meter Box Vacuum: Meter Box Serial No: 0028-061113-1 0028 Manufacturer Part No:

	1.0034	1.7732
Calibration Signature:	Meter Box Yd:	Meter Box ∆H@:

ion S		ΔH@	1.8203	1.8178	1.7443	1.7394	1.7621	1.7554	1.77321	
Calibration Results		۲	1.0053	1.0046	1.0057	1.0051	0.9992	1.0005	1.00339	
Time (min.)		Θ	12.56	12.54	14.21	14.19	10.09	10,08	Averages	
Œ.	T	Avg.	91.50	91.00	95.50	95.50	95.50	96.50		
Meter Box Temperature ('F)	T	Out	0.06	89.0	91.0	91.0	90.0	91.0		
	F	٥	93.0	93.0	100.0	100.0	101.0	102.0		
C	Tds	Avg.	77.00	77.00	77.00	00'22	77.00	77.00		
Std. Meter Temperature (F)	Tos	Out	77.0	77.0	77.0	77.0	0.77	77.0		
Ter	**************************************	드	77.0	77.0	77.0	77.0	77.0	77.0		
sas 3 ₁	٩	Net	5.086	5.085	10,210	10,217	10.228	10.233		
Meter Box Gas		Final	132.507	137,592	113.533	123.750	84.633	94.866		
We	/	Initia	127.421	132.507	103,323	113,533	74,405	84,633		
Weter s (#3)	\$ ^	Net	5.000	5.000	10.000	10.000	10.000	10.000		
Standard Meter		Final	5.000	5,000	10.000	10.000	10.000	10.000		
Sta		Initial	000'0	0.000	000'0	0.000	000'0	000'0		
		æ	8	0000	800	8	8	8		

11.		10.08 Averages	96.50	90.0	102.0	77.00	77.0	77.0	10.233	94.866	84,633	10.000	10.000	0.000	1.0000	-1.80	$\neg \neg$	3.00
1.0051 1.73		14.19	95.50	91.0	100.0	77.00	77.0	77.0	10.217	123.750	113,533	10.000	10.000	0.000	0000	-	-1.40 1.0	Ľ
\dashv		-	95.50	91.0	100.0	77.00	77.0	0.77	10,210	113.533	103,323	10.000	10.000	0,000	0000	_	-1.40	
1.0046 1.81		12.54	91.00	89.0	93.0	77.00	77.0	77.0	5.085	137,592	132.507	5.000	5,000	0.000	0000		-1.20	Ë
┪	Ì	4	91.50	0.06	93.0	77.00	77.0	77.0	5.086	132.507	127.421	5.000	5.000	0,000	1.0000	L	-1.20	0.50 -1.20
Υ _d	_	Θ	Avg.	Ont	드	Avg.	Ont	딘	Net	Final	Initial	Net	Final	Initial	۲å		ЧЪ	ΔH ΔP

(0) (0) (0) (0) (0)	
	1
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	- 6
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0000 0000 0000 0000 0000 0000 0000 0000 0000	{ -
1,0060 1,0040 1,0020 1,0000 1,9980 1,9960	Ď.

Average CFM

ange	Gauge	(in.Hg)	5.0	10.0	15.0	20.0	25.0		-
Vacuum Gauge	Standard	(in.Hg)	4.8	9.6	14.9	20.1	25.1		
∑					<u>'</u>			_	

Equations	$Y_{d} = (Y_{ds}) \left[\frac{V_{ds}}{V_{d}} \left[\frac{T_{d} + 460}{T_{ds} + 460} \left[\frac{P_{b} + \Delta P / 13.6}{P_{b} + \Delta H / 13.6} \right] \right]$ $\Delta H \textcircled{@} = \frac{(0.0319)(\Delta H)}{P_{b}(T_{c} + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^{2}$ $Q = \frac{17.64(V_{ds})(P_{b})}{(T_{ds} + 460)(\Theta)}$
Nomenclature	Barometric Pressure (in. Hg) Flow Rate (cfm) Orflice Pressure differential (in. H ₂ O) Inlet Pressure Differential (in. H ₂ O) Gas Meter Volume - Dry (it²) Standard Meter Volume - Dry (it²) Average Meter Box Temperature ('F) Outlet Meter Box Temperature ('F) Average Standard Meter Temperature ('F) Meter Correction Factor (unitless) Orifice Pressure Differential giving 0.75 cfm of air at 68'F and 29.92 in. Hg (in. H ₂ O) AH@,s AH@ _{svg} +0.2 Duration of Run (minutes)
	۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵ ۵

tion	Pass	Pass	Pass
ration Inspec	Electrical Check:	Pyrometer Checl	YD Tolerance: ± 2% of 1.0000
-Calib	Pass	Pass	Pass
Meter Box Pre-Calibration Inspection	Positive Leak Check:	Negative Leak Check:	Vacuum Gauge Check
8.3			

7/22/2012 7/23/2013

Calibration Due Date:

11AG9

Serial No: Date Calibrated:

Reference Used: Wet Test Meter Calibrated By: Martin Vaquero

Percent Error:

Calibration Reference Information (Standard Meter)

Meter Box - Pyrometer Calibration Sheet

 Meter Box No:
 0028-061113-1
 Office:
 Clean Air 80

 Calibrated by:
 O.Lavrov
 Client:
 AECOM

 Date:
 6/11/13
 Job No:
 N/A

 Temperature Scale Used:
 Fahrenheit
 Type of Calibration:
 Full-Test

Calibration			Pyron	neter Re	ading	•	
Reference			for e	ach Cha	nnel		
Settings				(°F)			
(°F)	1	2	3	4	5		
	Stack	Probe	Filter	Imp Out	Aux		
50	50	49	50	50	50		
100	100	99	100	100	100		╝
150	150	149	150	150	150		
200	200	199	200	200	200		
250	250	249	250	250	250		
300	300	299	300	300	300		
350	350	349	350	350	350		
400	400	399	400	400	400		
450	450	449	450	450	450		
500	500	499	500	500	500		
550	550	549	550	550	550		
600	600	599	600	600	600		

Tolerance = ±2°F difference from reference setting.

Calibration Reference Information

Reference Used: Omega CL23A Serial No: T-279500

Calibrated By: JH Metrology Date Calibrated: 8/20/2012

Calibration Report No: 1000164078 Calibration Due Date: 8/20/2013



Alternative RM-5 Post Test Calibration
SMMI - Pogo Mine
Particulate and Hydrogen Chloride Sample Runs
Incinerator
09/29/13

	0.9987	1.0054	1.0020	1.0020
SQRT (in. H ₂ O)	1.31	1.28	1.28	Average
(in. H ₂ O)	1.71	1.63	1.63	
(acf)	60.407	57.485	58.110	
(°R)	520.3	528.7	525.3	
(°F)	60.3	68.7	65.3	
(in. Hg)	28.00	28.25	28.40	
	29.63	29.67	29.59	
-	1.7732	1.7732	1.7732	
(min)	81	79	80	
	Hawkeye	Hawkeye	Hawkeye	
	15-1	15-2	15-3	
	$(min) \qquad \qquad (in. Hg) \qquad (^{\circ}F) \qquad (^{\circ}R) \qquad (acf)$	(min) (in. Hg) (°F) (°R) (acf) (in. H2O) SQRT (in. H2O) 81 1.7732 29.63 28.00 60.3 520.3 60.407 1.71 1.31	Hawkeye (min) (min) (in. Hg) (°F) (°R) (°R) (in. H ₂ O) SQRT (in. H ₂ O) Hawkeye 79 1.7732 29.63 28.25 68.7 528.7 57.485 1.63 1.28	Hawkeye Road (in. Hg) (°F) (°F) (°R) (in. H ₂ O) Hawkeye 81 1.7732 29.67 28.00 60.3 520.3 60.407 1.71 Hawkeye 79 1.7732 29.67 28.25 68.7 528.7 57.485 1.63 Hawkeye 80 1.7732 29.59 28.40 65.3 525.3 58.110 1.63

% Difference	0.14%	
Meter Y _d	1.0034	
Average $ m Y_{dq}$	1.0020	

The difference between the average Yqa for the three runs and the meter box Yd must be within five percent to pass the calibration

Reference: Roger T. Shigehara, P.G. Royals, and E.W. Steward, "Alternative Method 5 Post-Test Calibration", Entropy Inc.

Alternative RM-5 Post Test Calibration
SMMI - Pogo Mine
Dioxin and Furans Sample Runs
Incinerator
09/29/13

2010	1_0										
1.0133	Average										
1.0194	1.27	1.62	90.196	525.2	65.2	28.40	29.67	1.7732	127	Hawkeye	I23-3
1.0132	1.28	1.64	688.06	515.7	55.7	28.20	29.68	1.7732	127	Hawkeye	I23-2
1.0073	1.28	1.64	92.252	522.8	62.8	28.05	29.63	1.7732	127	Hawkeye	123-1
	SQRT (in. H ₂ O)	(in. H ₂ O)	(acf)	(°R)	(°F)	(in. Hg)			(min)		
<u> </u>)							TIME	BOX	
Y	(SQRT dH) _{avs}	dHave	V _{dm}	T_{dm}	$T_{\sf dm}$	P _b	M	dH@	RUN	METER	RUN#

% Difference	0.97%
Meter Y _d	1.0034
Average Y _{dq}	1.0133

The difference between the average Yqa for the three runs and the meter box Yd must be within five percent to pass the calibration

Reference: Roger T. Shigehara, P.G. Royals, and E.W. Steward, "Alternative Method 5 Post-Test Calibration", Entropy Inc.

Alternative RM-5 Post Test Calibration

SMMI - Pogo Mine

Metals Sample Runs Incinerator 09/29/13

	1 0068	Average										
	1.0030	1.28	1.63	91.847	522.5	62.5	28.40	29.66	1.7732	127	Hawkeye	129-3
	1.0058	1.28	1.63	92.412	529.9	6.69	28.25	29.66	1.7732	127	Hawkeye	129-2
	1.0115	1.28	1.63	43.625	530.2	70.2	28.00	29.69	1.7732	09	Hawkeye	129-1
		SQRT (in. H ₂ O)	(in. H ₂ O)	(acf)	(°R)	(°F)	(in. Hg)			(min)	·	
	$ m Y_{qa}$	(SQRT dH) _{avg}	$^{ m q}$	$V_{\sf dm}$	T	T_{dm}	Д	M _d	@Hp	RUN	METER BOX	RON #
_					1	(,	•	()	֡֝֝֝֝֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	מתה ל	ח ועונים

nce	
% Differe	0.34%
Meter Y _d	1.0034
Average Y _{dq}	1.0068

The difference between the average Yqa for the three runs and the meter box Yd must be within five percent to pass the calibration

Reference: Roger T. Shigehara, P.G. Royals, and E.W. Steward, "Alternative Method 5 Post-Test Calibration", Entropy Inc.

AECOM

PROBE CALIBRATION FORM

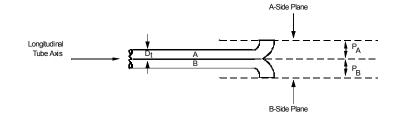
S-TYPE CALIBRATION DATA

403 Date: 8/13/2013 Technician: Probe ID: D. Bopray

0.375 in. $3/16 \le D_t \le 3/8$ $D_t =$

0.449 in. $1.05D_t \le P \le 1.50D_t$

0.449 $P_B =$ in. $P_A = P_B$



 $a_1 =$ $a_1 \le 10^{\circ}$

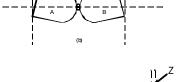
 $a_1 \le 10^{\circ}$ $a_2 =$

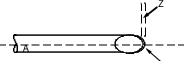
2 $b_2 \leq 5^{\circ}$ $b_1 =$

3 $b_2 \le 5^\circ$ $b_2 =$

0.000 in. **Z** =

 $Z \le 0.125$ " $W \le 0.031$ " **W** = in.







THERMOCOUPLE CALIBRATION DATA **Traceable** Thermocouple ID#: 403 Standard ID #: S/N 111976025 Ambient Temp (F°): 76 Barometric Pressure (in. Hg): 25.3

Temperature Reference Point	Source	Reference Temperature R °	Thermocouple Potentiometer Temperature	Temperature Difference (%) ≤ 1.5 %
0 C° (32 F°)	Ice Water	494	493.9	0.02
100 C° (212 F°)	Boiling Water	665	663	0.30
~25° C (~75°F)	Ambient	536	535	0.19
150-250 C° (300-500 F°)	Hot Oil	778	775	0.39
			·	

Thermocouple ID	IO-021	Standard ID Traceable S/N 11197602	
Date	9/14/2013	Ambient Temp.(°F) 76	
Barometric Pressure (in Hg)	25.3	· · · · · · · · · · · · · · · · · · ·	
Calibrator	D. Bopray		

Temperature Reference Point	Source	Reference Temperature (R)	Thermocouple Potentiometer Temperature (R)	Temperature Difference (%)
(32°F)	Ice Water	492	493	-0.20
(75°F)	Ambient	537	538	-0.19
(212°F)	Boiling Water	659	658	0.15

R= °F+460

Temperature Difference (%) <= 1.5%

Thermocouple ID	IO-031	Standard ID	Traceable S/N 111976025
Date	8/14/2013	Ambient Temp.(°F)	76
Barometric Pressure (in Hg)	25.3	_	
Calibrator Calibrator	D. Bopray	_	

Temperature Reference Point	Source	Reference Temperature (R)	Thermocouple Potentiometer Temperature (R)	Temperature Difference (%)
(32°F)	Ice Water	493	494	-0.20
(75°F)	Ambient	537	537.3	-0.06
(212°F)	Boiling Water	661	660	0.15

R= °F+460

Temperature Difference (%) <= 1.5%

Thermocouple ID_	IO-032	Standard ID Traceable S/N 111976025
Date	8/14/2013	Ambient Temp.(°F) 76
Barometric Pressure (in Hg)	25.3	
Calibrator	D. Boprav	

Temperature Reference Point	Source	Reference Temperature (R)	Thermocouple Potentiometer Temperature (R)	Temperature Difference (%)
(32°F)	Ice Water	494	493.8	0.04
(75°F)	Ambient	537	538	-0.19
(212°F)	Boiling Water	661	659	0.30

R= °F+460

Temperature Difference (%) <= 1.5%

Thermocouple ID	IO-033	Standard ID Traceable S/N 1119760	
Date	8/14/2013	Ambient Temp.(°F) 76	
Barometric Pressure (in Hg)	25.3	· · · · · · · · · · · · · · · · · · ·	
Calibrator	D. Bopray		

Temperature Reference Point	Source	Reference Temperature (R)	Thermocouple Potentiometer Temperature (R)	Temperature Difference (%)
(32°F)	Ice Water	494	494.5	-0.10
(75°F)	Ambient	536	536	0.00
(212°F)	Boiling Water	660	657	0.45

R= °F+460

Temperature Difference (%) <= 1.5%

Analyzer Calibration

A=COM

Client	SMMI - Pogo
Location	Delta Junction, AK
Source ID	Incinerator
Operator	J Rosburg
Date	09/29/13
Initial Cal Time	0910-0927
Final Cal Time	1941-1955

Cylinder #, Su	pplier, & Conc.
cc237902 NO:	x 46.31 CO 45.39 SO2 44.95
cc20720 NOx 9	92.01 CO 91.66 SO2 90.1
xc0094123 NO	ox 236.5 CO 230.3 SO2 234.9
cc37929 O2 19	0.98 CO2 19.41
cc255539	O2 10.01 CO2 10.13

Analyzer_	NOx
Full Scale	236.5
Analyzer	CO
Full Scale	91.7
Analyzer	
Full Scale	
Analyzer	SO2
Full Scale	90.1
Analyzer	O2
Full Scale	19.98
Analyzer	CO2
Full Scale	19.41
_	

Model	TEI 42C
Serial #	
Model	TEI 48C
Serial #	
Model	
Serial #	
Model	AMETEK 921
Serial #	
Model	Sevomex1440
Serial #	
Model	Sevomex1440
Serial #	

				1	1	
		Cylinder	Analyzer	Absolute	Per	cent
		Value	Response	Difference		rence
		(ppm/%)	(ppm/%)	(ppm/%)	(% of span)	(Pass/Fail)
Analyzer NOx	Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	92.0	91.4	0.6	0.0	Pass
initiai Anaiyzei Response	High-Range	236.5	236.9	0.4	0.2	Pass
	111gii 111111gi	2000	2000	VI.	V.2	2 400
	Zero	0.0	0.0	0.0	0.0	Pass
Analyzer Response	Mid-Range	92.0	92.0	0.0	0.0	Pass
	High-Range	236.5	238.5	2.0	0.8	Pass
	_					
Analyzer CO	Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	45.4	46.4	1.0	1.1	Pass
	High-Range	91.7	92.4	0.7	0.8	Pass
	Zero	0.0	-0.8	0.8	0.9	Pass
Analyzer Response	Mid-Range	45.4	46.5	1.1	1.2	Pass
Analyzer Response	High-Range	91.7	93.1	1.4	1.6	Pass
	Ingn-Kange	71.7	75.1	1,4	1.0	1 433
Analyzer SO2	Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	45.0	44.9	0.1	0.1	Pass
	High-Range	90.1	90.7	0.6	0.7	Pass
	Zero	0.0	-1.5	1.5	1.7	Pass
Analyzer Response	Mid-Range	45.0	45.8	0.8	0.9	Pass
	High-Range	90.1	91.5	1.4	1.6	Pass
Analyzer Predict	ed Zero					
Initial Analyzer Response	Mid-Range					
ilitiai Aliaiyzei Kesponse	Mid-Range					
* Cal. through CEM system	High-Range					
Predict	ed Zero					
Analyzer Response	Mid-Range					
	Mid-Range					
* Cal. through CEM system	High-Range					
Analyzer O2	Zero	0.00	0.01	0.0	0.1	Dogg
Initial Analyzer Response	Mid-Range	10.01	10.05	0.0	0.1	Pass Pass
finitiai Anaiyzei Kesponse	High-Range	19.98	20.08	0.0	0.5	Pass
	Zero	0.00	0.00	0.0	0.0	Pass
Analyzer Response	Mid-Range	10.01	10.07	0.1	0.3	Pass
	High-Range	19.98	20.16	0.2	0.9	Pass
Analyzan CO2	7	0.00	0.04	0.0	0.2	D
Analyzer CO2	Zero	0.00	9.84	0.0	0.2	Pass
Initial Analyzer Response	Mid-Range High-Range	10.13 19.41	9.84 19.39	0.3	1.5 0.1	Pass Pass
	гида-капде	17,41	19.39	0.0	U.1	rass
	Zero	0.00	-0.04	0.0	0.2	Pass
Analyzer Response	Mid-Range	10.13	9.80	0.3	1.7	Pass
, ser reepone	High-Range	19.41	19.43	0.0	0.1	Pass
	-					*****

A=COM

Analyzer: NOx
Analyzer: CO
Analyzer: SO2
Analyzer:
Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

Run No.	Monitor ID	Analyzer Response (ppm)	Initial Time (military)	Initial Va System Response (ppm)		libration Bias (Pass/Fail)	Final Time (military)	Final Va System Response (ppm)		libration Bias (Pass/Fail)		libration Drift (Pass/Fail)
Run 1 Zero Run 1 Span	NOx NOx	0.0 91.4	940 932	0.0 90.4	0.0 -0.4	Pass Pass	1253 1246	-0.1 90.9	0.0	Pass Pass	0.0 0.2	Pass Pass
Run 1 Zero Run 1 Span	CO	0.0 46.4	940 935	-0.7 45.9	-0.8 -0.5	Pass Pass	1253 1250	0.1 45.7	0.1 -0.8	Pass Pass	0.9	Pass Pass
Run 1 Zero Run 1 Span	SO2 SO2	0.0 44.9	940 935	0.5 45.5	0.6 0.7	Pass Pass	1253 1250	1.1 45.6	1.2 0.8	Pass Pass	0.7 0.1	Pass Pass
Run 1 Zero Run 1 Span												
Run 1 Zero Run 1 Span	O2 O2	0.01 10.05	932 940	0.07 10.07	0.3 0.1	Pass Pass	1246 1253	0.07 10.03	0.3 -0.1	Pass Pass	0.0 -0.2	Pass Pass
Run 1 Zero Run 1 Span	CO2 CO2	0.04 9.84	932 940	0.02 9.56	-0.1 -1.4	Pass Pass	1246 1253	0.02 9.51	-0.1 -1.7	Pass Pass	0.0 -0.3	Pass Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = **5.0**

A=COM

Client: SMMI - Pogo
Location: Delta Junction, AK
Source ID: Incinerator
Run Number: Run I29-1
Date: 09/29/13
Run Time: 1406-1506

Analyzer: CO
Analyzer: SO2
Analyzer: Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

				Initial Va	lues			Final Va	lues			
Run No.	Monitor ID	Analyzer Response (ppm)	Initial Time (military)	System Response (ppm)	(%)	libration Bias (Pass/Fail)	Final Time (military)	System Response (ppm)	(%)	libration Bias (Pass/Fail)		libration Drift (Pass/Fail)
Run 2 Zero Run 2 Span	NOx NOx	0.0 91.4	1253 1246	-0.1 90.9	0.0 -0.2	Pass Pass	1600 1554	0.0 91.0	0.0 -0.2	Pass Pass	0.0	Pass Pass
Run 2 Zero Run 2 Span	CO	0.0 46.4	1253 1250	0.1 45.7	0.1 -0.8	Pass Pass	1600 1557	-2.2 44.6	-2.4 -2.0	Pass Pass	-2.5 -1.2	Pass Pass
Run 2 Zero Run 2 Span	SO2 SO2	0.0 44.9	1253 1250	1.1 45.6	1.2 0.8	Pass Pass	1600 1557	0.7 44.5	0.8 -0.4	Pass Pass	-0.4 -1.2	Pass Pass
Run 2 Zero Run 2 Span												
Run 2 Zero Run 2 Span	O2 O2	0.01 10.05	1246 1253	0.07 10.03	0.3 -0.1	Pass Pass	1554 1600	0.06 10.03	0.3 -0.1	Pass Pass	-0.1 0.0	Pass Pass
Run 2 Zero Run 2 Span	CO2 CO2	0.04 9.84	1246 1253	0.02 9.51	-0.1 -1.7	Pass Pass	1554 1600	0.02 9.49	-0.1 -1.8	Pass Pass	0.0 -0.1	Pass Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = 5.0

A=COM

Analyzer: CO
Analyzer: SO2
Analyzer: Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

			Initial Values					Final Va				
Run	Monitor	Analyzer	Initial	System	Ca	libration	Final	System	Ca	libration	Ca	libration
No.	ID	Response	Time	Response		Bias	Time	Response		Bias		Drift
		(ppm)	(military)	(ppm)	(%)	(Pass/Fail)	(military)	(ppm)	(%)	(Pass/Fail)	(%)	(Pass/Fail)
Run 3 Zero	NOx	0.0	1600	0	0.0	Pass	1940	0.0	0.0	Pass	0.0	Pass
Run 3 Span	NOx	91.4	1554	91	-0.2	Pass	1933	90.5	-0.4	Pass	-0.2	Pass
Run 3 Zero	СО	0.0	1602	0	0.0	Pass	1940	0.1	0.1	Pass	Λ1	Pass
Run 3 Zero Run 3 Span	co	0.0 46.4	1557	44.6	0.0 -2.0	Pass Pass	1936	44.9	-1.6	Pass Pass	0.1 0.3	Pass Pass
D 2.77	502	0.0	1600	0.7	0.0	D	1040	0.4	0.4	Pass	1.2	D
Run 3 Zero Run 3 Span	SO2 SO2	0.0 44.9	1600 1557	0.7 44.5	0.8 -0.4	Pass Pass	1940 1936	-0.4 46.8	-0.4 2.1	Pass Pass	-1.2 2.6	Pass Pass
Run 3 Zero												
Run 3 Span												
Run 3 Zero	02	0.01	1554	0.06	0.3	Pass	1933	0.06	0.3	Pass	0.0	Pass
Run 3 Span	O2	10.05	1600	10.03	-0.1	Pass	1940	10.02	-0.2	Pass	-0.1	Pass
Run 3 Zero	CO2	0.04	1554	0.02	-0.1	Pass	1933	0.00	-0.2	Pass	-0.1	Pass
Run 3 Span	CO2	9.84	1600	9.49	-1.8	Pass	1940	9.48	-1.9	Pass	-0.1	Pass
	ļ											

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = 5.0 % Allowable = 3.0

Analyzer Calibration

A=COM

Client SMMI - Pogo
Location Delta Junction, AK
Source ID Incinerator
Operator J Rosburg
Date 09/30/13
Initial Cal Time 0804-0821
Final Cal Time 1728-1744

Cylinder #, Supplier, & Conc.
cc237902 NOx 46.31 CO 45.39 SO2 44.95
cc20720 NOx 92.01 CO 91.66 SO2 90.1
xc0094123 NOx 236.5 CO 230.3 SO2 234.9
cc37929 O2 19.98 CO2 19.41
cc255539 O2 10.01 CO2 10.13

NOx Analyzer Full Scale 236.5 Analyzer CO Full Scale 91.7 Analyzer Full Scale SO2 Analyzer Full Scale 90.1 Analyzer 02 Full Scale 19.98 CO2 Analyzer Full Scale 19.41

COATT	
Model	TEI 42C
Serial #	
Model	TEI 48C
Serial #	
Model	
Serial #	
Model	AMETEK 921
Serial #	
Model	Sevomex1440
Serial #	
Model	Sevomex1440
Serial #	

		Cylinder Value	Analyzer Response	Absolute Difference		cent rence
		(ppm/%)	(ppm/%)	(ppm/%)	(% of span)	(Pass/Fail)
Analyzer NOx	Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	92.0	91.5	0.5	0.2	Pass
Ilitiai Aliaiyzei Kespolise	High-Range	236.5	236.9	0.4	0.2	Pass
	Ingii Ruinge	250.5	20017	0.4	0.2	1 433
	Zero	0.0	0.0	0.0	0.0	Pass
Analyzer Response	Mid-Range	92.0	90.4	1.6	0.7	Pass
	High-Range	236.5	235.5	1.0	0.4	Pass
	_					
Analyzer CO	Zero	0.0	0.1	0.1	0.1	Pass
Initial Analyzer Response	Mid-Range	45.4	46.4	1.0	1.1	Pass
	High-Range	91.7	92.2	0.5	0.6	Pass
	Zero	0.0	-0.9	0.9	1.0	Pass
Analyzer Response	Mid-Range	45.4	46.7	1.3	1.4	Pass
Timiyaci itespoiase	High-Range	91.7	91.9	0.2	0.3	Pass
Analyzer SO2	Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	45.0	44.8	0.2	0.2	Pass
	High-Range	90.1	90.6	0.5	0.6	Pass
	7	0.0	0.6	0.6	0.7	n
A D	Zero	0.0	0.6	0.6	0.7	Pass
Analyzer Response	Mid-Range High-Range	45.0 90.1	46.3 91.9	1.3	1.5 2.0	Pass Pass
Analyzer	Predicted Zero					
Initial Analyzer Response	Mid-Range Mid-Range					
* Cal. through CEM system	High-Range					
	Predicted Zero					
Analyzer Response	Mid-Range					
	Mid-Range					
* Cal. through CEM system	High-Range					
Analyzer O2	Zero	0.00	0.01	0.0	0.1	Pass
Initial Analyzer Response	Mid-Range	10.01	10.09	0.0	0.1	Pass
Initial Analyzer Response	High-Range	19.98	20.20	0.2	1.1	Pass
	Zero	0.00				
Analyzer Response	Mid-Range	10.01	10.08	0.1	0.4	Pass
	High-Range	19.98	20.12	0.1	0.7	Pass
Analyzer CO2	Zero	0.00	0.02	0.0	0.1	Pass
Initial Analyzer Response	Mid-Range	10.13	9.79	0.3	1.8	Pass
	High-Range	19.41	19.48	0.1	0.4	Pass
	Zero	0.00				
Analyzer Response	Mid-Range	10.13	9.78	0.4	1.8	Pass
	High-Range	19.41	19.72	0.3	1.6	Pass

A=COM

Analyzer: CO
Analyzer: SO2
Analyzer: Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

				Initial Va				Final Va				
Run	Monitor	Analyzer	Initial	System	Ca	libration	Final	System	Ca	libration	Ca	libration
No.	ID	Response	Time	Response		Bias	Time	Response		Bias		Drift
		(ppm)	(military)	(ppm)	(%)	(Pass/Fail)	(military)	(ppm)	(%)	(Pass/Fail)	(%)	(Pass/Fail)
Run 1 Zero	NOx	0.0	912	0.0	0.0	Pass	1133	0.0	0.0	Pass	0.0	Pass
Run 1 Span	NOx	91.5	918	89.5	-0.8	Pass	1137	88.5	-1.3	Pass	-0.4	Pass
D 4.7		0.1	010		0.0		1122					
Run 1 Zero	CO	0.1	912	0.8	0.8	Pass	1133	-0.5	-0.7	Pass	-1.4	Pass
Run 1 Span	CO	46.4	920	46.1	-0.3	Pass	1140	46.4	0.0	Pass	0.3	Pass
Run 1 Zero	SO2	0.0	912	0.0	0.0	Pass	1133	1.1	1.2	Pass	1.2	Pass
Run 1 Span	SO2	44.8	920	46.7	2.1	Pass	1140	46.9	2.3	Pass	0.2	Pass
Run 1 Zero												
Run 1 Span												
Run 1 Zero	02	0.01	918	0.07	0.3	Pass	1140	0.06	0.3	Pass	-0.1	Pass
Run 1 Zero Run 1 Span	02	10.09	918 912	10.05	-0.2	Pass Pass	1133	10.03	-0.3	Pass Pass	-0.1 -0.1	Pass
Kun 1 Span	02	10.07	712	10.03	-0.2	1 455	1133	10.03	-0.3	1 455	-0.1	1 455
Run 1 Zero	CO2	0.02	918	0.04	0.1	Pass	1140	0.03	0.1	Pass	-0.1	Pass
Run 1 Span	CO2	9.79	912	9.82	0.2	Pass	1133	9.81	0.1	Pass	-0.1	Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = **5.0**

A=COM

Analyzer: CO
Analyzer: SO2
Analyzer: Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

Run No.	Monitor ID	Analyzer Response (ppm)	Initial Time (military)	Initial Va System Response (ppm)		libration Bias (Pass/Fail)	Final Time (military)	Final Va System Response (ppm)		libration Bias (Pass/Fail)		libration Drift (Pass/Fail)
Run 2 Zero Run 2 Span	NOx NOx	0.0 91.5	1133 1137	0 88.5	0.0	Pass Pass	1423 1416	0.0 87.9	0.0 -1.5	Pass Pass	0.0	Pass Pass
Run 2 Zero	CO	0.1	1133	-0.5	-0.7	Pass	1423	0.0	-0.1	Pass	0.5	Pass
Run 2 Span		46.4	1140	46.4	0.0	Pass	1420	46.8	0.4	Pass	0.4	Pass
Run 2 Zero	SO2	0.0	1133	1.1	1.2	Pass	1423	1.4	1.6	Pass	0.3	Pass
Run 2 Span	SO2	44.8	1140	46.9	2.3	Pass	1420	46.5	1.9	Pass	-0.4	Pass
Run 2 Zero Run 2 Span												
Run 2 Zero	O2	0.01	1140	0.06	0.3 -0.3	Pass	1416	0.04	0.2	Pass	-0.1	Pass
Run 2 Span	O2	10.09	1133	10.03		Pass	1423	10.01	-0.4	Pass	-0.1	Pass
Run 2 Zero	CO2	0.02	1140	0.03	0.1	Pass	1416	0.02	0.0	Pass	-0.1	Pass
Run 2 Span	CO2	9.79	1133	9.81	0.1	Pass	1423	9.82	0.2	Pass	0.1	Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = **5.0**

A=COM

Analyzer: CO
Analyzer: SO2
Analyzer: Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

				Initial Va				Final Va				
-	Monitor	Analyzer	Initial	System	Ca	libration	Final	System	Ca	libration	Ca	libration
No.	ID	Response	Time	Response		Bias	Time	Response		Bias		Drift
		(ppm)	(military)	(ppm)	(%)	(Pass/Fail)	(military)	(ppm)	(%)	(Pass/Fail)	(%)	(Pass/Fail)
Run 3 Zero	NOx	0.0	1423	0	0.0	Pass	1719	0.0	0.0	Pass	0.0	Pass
Run 3 Span	NOx	91.5	1416	87.9	-1.5	Pass	1723	88.9	-1.1	Pass	0.4	Pass
Dun 2 Zono	CO	0.1	1422	0	0.1	Dogg	1710	0.1	0.0	Pass	Λ1	Dogg
Run 3 Zero Run 3 Span	co	0.1 46.4	1423 1420	46.8	-0.1 0.4	Pass Pass	1719 1727	0.1 46.7	0.0 0.3	Pass Pass	0.1 -0.1	Pass Pass
Run 3 Zero	SO2	0.0	1423	1.4	1.6	Pass	1719	1.1	1.2	Pass	-0.3	Pass
Run 3 Span	SO2	44.8	1420	46.5	1.9	Pass	1727	46.4	1.8	Pass	-0.1	Pass
Run 3 Zero												
Run 3 Span												
Run 3 Zero	02	0.01	1416	0.04	0.2	Pass	1723	0.06	0.3	Pass	0.1	Pass
Run 3 Span	02	10.09	1423	10.01	-0.4	Pass	1719	10.04	-0.3	Pass	0.2	Pass
Run 3 Zero	CO2	0.02	1416	0.02	0.0	Pass	1723	0.04	0.1	Pass	0.1	Pass
Run 3 Span	CO2	9.79	1423	9.82	0.2	Pass	1719	9.85	0.3	Pass	0.2	Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = **5.0**

Analyzer Calibration

AECOM

Client SMMI - Pogo
Location Delta Junction, AK
Source ID Incinerator
Operator J Rosburg
Date 10/01/13
Initial Cal Time 0809-0828
Final Cal Time 1642-1652

Cylinder #, Supplier, & Conc.
cc237902 NOx 46.31 CO 45.39 SO2 44.95
cc20720 NOx 92.01 CO 91.66 SO2 90.1
xc0094123 NOx 236.5 CO 230.3 SO2 234.9
cc37929 O2 19.98 CO2 19.41
cc255539 O2 10.01 CO2 10.13

NO_x Analyzer Full Scale 236.5 Analyzer CO Full Scale 91.7 Analyzer Full Scale SO₂ Analyzer Full Scale 90.1 Analyzer 02 Full Scale 19.98 CO2 Analyzer Full Scale 19.41

			_	1		
		Cylinder Value	Analyzer Response	Absolute Difference	Diffe	cent
		(ppm/%)	(ppm/%)	(ppm/%)	(% of span)	(Pass/Fail)
		0.7		0.7	0.7	_
Analyzer NOx	_ Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range High-Range	92.0 236.5	91.8 238.0	0.2 1.5	0.1	Pass Pass
	Ingn-Kange	230.3	230.0	1.3	0.0	1 455
	Zero	0.0	0.0	0.0	0.0	Pass
Analyzer Response	Mid-Range	92.0	91.4	0.6	0.3	Pass
.,	High-Range	236.5	236.4	0.1	0.0	Pass
Analyzer CO	Zero	0.0	-0.7	0.7	0.8	Pass
Initial Analyzer Response	Mid-Range	45.4	45.0	0.4	0.4	Pass
	High-Range	91.7	90.0	1.7	1.8	Pass
	7	0.0	1.3	1.2	1.2	De
Analyzan Dagnanga	Zero	0.0	-1.2	1.2	1.3	Pass
Analyzer Response	Mid-Range High-Range	45.4 91.7	46.7 92.7	1.3	1.4 1.1	Pass Pass
	mgn-kange_	91.7	74.1	1.0	1,1	1 455
Analyzer SO2	Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	45.0	45.7	0.8	0.8	Pass
	High-Range	90.1	91.2	1.1	1.2	Pass
	Zero	0.0	-0.1	0.1	0.1	Pass
Analyzer Response	Mid-Range	45.0	46.7	1.8	1.9	Pass
	High-Range	90.1	91.9	1.8	2.0	Pass
Analyzer	Predicted Zero					
Initial Analyzer Response	_ Fredicted Zero					
Initial Analyzer Response	Mid-Range					
* Cal. through CEM system	High-Range					
	Predicted Zero					
Analyzer Response	Mid-Range					
* Cal Abassah CEM assatsas	Mid-Range					
* Cal. through CEM system	High-Range					
Analyzer O2	Zero	0.00	-0.02	0.0	0.1	Pass
Initial Analyzer Response	Mid-Range	10.01	10.07	0.1	0.3	Pass
	High-Range	19.98	20.08	0.1	0.5	Pass
	Zero	0.00	-0.02	0.0	0.1	Pass
Analyzer Response	Mid-Range	10.01	10.08	0.1	0.4	Pass
	High-Range	19.98	20.16	0.2	0.9	Pass
Analyzer CO2	Zero	0.00	0.00	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	10.13	9.85	0.3	1.4	Pass
	High-Range	19.41	19.50	0.1	0.5	Pass
	Zero	0.00	0.00	0.0	0.0	Pass
Analyzer Response	Mid-Range	10.13	9.88	0.3	1.3	Pass
	High-Range	19.41	19.67	0.3	1.3	Pass
				<u> </u>	I	

A=COM

Analyzer: NOx
Analyzer: CO
Analyzer: SO2
Analyzer:
Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

				Initial Va	lues			Final Va	lues			
Run No.	Monitor ID	Analyzer Response (ppm)	Initial Time (military)	System Response (ppm)	(%)	libration Bias (Pass/Fail)	Final Time (military)	System Response (ppm)	(%)	libration Bias (Pass/Fail)		libration Drift (Pass/Fail)
Run 1 Zero Run 1 Span	NOx NOx	0.0 91.8	834 838	0.0 90.4	0.0	Pass Pass	1113 1118	-0.1 89.9	0.0	Pass Pass	0.0	Pass Pass
Run 1 Zero	CO	-0.7	834	0.3	1.1	Pass	1113	0.0	0.8	Pass	-0.3	Pass
Run 1 Span		45.0	840	45.9	1.0	Pass	1122	46.1	1.2	Pass	0.2	Pass
Run 1 Zero	SO2	0.0	834	0.0	0.0	Pass	1113	0.8	0.9	Pass	0.9	Pass
Run 1 Span	SO2	45.7	840	45.3		Pass	1122	46.1	0.4	Pass	0.9	Pass
Run 1 Zero Run 1 Span												
Run 1 Zero	O2	-0.02	838	0.04	0.3	Pass	1118	0.04	0.3	Pass	0.0	Pass
Run 1 Span	O2	10.07	834	10.08	0.1	Pass	1113	10.04	-0.2	Pass	-0.2	Pass
Run 1 Zero	CO2	0.00	838	0.04	0.2	Pass	1118	0.00	0.0	Pass	-0.2	Pass
Run 1 Span	CO2	9.85	834	9.77	-0.4	Pass	1113	9.74		Pass	-0.2	Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = **5.0**

A=COM

Analyzer: NOx
Analyzer: CO
Analyzer: SO2
Analyzer:
Analyzer: O2
Analyzer: CO2

Span Value: 91.7
Span Value: 90.1
Span Value: Span Value: 19.98
Span Value: 19.41

Span Value:

236.5

Run No.	Monitor ID	Analyzer Response (ppm)	Initial Time (military)	Initial Va System Response (ppm)		libration Bias (Pass/Fail)	Final Time (military)	Final Va System Response (ppm)		libration Bias (Pass/Fail)		libration Drift (Pass/Fail)
Run 2 Zero Run 2 Span	NOx NOx	0.0 91.8	1113 1118	-0.1 89.9	0.0	Pass Pass	1410 1414	0.0 89.6	0.0	Pass Pass	0.0 -0.1	Pass Pass
Run 2 Zero	CO	-0.7	1113	0	0.8	Pass	1410	0.0	0.8	Pass	0.0	Pass
Run 2 Span	CO	45.0	1122	46.1	1.2	Pass	1417	45.9	1.0	Pass		Pass
Run 2 Zero	SO2	0.0	1113	0.8	0.9	Pass	1410	0.9	1.0	Pass	0.1	Pass
Run 2 Span	SO2	45.7	1122	46.1	0.4	Pass	1417	45.9	0.2	Pass	-0.2	Pass
Run 2 Zero Run 2 Span												
Run 2 Zero	O2	-0.02	1118	0.04	0.3	Pass	1414	0.03	0.3	Pass	-0.1	Pass
Run 2 Span	O2	10.07	1113	10.04	-0.2	Pass	1410	10.03	-0.2	Pass	-0.1	Pass
Run 2 Zero	CO2	0.00	1118	0	0.0	Pass	1414	0.01	0.1	Pass	0.1	Pass
Run 2 Span	CO2	9.85	1113	9.74		Pass	1410	9.74	-0.6	Pass	0.0	Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = 5.0

A=COM

Analyzer: NOx
Analyzer: CO
Analyzer: SO2
Analyzer:
Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

	Monitor ID	Analyzer Response	Initial Values			Final Values							
Run			Initial System		Calibration		Final	System	Ca	Calibration		Calibration	
No.			Time	Response	Bias		Time	Response	Bias		Drift		
		(ppm)	(military)	(ppm)	(%)	(Pass/Fail)	(military)	(ppm)	(%)	(Pass/Fail)	(%)	(Pass/Fail)	
Run 3 Zero	NOx	0.0	1410	0	0.0	Pass	1629	0.0	0.0	Pass	0.0	Pass	
Run 3 Span	NOx	91.8	1414	89.6	-0.9	Pass	1635	88.4	-1.4	Pass	-0.5	Pass	
Run 3 Zero	CO	-0.7	1410	0	0.8	Pass	1629	-1.4	-0.8	Pass	-1.5	Pass	
Run 3 Span	co	45.0	1417	45.9	1.0	Pass	1637	45.1	0.1	Pass	-0.9	Pass	
Run 3 Zero	SO2	0.0	1410	0.9	1.0	Pass	1/20	0.5	0.6	Pass	-0.4	Pass	
Run 3 Zero Run 3 Span	SO2 SO2	0.0 45.7	1410	45.9	1.0 0.2	Pass Pass	1629 1637	0.5 46.4	0.6 0.8	Pass Pass	0.6	Pass	
Run 3 Zero													
Run 3 Span													
Run 3 Zero	02	-0.02	1414	0.03	0.3	Pass	1635	0.12	0.7	Pass	0.5	Pass	
Run 3 Span	02	10.07	1410	10.03	-0.2	Pass	1631	10.06	-0.1	Pass	0.2	Pass	
Run 3 Zero	CO2	0.00	1414	0.01	0.1	Pass	1635	0.12	0.6	Pass	0.6	Pass	
Run 3 Span	CO2	9.85	1410	9.74	-0.6	Pass	1631	9.80	-0.3	Pass	0.3	Pass	

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = **5.0**

Analyzer Calibration

A=COM

Client	SMMI - Pogo
Location	Delta Junction, AK
Source ID	Incinerator
Operator	J Rosburg
Date	10/02/13
Initial Cal Time	0814-0828
Final Cal Time	

Cylinder #, Suppl	lier, & Conc.
cc237902 NOx 46	5.31 CO 45.39 SO2 44.95
cc20720 NOx 92.0	01 CO 91.66 SO2 90.1
xc0094123 NOx 2	36.5 CO 230.3 SO2 234.9
cc37929 O2 19.98	CO2 19.41
cc255539	O2 10.01 CO2 10.13

Analyzer	NOx
Full Scale	236.5
Analyzer	CO
Full Scale	91.7
Analyzer	
Full Scale	
Analyzer	SO2
Full Scale	90.1
Analyzer	O2
Full Scale	19.98
Analyzer	CO2
Full Scale	19.41
	<u> </u>

Model	TEI 42C
Serial #	
Model	TEI 48C
Serial #	
Model	
Serial #	
Model	AMETEK 921
Serial #	
Model	Sevomex1440
Serial #	
Model	Sevomex1440
Serial #	

			Full Scale	19.41	_ Serial #	
		Cylinder Value	Analyzer Response	Absolute Difference	Percent Difference	
		(ppm/%)	(ppm/%)	(ppm/%)	(% of span)	(Pass/Fail)
		0.0	0.0	0.0	0.0	
Analyzer NOx	Zero	0.0	0.0	0.0	0.0	Pass
Initial Analyzer Response	Mid-Range	92.0	91.4	0.6	0.3	Pass
	High-Range	236.5	236.9	0.4	0.2	Pass
	Zero	0.0				
Analyzer Response	Mid-Range	92.0				
ining not recoposite	High-Range	236.5				
Analyzer CO	Zero	0.0	0.2	0.2	0.2	Pass
Initial Analyzer Response	Mid-Range	45.4	46.6	1.2	1.3	Pass
	High-Range	91.7	92.3	0.6	0.7	Pass
	7	0.0				
Analyzar Dognamaa	Zero Mid Panga	0.0	+		 	
Analyzer Response	Mid-Range	45.4 91.7		-	 	
	High-Range_	91.7				
Analyzer SO2	Zero	0.0	0.2	0.2	0.2	Pass
Initial Analyzer Response	Mid-Range	45.0	45.1	0.1	0.2	Pass
	High-Range	90.1	90.2	0.1	0.1	Pass
	7	0.0				
4 . 1 D	Zero	0.0				
Analyzer Response	Mid-Range High-Range	45.0 90.1				
Analyzer	Predicted Zero					
Initial Analyzer Response	Mid-Range					
	Mid-Range					
* Cal. through CEM system	High-Range					
	Predicted Zero					
Analyzer Response	Mid-Range					
· Image itempoles	Mid-Range					
* Cal. through CEM system	High-Range					
Analyzer O2	Zero	0.00	0.01	0.0	0.1	Pass
Initial Analyzer Response	Mid-Range High-Range	10.01 19.98	10.16 20.36	0.2 0.4	0.8 1.9	Pass Pass
	Zero	0.00	-0.03	0.0	0.2	Pass
Analyzer Response	Mid-Range	10.01	10.39	0.4	1.9	Pass
	High-Range_	19.98	20.01	0.0	0.2	Pass
Analyzer CO2	Zero	0.00	0.03	0.0	0.2	Pass
Initial Analyzer Response	Mid-Range	10.13	9.85	0.3	1.4	Pass
- · ·	High-Range	19.41	19.60	0.2	1.0	Pass
		0.00	0.00	6.1	0.4	D.
4 . 1 D	Zero	0.00	-0.08	0.1	0.4	Pass
Analyzer Response	Mid-Range High-Range	10.13 19.41	9.98 19.49	0.2	0.8	Pass
	HIGH-KANGE	19.41	1 17.47	0.1	0.4	Pass

Analyzer Bias

AECOM

Analyzer: CO
Analyzer: SO2
Analyzer: Analyzer: O2
Analyzer: CO2

 Span Value:
 236.5

 Span Value:
 91.7

 Span Value:
 90.1

 Span Value:
 19.98

 Span Value:
 19.41

Run No.	Monitor ID	Analyzer Response (ppm)	Initial Time (military)	Initial Va System Response (ppm)		libration Bias (Pass/Fail)	Final Time (military)	Final Va System Response (ppm)		libration Bias (Pass/Fail)		libration Drift (Pass/Fail)
Run 1 Zero Run 1 Span	NOx NOx	0.0 91.4	838 841	0.4 89.9	0.2	Pass Pass	838 841	0.4 89.9	0.2	Pass Pass	0.0 0.0	Pass Pass
Run 1 Zero Run 1 Span	CO	0.2 46.6	838 843	0.0 46.2	-0.2 -0.4	Pass Pass	838 843	0.0 46.2	-0.2 -0.4	Pass Pass	0.0	Pass Pass
Run 1 Zero Run 1 Span	SO2 SO2	0.2 45.1	838 843	0.0 46.3	-0.2 1.3	Pass Pass	838 843	0.0 46.3	-0.2 1.3	Pass Pass	0.0 0.0	Pass Pass
Run 1 Zero Run 1 Span												
Run 1 Zero Run 1 Span	O2 O2	0.01 10.16	841 838	0.04 10.15	0.2 -0.1	Pass Pass	841 838	0.04 10.15	0.2 -0.1	Pass Pass	0.0 0.0	Pass Pass
Run 1 Zero Run 1 Span	CO2 CO2	0.03 9.85	841 838	0.05 9.85	0.1 0.0	Pass Pass	841 838	0.05 9.85	0.1 0.0	Pass Pass	0.0 0.0	Pass Pass

System Cal Bias % = (System Cal Response - Analyzer Response) / CS X 100 Calibration Drift = (Final System Response - Initial System Response) / CS X 100

% Allowable = 5.0

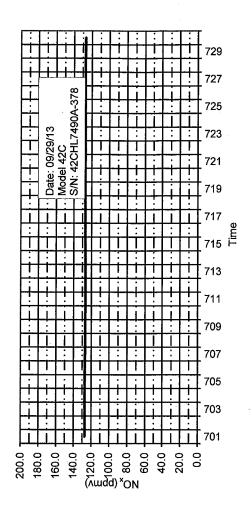
% Allowable = 3.0

NO_x Converter Efficiency Check

Date: Model : S/N : Plant: SMMI - Pogo Mine Source: Incinerator Parameter: NOx

09/29/13 42CHL 42CHL74490A-378

		Start of Run												
ጟ	Š.	_	7	က	4	5	9	7	∞	တ	19	7	12	<u>5</u>
Deviation	(%)	0.2%	0.2%	0.2%	%0.0	0.2%	0.4%	0.5%	0.5%	0.5%	%9.0	%9.0	%9.0	%9.0
Ň	(bbmv)	127.2	127.2	127.2	127.4	127.2	126.9	126.8	126.8	126.7	126.6	126.6	126.6	126.6
Time		701	702	703	704	202	206	707	708	209	710	711	712	713
Julian Day		272	272	272	272	272	272	272	272	272	272	272	272	272



0.6% 127.4 Peak Value

End of Run

0.6% 0.03% 0.03% 0.03% 0.03% 0.03% 0.03% 0.03% 0.03% 0.03% 0.03% 0.04% 0.05% 0

126.9 126.9 127.0 127.0 127.0 127.0 127.0 127.0 127.0 127.3 127.3 127.3 127.3 127.3

NO_x Converter Efficiency Check

10/02/13 42CHL 42CHL74490A-378 Date: Model : S/N : Plant: SMMI - Pogo Mine Source: Incinerator Parameter: NOx

																				•											
		Start of Run																													End of Run
ጟ	ģ	_	7	က	4	2	ဖ	7	∞	တ	10	7	12	73	14	15	16	17	18	19	20	7	22	23	24	25	26	27	28	59	30
Deviation	(%)	1.3%	1.6%	1.7%	1.1%	0.7%	%9:0	0.2%	0.4%	0.1%	0.5%	%9.0	%9.0	0.4%	0.4%	0.4%	0.1%	0.1%	0.1%	%0:0	0.1%	0.1%	0.2%	0.5%	0.2%	0.5%	0.4%	0.2%	0.1%	0.1%	0.1%
Ň	(bbmv)	81.4	81.2	81.1	81.6	81.9	82.0	82.3	82.2	82.4	82.1	82.0	82.0	82.2	82.2	82.2	82.4	82.4	82.4	82.5	82.4	82.4	82.3	82.1	82.3	82.1	82.2	82.3	82.4	82.4	82.4
Time		1307	1308	1309	1310	1311	1312	1313	1314	1315	1316	1317	1318	1319	1320	1321	1322	1323	1324	1325	1326	1327	1328	1329	1330	1331	1332	1333	1334	1335	1336
Julian Day		275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275

1331 (vmqq)_xON 0. 0. 0. 0. 0. 0. 0. 0. 180.0 40.0 20.0 160.0 140.0

> 1.7% 82.5 Peak Value

Response Time Check

AECOM

Plant:	SMMI- Pogo Mine	Date: 09/29/13
Location:	Delta Junction, AK	Check Time: 0740-0810
Source:	Incinerator	Operator: J. Rosburg

Upscale Response Time

Parameter	Run 1	Run 2	Run 3	Average
	(seconds)	(seconds)	(seconds)	(seconds)
NO_x	48	49	46	48
SO ₂	60	64	70	65
CO	48	56	60	55
O_2	34	40	44	39
CO_2	38	44	46	43

Downscale Response Time

Parameter	Run 1	Run 2	Run 3	Average
	(seconds)	(seconds)	(seconds)	(seconds)
NO_x	76	80	82	79
SO ₂	60	64	70	65
CO	72	74	75	74
O_2	26	28	30	28
CO ₂	28	33	35	32



12722 South Wentworth Avenue Chicago, IL 60628

(773) 785-3000 Fax: (773) 785-1928

www.airgas.com

CERTIFICATE OF ANALYSIS Grade of Product: EPA Protocol

Part Number:

E03NI60E15A0286

Reference Number:

54-124389359-1

Cylinder Number:

CC337929

Cylinder Volume: 1

159.6 CF

Laboratory:

ASG - Chicago - IL

Cylinder Pressure:

2015 PSIG

PGVP Number:

B12013

Valve Outlet:

590

Gas Code:

CO2,O2,BALN

Certification Date:

Aug 13, 2013

Expiration Date: Aug 13, 2021

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

		ANALYTICAL 1	RESULTS	•	
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	20.00 %	19.41 %	G1	+/- 1.2% NIST Traceable	08/13/2013
OXYGEN	20.00 %	19.98 %	G1	+/- 0.5% NIST Traceable	08/13/2013
NITROGEN	Balance				

Туре	Lot ID	Cylinder No	CALIBRATION STAT		Uncertainty	Expiration Date
NTRM/CO2	06120405	CC184974	19.66 % CARBON DIOXIDE	NITROGEN	+/- 0.5%	May 01, 2016
NTRM/O2	09061411	CC268005	22.53 % OXYGEN/NITROGE	EN	+/- 0.4%	Mar 08, 2019
			ANALYTICAL EQU		Itipoint Calibration	•
Instrument	Make/Model		Analytical Principle	Lastiviu	itipoliti Calibration	
CO2-1 HORIE	BA VIA-510 V1E3	H7P5	NDIR .	Aug 10, 2	013	
	\ MPA-510 3VU\		Paramagnetic	Aug 01, 2	013	

Triad Data Available Upon

Request

Notes:

Approved for Release



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CERTIFICATE OF ANALYSIS Grade of Product: EPA Protocol

Part Number:

E03NI80E15A0138

Reference Number: 54-124375951-1

Cylinder Number:

CC255539

Cylinder Volume:

150.9 CF

Laboratory:

ASG - Chicago - IL

Cylinder Pressure:

2015 PSIG

PGVP Number:

B12013

Valve Outlet:

590

Gas Code:

CO2, O2, BALN

Certification Date:

May 28, 2013

Expiration Date: May 28, 2021

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

		ANALYTICAL	RESULTS		
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	10.00 %	10.13 %	G1	+/- 1.0% NIST Traceable	05/28/2013
OXYGEN	10.00 %	10.01 %	G1	+/- 1.0% NIST Traceable	05/28/2013
NITROGEN	Balance				

			CALIBRATION STA	NDARDS		· ·
Туре	Lot ID	Cylinder No	Concentration		Uncertainty	Expiration Date
NTRM/CO2	06120405	CC184974	19.66 % CARBON DIOXIDE	/NITROGEN	+/- 0.5%	May 01, 2016
NTRM/O2	06120211	CC195925	20.90 % OXYGEN/NITROGI	ΕN	+/- 0.4%	Dec 01, 2015
			ANALYTICAL EQU	IPMENT		
Instrument/	Make/Model	•	Analytical Principle	Last Mu	Itipoint Calibratio	n ·
CO2-1 HORIE	3A VIA-510 V1E3	BH7P5	NDIR	May 20, 2	013	· · · · · · · · · · · · · · · · · · ·
O2-1 HORIBA	MPA-510 3VUY	L9NR	Paramagnetic	May 15, 2	013	

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CERTIFICATE OF ANALYSIS Grade of Product: EPA Protocol

Part Number:

E04NI99E15A0PK6

XC009412B&

Cylinder Volume:

Reference Number: 54-124389362-1

Cylinder Number:

144.4 CF

Laboratory:

ASG - Chicago - IL

Cylinder Pressure:

2015 PSIG

PGVP Number:

B12013

Valve Outlet:

660

Gas Code:

CO,NO,NOX,SO2,BALN

Certification Date:

Aug 22, 2013

Expiration Date: Aug 22, 2021

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

		ANALYTICAL	RESULTS		
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
NOX	230.0 PPM	236.5 PPM	G1	+/- 0.8% NIST Traceable	08/15/2013, 08/22/2013
CARBON MONOXIDE	230.0 PPM	230.3 PPM	G1	+/- 1.1% NIST Traceable	08/15/2013
NITRIC OXIDE	230.0 PPM	236.5 PPM .	G1	+/- 0.8% NIST Traceable	08/15/2013, 08/22/2013
SULFUR DIOXIDE	230.0 PPM	234.9 PPM	G1	+/- 1.0% NIST Traceable	08/15/2013, 08/22/2013
NITROGEN	Balance				

		C	ALIBRATION STAI	NDARDS		
Туре	Lot ID	Cylinder No	Concentration		Uncertainty	Expiration Date
CO	12062424	CC366872	487.1 PPM CARBON MON	IOXIDE/NITROGEN	+/- 0.6%	Jun 22, 2018
NO	12061957	CC367731	250.8 PPM NITRIC OXIDE	NITROGEN	+/- 0.5%	May 14, 2018
NO2	124206889130	CC323209	4.824 PPM NITROGEN DI	OXIDE/NITROGEN	+/- 2.0%	Oct 25, 2015
NTRM/SO2	11060839	CC341872	241.0 PPM SULFUR DIOX	IDE/NITROGEN	+/- 0.9%	May 13, 2017
		A	NALYTICAL EQUI	PMENT		
Instrument	/Make/Model	*	Analytical Principle	Last Multipoin	t Calibration	,
Nexus 470 Al	EP0000428		FTIR	Jul 21, 2013		
Nexus 470 Al	EP0000428		FTIR	Aug 21, 2013		
Nexus 470 At	EP0000428		FTIR	Aug 21, 2013		
Nexus 470 Al	EP0000428		FTIR	Aug 21, 2013		

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Page 1 of 54-124389362-1



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CERTIFICATE OF ANALYSIS Grade of Product: EPA Protocol

Part Number:

E04NI99E15A0443

Reference Number: 54-124389361-1

Cylinder Number:

CC20720

Cylinder Volume:

144.4 CF

Laboratory:

ASG - Chicago - IL

Cylinder Pressure:

2015 PSIG

PGVP Number:

B12013

Valve Outlet:

660

Gas Code:

CO,NO,SO2,BALN

Certification Date:

Aug 23, 2013

Expiration Date: Aug 23, 2021

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

AND THE RESERVE OF THE PARTY OF		ANALYTICAL	RESULTS		
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
NOX	90.00 PPM	92.01 PPM	G1	+/- 1.0% NIST Traceable	08/16/2013, 08/23/2013
CARBON MONOXIDE	90.00 PPM	91.66 PPM	G1	+/- 1.0% NIST Traceable	08/16/2013
NITRIC OXIDE	90.00 PPM	92.01 PPM	G1	+/- 1.0% NIST Traceable	08/16/2013, 08/23/2013
SULFUR DIOXIDE	90.00 PPM	90.10 PPM	G1	+/- 1.0% NIST Traceable	08/16/2013, 08/23/2013
NITROGEN	Balance				

		C	ALIBRATION STAI	NDARDS	,
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
СО	12062234	CC365729	97.56 PPM CARBON MON	NOXIDE/NITROGEN+/- 0.6%	May 25, 2018
NTRM/NO	11060516	CC331275	101.2 PPM NITRIC OXIDE	/NITROGEN +/- 0.6%	Feb 16, 2017
NO2	124206889130	CC323209	4.824 PPM NITROGEN DI	OXIDE/NITROGEN +/- 2.0%	Oct 25, 2015
NTRM/SO2	11060839	CC341872	241.0 PPM SULFUR DIOX	(IDE/NITROGEN +/- 0.9%	May 13, 2017
		A	NALYTICAL EQUI	PMENT	
Instrument/	Make/Model		Analytical Principle	Last Multipoint Calibration	
Nexus 470 AE	EP0000428	 	FTIR	Jul 21, 2013	
Nexus 470 AE	EP0000428		FTIR	Aug 21, 2013	
Nexus 470 AE	EP0000428		FTIR	Aug 21, 2013	
Nexus 470 AB	EP0000428		FTIR	Aug 21, 2013	

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Page 1 of 54-124389361-1



12722 South Wentworth Avenue Chicago, IL 60628 (773) 785-3000 Fax: (773) 785-1928 www.airgas.com

CERTIFICATE OF ANALYSIS **Grade of Product: EPA Protocol**

Part Number:

E04NI99E15A7377

Reference Number: 54-124389373-1

Cylinder Number:

CC237902

Cylinder Volume:

144.4 CF

Laboratory:

ASG - Chicago - IL

Cylinder Pressure:

2015 PSIG

PGVP Number:

B12013

Valve Outlet:

660

Gas Code:

CO,NO,SO2,BALN

Certification Date:

Aug 23, 2013

Expiration Date: Aug 23, 2016

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

		ANALYTICAL	RESULTS		
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
NOX	45.00 PPM	46.31 PPM	G1	+/- 1.4% NIST Traceable	08/16/2013, 08/23/2013
CARBON MONOXIDE	45.00 PPM	45.39 PPM	G1	+/- 1.0% NIST Traceable	08/16/2013
NITRIC OXIDE	45.00 PPM	46.31 PPM	G1	+/- 1.4% NIST Traceable	08/16/2013, 08/23/2013
SULFUR DIOXIDE	45.00 PPM	44.95 PPM	G1	+/- 1.0% NIST Traceable	08/16/2013, 08/23/2013
NITROGEN	Balance				

			CALIBRATION ST	ANDARDS		
Type	Lot ID	Cylinder No	Concentration		Uncertainty	Expiration Date
со	12060505	CC353897	49.53 PPM CARBON MON	OXIDE/NITROGEN	+/- 0.6%	Dec 20, 2017
NTRM	10061122	CC283641	49.95 PPM NITRIC OXIDE	NITROGEN	+/- 0.8%	Dec 16, 2017
NO	10061122	CC283848	49.73 PPM NITRIC OXIDE	NITROGEN	+/- 1.0%	Jul 23, 2016
NO2	124206889130	CC323209	4.824 PPM NITROGEN DIG	OXIDE/NITROGEN	+/- 2.0%	Oct 25, 2015
NTRM	110602	CC280998	49.67 PPM SULFUR DIOX	IDE/NITROGEN	1.2%	May 13, 2017
			ANALYTICAL EQ	UIPMENT		
Instrum	ent/Make/Model		Analytical Principle	Last Multipoi	nt Calibration	
Nexus 47	70 AEP0000428		FTIR	Jul 21, 2013		
Nexus 47	70 AEP0000428		FTIR	Aug 21, 2013		
Nexus 47	70 AEP0000428	•	FTIR	Aug 21, 2013		
	70 AEP0000428		FTIR	Aug 21, 2013		

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Page 1 of 54-124389373-1

AECOM Environment

Appendix D

Process Information

Date	Run#	Run Time Start / End	Start Time Charge	Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min	Secondary Temp °F Plus 5 Min	Primary Temp °F Plus 10 Min	Secondary Temp °F Plus 10 Min	Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry lbs	Type III Waste Wet Ibs	Sludge lbs	Oily Rags lbs
	15-1	11:06	11:06			1440	1842	1566	1835	1416	1827	11:21	1405	1814	37			
9/29/2013	15-1		11:22	1381	1835	1475	1832	1494	1816	1488	1836	11:37	1487	1819			27	15
9/29/2013	I5-1		11:38	1485	1837	1543	1831	1431	1825	1457	1817	11:53	1467	1835	20	30		
9/29/2013	15-1		11:54	1482	1827	1428	1835	1475	1826	1403	1822	12:10	1386	1815			33	20
9/29/2013	15-1		12:11	1421	1815	1551	1819	1446	1817	1453	1834	12:26	1468	1818	27	20		
9/29/2013	15-1	12:42	12:27	1480	1836	1515	1838	1596	1838	1512	1838	12:42	1505	1818			30	32
DATE OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OF THE OWNER OWNER OF THE OWNER OWNER.	NANEX (841/04 20-00)	Salara Salarana ali versi emingra	POSTEROTO AND AND AND	terio con esta a l'esta l'activa antiqua mana		E CONTRACTOR OF THE PROPERTY O	William water a constraint a series					Total lbs	trash burne	d for run	84	50	90	67
9/29/2013	129-1	14:06	14:06	1482	1834	1539	1833	1606	1830	1551	1822	14:21	1549	1838	15	28		
9/29/2013	129-1		14:22	1533	1834	1590	1827	1625	1819	1574	1817	14:34	1571	1823			29	16
9/29/2013	129-1		14:38	1542	1833	1590	1826	1516	1817	1453	1816	14:53	1447	1837	19		34	
9/29/2013	129-1		14:53	1435	1834	1508	1832	1542	1819	1484	1819	15:08	1477	1819			30	17
9/29/2013	129-1	15:08	15:09	1468	1816	1520	1833	1483	1824		· ·				10		35	
	THE RESERVE OF THE PROPERTY OF	NAMES OF THE PARTY	Josephonestiggen / Telement Josephonestig / Telement Josephonestig / T	The party for the Party Market and a second contract of the second	and the state of t	A 10 the consists between a construction of the con-						Total lbs	trash burne	d for run	44	28	128	33
			intropering a biological parties															
9/29/2013	123-1	17:21	17:21	1391	1836	1464	1832	1434	1819	1400	1821	17:36	1393	1835	14		28	
9/29/2013	123-1		17:37	1392	1822	1425	1836	1402	1821	1487	1837	17:52	1503	1818	22		29	
9/29/2013	123-1		17:54	1473	1831	1522	1820	1470	1826	1419	1825	18:09	1417	1836	16		28	
9/29/2013	123-1		18:10	1418	1827	1427	1833	1409	1819	1443	1831	18:25	1437	1817			28	14
9/29/2013	123-1		18:26	1419	1824	1423	1835	1480	1836	1418	1817	18:41	1417	1820			29	14
9/29/2013	123-1	ļ	18:42	1412	1838	1474	1821	1480	1821	1472	1837	18:57	1472	1834			28	10
9/29/2013	123-1		18:58	1470	1821	1553	1825	1491	1834	1468	1822	19:13	1467	1836			30	11
9/29/2013	123-1	19:29	19:14	1453	1837	1558	1837	1508	1837	1472	1826	19:29	1471	1828		21		12
	VOICEMON CONTRACTOR CONTRACTOR		HEED AND THE COMPANY OF COM-	100 THE THE THE THE THE THE THE THE THE THE		TO CONTRACT THE PROPERTY AND ADMINISTRATIVE PROPERTY.	MARKA SAN MANANTA SANTA SANTA					Total lbs	trash burne	d for run	52	21	200	61
	30000000																	

Date	Run #	Run Time Start / End	Start Time Charge	Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min	Secondary Temp °F Plus 5 Min	Primary Temp °F Plus 10 Min	Secondary Temp °F Plus 10 Min	Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry (lb)	Type III Waste Wet (lb)	Sludge (lb)	Adsorbs (lb)	Total Charge Wt (lb)
	I5-1	11:06	11:06	_	_	1440	1842	1566	1835	1416	1827	11:21	1405	1814	37				37
9/29/2013	I5-1		11:22	1381	1835	1475	1832	1494	1816	1488	1836	11:37	1487	1819			27	15	42
9/29/2013	I5-1		11:38	1485	1837	1543	1831	1431	1825	1457	1817	11:53	1467	1835	20	30			50
9/29/2013	I5-1		11:54	1482	1827	1428	1835	1475	1826	1403	1822	12:10	1386	1815			33	20	53
9/29/2013	I5-1		12:11	1421	1815	1551	1819	1446	1817	1453	1834	12:26	1468	1818	27	20			47
9/29/2013	I5-1	12:42	12:27	1480	1836	1515	1838	1596	1838	1512	1838	12:42	1505	1818			30	32	62
9/29/2013	129-1	14:06	14:06	1482	1834	1539	1833	1606	1830	1551	1822	14:21	1549	1838	15	28			43
9/29/2013	129-1		14:22	1533	1834	1590	1827	1625	1819	1574	1817	14:34	1571	1823			29	16	45
9/29/2013	129-1		14:38	1542	1833	1590	1826	1516	1817	1453	1816	14:53	1447	1837	19		34		53
9/29/2013	129-1		14:53	1435	1834	1508	1832	1542	1819	1484	1819	15:08	1477	1819			30	17	47
9/29/2013	129-1	15:08	15:09	1468	1816	1520	1833	1483	1824						10		35		45
9/29/2013	123-1	17:21	17:21	1391	1836	1464	1832	1434	1819	1400	1821	17:36	1393	1835	14		28		42
9/29/2013	123-1		17:37	1392	1822	1425	1836	1402	1821	1487	1837	17:52	1503	1818	22		29		51
9/29/2013	123-1		17:54	1473	1831	1522	1820	1470	1826	1419	1825	18:09	1417	1836	16		28		44
9/29/2013	123-1		18:10	1418	1827	1427	1833	1409	1819	1443	1831	18:25	1437	1817			28	14	42
9/29/2013	123-1		18:26	1419	1824	1423	1835	1480	1836	1418	1817	18:41	1417	1820			29	14	43
9/29/2013	123-1		18:42	1412	1838	1474	1821	1480	1821	1472	1837	18:57	1472	1834			28	10	38
9/29/2013	123-1		18:58	1470	1821	1553	1825	1491	1834	1468	1822	19:13	1467	1836			30	11	41
9/29/2013	I23-1	19:29	19:14	1453	1837	1558	1837	1508	1837	1472	1826	19:29	1471	1828		21		12	33
		<u> </u>		l			I							Total Wt =	180	99	418	161	858

											_		
Average Temp =	1452	1830	1502	1831	1498	1825	1465	1826	1463	1826		Average Charge Wt =	45

Primary Chamber

Average Temp of 3 Runs =	1480 F
Minimum Temp of 3 Runs =	1381 F

Secondary Chamber

Average Temp of 3 Runs =	1828 F
Minimum Temp of 3 Runs =	1815 F

Waste Composition

waste con	iposition		
MSW*	Sludge	Adsorbs	Total
279	418	161	858
33%	19%	19%	100%

^{*}MSW = Type II + Type III

Date	Run #	Run Time Start / End	Start Time Charge	Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min	Secondary Temp °F Plus 5 Min	Primary Temp °F Plus 10 Min	Secondary Temp °F Plus 10 Min	Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry Ibs	Type III Waste Wet Ibs	Sludge lbs	Oily Rags Ibs
9/30/2013	123-2	9:23	9:23	989	1770	806	1521	1106	1758	1151	1779	9:38	1152	1781		34		10
9/30/2013	123-2		9:40	1129	1775	1287	1833	1485	1815	1387	1814	9:53	1383	1820	18	27		
9/30/2013	123-2		9:54	1373	1824	1431	1818	1411	1831	1384	1832	10:09	1380	1813		35		18
9/30/2013	123-2		10:10	1362	1818	1412	1829	1363	1825	1337	1819	10:25	1365	1832	29	16		
9/30/2013	123-2		10:26	1334	1832	1490	1820	1445	1827	1447	1825	10:41	1451	1818			30	19
9/30/2013	123-2		10:42	1455	1826	1480	1825	1440	1826	1417	1820	10:57	1415	1825	24	20	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
9/30/2013	123-2		10:58	1412	1819	1476	1826	1483	1824	1479	1875	11:13	1480	1877			28	17
9/30/2013	123-2	11:29	11:14	1477	1819	1528	1818	1494	1826	1440	1834	11:29	1431	1823			30	16
2-32 - V												Total lbs t	rash burned	for run	71	132	88	80
						dalih, List.									Garallo I			
9/30/2013	15-2	12:51	12:51	1470	1823	1582	1828	1578	1826	1517	1825	13:06	1515	1836	20	24		
9/30/2013	15-2		13:07	1507	1825	1577	1830	1501	1832	1445	1819	13:22	1443	1826			28	13
9/30/2013	15-2		13:23	1432	1835	1442	1828	1406	1834	1504	1835	13:38	1505	1827			28	. 16
9/30/2013	15-2		13:39	1405	1822	1522	1834	1455	1820	1405	1819	13:54	1404	1820			29	11
9/30/2013	15-2	14:10	13:55	1395	1835	1538	1826	1504	1822	1472	1819	14:10	1471	1821			29	13
war and section probabilities and	and the section of the section of		A A TO THE TOTAL PROPERTY AND THE PROPERTY AND TH									Total lbs t	rash burned	for run	20	24	114	53
9/30/2013	129-2	15:05	15:05	1423	1822	1514	1820	1456	1830	1408	1824	15:20	1407	1818	13		29	
9/30/2013	129-2		15:21	1400	1825	1546	1821	1535	1836	1523	1820	15:36	1523	1827		29		17
9/30/2013	129-2		15:37	1519	1823	1618	1826	1654	1821	1622	1828	15:52	1620	1831		24		20
9/30/2013	129-2		15:53	1618	1851	1679	1822	1621	1820	1576	1820	16:08	1575	1819	-	36		11
9/30/2013	129-2		16:09	1571	1834	1597	1819	1540	1825	1512	1833	16:24	1512	1824			29	14
9/30/2013	129-2		16:25	1511	1826	1541	1836	1583	1824	1553	1820	16:40	1553	1820		29		14
9/30/2013	129-2		16:41	1551	1838	1477	1834	1469	1836	1440	1833	16:56	1439	1826			28	22
9/30/2013	129-2	17:12	16:57	1433	1821	1576	1822	1631	1826	1684	1830	17:12	1685	1822			30	20
v												Total lbs t	rash burned	for run	13	118	116	118
To the season of the common of		Element of the		- X					en ingeneral service de la companya de la companya de la companya de la companya de la companya de la companya						SALE FAILS			

Date	Run #	Run Time Start / End	Start Time Charge	Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min	Secondary Temp °F Plus 5 Min	Primary Temp °F Plus 10 Min	Secondary Temp °F Plus 10 Min	Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry (lb)	Type III Waste Wet (lb)	Sludge (lb)	Adsorbs (lb)	Total Charge Wt (lb)
9/30/2013	123-2	9:23	9:23	989	1770	806	1521	1106	1758	1151	1779	9:38	1152	1781		34		10	44
9/30/2013	123-2		9:40	1129	1775	1287	1833	1485	1815	1387	1814	9:53	1383	1820	18	27			45
9/30/2013	123-2		9:54	1373	1824	1431	1818	1411	1831	1384	1832	10:09	1380	1813		35		18	53
9/30/2013	123-2		10:10	1362	1818	1412	1829	1363	1825	1337	1819	10:25	1365	1832	29	16			45
9/30/2013	123-2		10:26	1334	1832	1490	1820	1445	1827	1447	1825	10:41	1451	1818			30	19	49
9/30/2013	123-2		10:42	1455	1826	1480	1825	1440	1826	1417	1820	10:57	1415	1826	24	20			44
9/30/2013	123-2		10:58	1412	1819	1476	1826	1483	1824	1479	1875	11:13	1480	1877			28	17	45
9/30/2013	123-2	11:29	11:14	1477	1819	1528	1818	1494	1826	1440	1834	11:29	1431	1823			30	16	46
9/30/2013	15-2	12:51	12:51	1470	1823	1582	1828	1578	1826	1517	1825	13:06	1515	1836	20	24			44
9/30/2013	15-2		13:07	1507	1825	1577	1830	1501	1832	1445	1819	13:22	1443	1826			28	13	41
9/30/2013	15-2		13:23	1432	1835	1442	1828	1406	1834	1504	1835	13:38	1505	1827			28	16	44
9/30/2013	15-2		13:39	1405	1822	1522	1834	1455	1820	1405	1819	13:54	1404	1820			29	11	40
9/30/2013	15-2	14:10	13:55	1395	1835	1538	1826	1504	1822	1472	1819	14:10	1471	1821			29	13	42
9/30/2013	129-2	15:05	15:05	1423	1822	1514	1820	1456	1830	1408	1824	15:20	1407	1818	13		29		42
9/30/2013	129-2		15:21	1400	1825	1546	1821	1535	1836	1523	1820	15:36	1523	1827		29		17	46
9/30/2013	129-2		15:37	1519	1823	1618	1826	1654	1821	1622	1828	15:52	1620	1831		24		20	44
9/30/2013	129-2		15:53	1618	1851	1679	1822	1621	1820	1576	1820	16:08	1575	1819		36		11	47
9/30/2013	129-2		16:09	1571	1834	1597	1819	1540	1825	1512	1833	16:24	1512	1824			29	14	43
9/30/2013	129-2		16:25	1511	1826	1541	1836	1583	1824	1553	1820	16:40	1553	1820		29		14	43
9/30/2013	129-2		16:41	1551	1838	1477	1834	1469	1836	1440	1833	16:56	1439	1826			28	22	50
9/30/2013	129-2	17:12	16:57	1433	1821	1576	1822	1631	1826	1684	1830	17:12	1685	1822			30	20	50
														Total Wt =	104	274	318	251	947

Primary	Chamber
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Average Temp = 1417

Average Temp of 3 Runs =	1461	F	
Minimum Temp of 3 Runs =	806	F	

Secondary Chamber

,	- Citatina Ci		
	Average Temp of 3 Runs =	1820	F
	Minimum Temp of 3 Rups =	1521	F

Waste Composition

Trabte comp	Tradic Composition											
MSW*	Sludge	Adsorbs	Total									
378	318	251	947									
40%	34%	27%	100%									

Average Charge Wt =

^{*}MSW = Type II + Type III

					•								•					
							* .											
								,										*
Date	Run #	Run Time Start / End	Start Time Charge	Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min		Primary Temp °F Plus 10 Min		Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry Ibs	Type III Waste Wet Ibs	Sludge lbs	Oily Rags lbs
10/1/2013	129-3	8:58	8:58	1085	1817	1184	1819	1183	1816	1169	1818	9:13	1167	1831	23.	38		
10/1/2013	129-3		9:14	1164	1824	1186	1831	1173	1818	1168	1828	9:29	1167	1821	27	19		
10/1/2013	129-3		9:30	1166	1825	1360	1820	1339	1830	1311	1827	9:45	1310	1827	26	17		
10/1/2013	129-3		9:46	1305	1817	1429	1826	1477	1834	1426	1819	10:01	1432	1831	20	26		
10/1/2013	129-3		10:02	1439	1821	1447	1825	1433	1830	1457	1818	10:17	1457	1829		30		10
10/1/2013	129-3		10:18	1454	1833	1452	1821	1433	1820	1476	1819	10:33	1476	1828	16	29		
10/1/2013	129-3	11.05	10:34	1476	1834	1410	1819	1441	1822	1461	1823	10:49	1461	1818			30	14
10/1/2013	129-3	11:05	10:50	1457	1835	1495	1833	1404	1829	1493	1829	11:05	1494	1833	21	24	<u></u>	
			or energy									lotal lbs	trash burned	tor run	133	183	30	24
10/1/2013	123-3	11:58	11:58	1400	1817	1588	1838	1529	1822	1438	1835	12:13	1432	1818	25	31		
10/1/2013	123-3		12:14	1503	1832	1507	1827	1419	1831	1451	1818	12:13	1446	1821	25	37		10
10/1/2013	123-3		12:30	1440	1821	1510	1819	1450	1825	1402	1819	12:45	1397	1824		3,	28	16
10/1/2013	123-3		12:46	1391	1821	1524	1819	1433	1829	1451	1821	13:01	1467	1826	23	27	20	
10/1/2013	123-3		13:02	1484	1830	1460	1821	1403	1821	1456	1830	13:17	1452	1822		48		13
10/1/2013	123-3		13:18	1437	1822	1590	1822	1593	1836	1555	1822	13:33	1548	1828	22	28		
10/1/2013	123-3		13:34	1531	1825	1658	1837	1633	1836	1587	1824	13:49	1581	1837		33		16
10/1/2013	123-3	14:05	13:50	1574	1821	1679	1843	1736	1830	1782	1833	14:05	1783	1836			28	25
												Total lbs	trash burned	for run	70	204	56	80
								Established.										
10/1/2013	15-3	15:05	15:05	1458	1834	1556	1837	1508	1821	1450	1825	15:20	1430	1842	21	19		
10/1/2013	15-3		15:22	1433	1819	1539	1833	1478	1823	1430	1828	15:37	1429	1835	10	33		
10/1/2013	15-3		15:38	1419	1821	1469	1819	1406	1832	1481	1831	15:53	1485	1835	17	30		
10/1/2013	15-3		15:54	1501	1829	1563	1837	1475	1823	1424	1819	16:09	1422	1824	24	19		
10/1/2013	15-3	16:25	16:10	1413	1828	1561	1820	1537	1824	1500	1835	16:25	1499	1834		-	29	21
						20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Jan 20 Ja	alternation of the state of the state of		annorman constrain			Total lbs	trash burned	for run	72	101	29	21
							<u> </u>											

Date	Run #	Run Time Start / End	Start Time Charge	Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min	Secondary Temp °F Plus 5 Min	Primary Temp °F Plus 10 Min	Secondary Temp °F Plus 10 Min	Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry (lb)	Type III Waste Wet (lb)	Sludge (lb)	Adsorbs (lb)	Total Charge Wt (lb)
10/1/2013	129-3	8:58	8:58	1085	1817	1184	1819	1183	1816	1169	1818	9:13	1167	1831	23	38			61
10/1/2013	129-3		9:14	1164	1824	1186	1831	1173	1818	1168	1828	9:29	1167	1821	27	19			46
10/1/2013	129-3		9:30	1166	1825	1360	1820	1339	1830	1311	1827	9:45	1310	1827	26	17			43
10/1/2013	129-3		9:46	1305	1817	1429	1826	1477	1834	1426	1819	10:01	1432	1831	20	26			46
10/1/2013	129-3		10:02	1439	1821	1447	1825	1433	1830	1457	1818	10:17	1457	1829		30		10	40
10/1/2013	129-3		10:18	1454	1833	1452	1821	1433	1820	1476	1819	10:33	1476	1828	16	29			45
10/1/2013	129-3		10:34	1476	1834	1410	1819	1441	1822	1461	1823	10:49	1461	1818			30	14	44
10/1/2013	129-3	11:05	10:50	1457	1835	1495	1833	1404	1829	1493	1829	11:05	1494	1833	21	24			45
10/1/2013	123-3	11:58	11:58	1400	1817	1588	1838	1529	1822	1438	1835	12:13	1432	1818	25	31			56
10/1/2013	123-3		12:14	1503	1832	1507	1827	1419	1831	1451	1818	12:29	1446	1821		37		10	47
10/1/2013	123-3		12:30	1440	1821	1510	1819	1450	1825	1402	1819	12:45	1397	1824			28	16	44
10/1/2013	123-3		12:46	1391	1821	1524	1819	1433	1829	1451	1821	13:01	1467	1826	23	27			50
10/1/2013	123-3		13:02	1484	1830	1460	1821	1403	1821	1456	1830	13:17	1452	1822		48		13	61
10/1/2013	123-3		13:18	1437	1822	1590	1822	1593	1836	1555	1822	13:33	1548	1828	22	28			50
10/1/2013	123-3		13:34	1531	1825	1658	1837	1633	1836	1587	1824	13:49	1581	1837		33		16	49
10/1/2013	123-3	14:05	13:50	1574	1821	1679	1843	1736	1830	1782	1833	14:05	1783	1836			28	25	53
10/1/2013	15-3	15:05	15:05	1458	1834	1556	1837	1508	1821	1450	1825	15:20	1430	1842	21	19			40
10/1/2013	15-3		15:22	1433	1819	1539	1833	1478	1823	1430	1828	15:37	1429	1835	10	33			43
10/1/2013	15-3		15:38	1419	1821	1469	1819	1406	1832	1481	1831	15:53	1485	1835	17	30			47
10/1/2013	15-3		15:54	1501	1829	1563	1837	1475	1823	1424	1819	16:09	1422	1824	24	19			43
10/1/2013	15-3	16:25	16:10	1413	1828	1561	1820	1537	1824	1500	1835	16:25	1499	1834			29	21	50
														Total Wt =	275	488	115	125	1003

Average Temp =	1406
Primary Ch	ambor

,		
Average Temp of 3 Runs =	1447 F	
Minimum Temp of 3 Rups =	1085 F	

Secondary	Chambe
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Average Temp of 3 Runs =	1826 F	
Minimum Temp of 3 Runs =	1816 F	

Waste Composition

waste composition											
MSW*	Sludge	Adsorbs	Total								
763	115	125	1003								
76%	11%	12%	100%								

Average Charge Wt =

^{*}MSW = Type II + Type III

										·. ·		,						
Date	Run #	Run Time Start / End		Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min	Secondary Temp °F Plus 5 Min	Primary Temp °F Plus 10 Min	Secondary Temp °F Plus 10 Min	Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry Ibs	Type III Waste Wet Ibs	Sludge lbs	Oily Rags lbs
10/2/2013	129-4	8:46	8:46	1028	1810	1300	1842	1347	1814	1236	1829	9:01	1234	1830	37	17		
10/2/2013	129-4		9:02	1219	1816	1399	1814	1350	1828	1323	1821	9:17	1322	1824	23	17		
10/2/2013	129-4		9:18	1312	1819	1335	1816	1305	1826	1279	1822	9:33	1278	1825	10	39		
10/2/2013	129-4		9:34	1272	1816	1449	1833	1392	1825	1345	1823	9:49	1344	1826	22	25		
10/2/2013	129-4		9:50	1335	1822	1502	1834	1408	1832	1448	1827	10:05	1447	1832	24	19		
10/2/2013	129-4		10:06	1445	1833	1528	1833	1384	1830	1462	1818	10:21	1463	1821	29	21		
10/2/2013	129-4		10:22	1466	1827	1461	1821	1418	1820	1468	1832	10:37	1469	1826	42	15		
10/2/2013	129-4	10:53	10:38	1468	1821	1481	1822	1404	1830	1471	1834	10:53	1467	1833	18	27		
	_											Total lbs	trash burr	ed for run	205	180		
								ta in divini		11252001450		action a						
10/2/2013	123-4	11:57	11:57	1446	1822	1448	1820	1426	1818	1479	1819	12:12	1480	1825	25	18		
10/2/2013	123-4		12:13	1480	1823	1496	1818	1399	1822	1466	1825	12:28	1468	1834	26	19		
10/2/2013	123-4		12:29	1471	1820	1450	1819	1414	1818	1439	1824	12:44	1439	1834	32	18		
10/2/2013	123-4		12:45	1438	1820	1502	1828	1446	1831	1405	1827	13:00	1411	1818	12	34		
10/2/2013	123-4		13:01	1444	1837	1584	1835	1519	1819	1456	1836	13:16	1453	1822	12	35		
10/2/2013	123-4		13:17	1444	1827	1550	1835	1482	1821	1434	1830	13:32	1432	1831	27	30		
10/2/2013	123-4		13:33	1424	1829	1535	1820	1483	1820	1436	1820	13:48	1435	1825	11	42	-	
10/2/2013	123-4	14:04	13:49	1427	1826	1405	1820	1469	1834	1421	1831	14:04	1418	1819	21	25		
												Total lbs	trash burn	ed for run	166	221		
10/2/2013	15-4	15:11	15:11	1460	1828	1417	1835	1469	1822	1427	1823	15:26	1424	1818	28	24		
10/2/2013	15-4		15:27	1386	1836	1500	1833	1399	1823	1504	1819	15:42	1502	1824	14	29		
10/2/2013	15-4		15:43	1475	1834	1519	1832	1440	1831	1402	1828	15:58	1409	1827	15	26	1	
10/2/2013	15-4		15:59	1451	1828	1575	1830	1507	1822	1423	1829	16:14	1419	1825	13	34		
10/2/2013	15-4	16:30	16:15	1384	1821	1511	1835	1418	1828	1452	1824	16:30	1465	1833	30	27		
			Contractive Contra			Home and the second		**************************************					trash burn	ed for run	100	140		

Date	Run #	Run Time Start / End	Start Time Charge	Primary Temp °F Initial	Secondary Temp °F Initial	Primary Temp °F Plus 5 Min	Secondary Temp °F Plus 5 Min	Primary Temp °F Plus 10 Min	Secondary Temp °F Plus 10 Min	Primary Temp °F Plus 15 Min	Secondary Temp °F Plus 15 Min	End Charge (Time)	End Primary °F	End Secondary °F	Type II Waste Dry (lb)	Type III Waste Wet (lb)	Sludge (lb)	Adsorbs (lb)	Total Charge Wt (lb)
10/2/2013	129-4	8:46	8:46	1028	1810	1300	1842	1347	1814	1236	1829	9:01	1234	1830	37	17			54
10/2/2013	129-4		9:02	1219	1816	1399	1814	1350	1828	1323	1821	9:17	1322	1824	23	17			40
10/2/2013	129-4		9:18	1312	1819	1335	1816	1305	1826	1279	1822	9:33	1278	1825	10	39			49
10/2/2013	129-4		9:34	1272	1816	1449	1833	1392	1825	1345	1823	9:49	1344	1826	22	25			47
10/2/2013	129-4		9:50	1335	1822	1502	1834	1408	1832	1448	1827	10:05	1447	1832	24	19			43
10/2/2013	129-4		10:06	1445	1833	1528	1833	1384	1830	1462	1818	10:21	1463	1821	29	21			50
10/2/2013	129-4		10:22	1466	1827	1461	1821	1418	1820	1468	1832	10:37	1469	1826	42	15			57
10/2/2013	129-4	10:53	10:38	1468	1821	1481	1822	1404	1830	1471	1834	10:53	1467	1833	18	27			45
10/2/2013	123-4	11:57	11:57	1446	1822	1448	1820	1426	1818	1479	1819	12:12	1480	1825	25	18			43
10/2/2013	123-4		12:13	1480	1823	1496	1818	1399	1822	1466	1825	12:28	1468	1834	26	19			45
10/2/2013	123-4		12:29	1471	1820	1450	1819	1414	1818	1439	1824	12:44	1439	1834	32	18			50
10/2/2013	123-4		12:45	1438	1820	1502	1828	1446	1831	1405	1827	13:00	1411	1818	12	34			46
10/2/2013	123-4		13:01	1444	1837	1584	1835	1519	1819	1456	1836	13:16	1453	1822	12	35			47
10/2/2013	123-4		13:17	1444	1827	1550	1835	1482	1821	1434	1830	13:32	1432	1831	27	30			57
10/2/2013	123-4		13:33	1424	1829	1535	1820	1483	1820	1436	1820	13:48	1435	1825	11	42			53
10/2/2013	123-4	14:04	13:49	1427	1826	1405	1820	1469	1834	1421	1831	14:04	1418	1819	21	25			46
10/2/2013	15-4	15:11	15:11	1460	1828	1417	1835	1469	1822	1427	1823	15:26	1424	1818	28	24			52
10/2/2013	15-4		15:27	1386	1836	1500	1833	1399	1823	1504	1819	15:42	1502	1824	14	29			43
10/2/2013	15-4		15:43	1475	1834	1519	1832	1440	1831	1402	1828	15:58	1409	1827	15	26			41
10/2/2013	15-4		15:59	1451	1828	1575	1830	1507	1822	1423	1829	16:14	1419	1825	13	34			47
10/2/2013	15-4	16:30	16:15	1384	1821	1511	1835	1418	1828	1452	1824	16:30	1465	1833	30	27			57
														Total Wt =	471	541	0	0	1012

											_	
Average Temp =	1394	1825	1474	1827	1423	1824	1418	1826	1418	1826		Average Charge Wt =

Primary Chamber

Average Temp of 3 Runs =	1427 F
Minimum Temp of 3 Runs =	1028 F

Secondary Chamber

Secondary chamber		
Average Temp of 3 Runs =	1826 F	
Minimum Temp of 3 Runs =	1810 F	

Waste Composition

Waste Con	iposition				
MSW*	Sludge	Adsorbs	Total		
1012	0	0	1012		
100%	0%	0%	100%		

48

^{*}MSW = Type II + Type III